

# Chapter 9: Stress Transformation

## Chapter Objectives

- ✓ Navigate between rectilinear coordinate systems for stress components
- ✓ Determine principal stresses and maximum in-plane shear stress
- ✓ Determine the absolute maximum shear stress in 2D and 3D cases

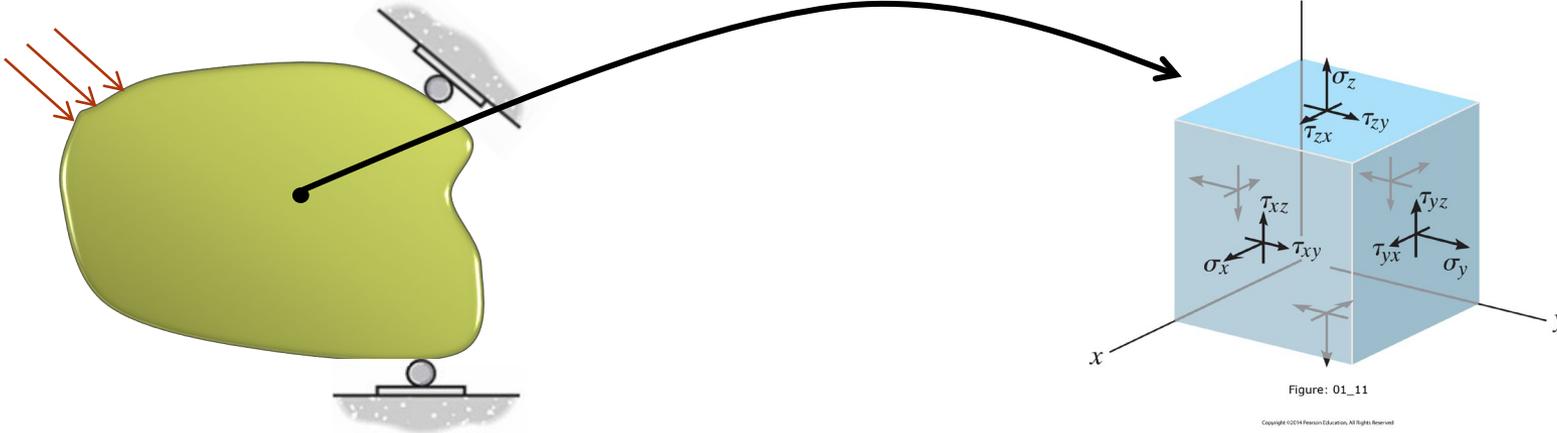


# General stress state

The general state of stress at a point is characterized by

- three independent normal stress components  $\sigma_x$ ,  $\sigma_y$ , and  $\sigma_z$
- three independent shear stress components  $\tau_{xy}$ ,  $\tau_{yz}$ , and  $\tau_{xz}$

At a given point, we can draw a stress element that shows the normal and shear stresses acting on the faces of a small (infinitesimal) cube of material surrounding the point of interest



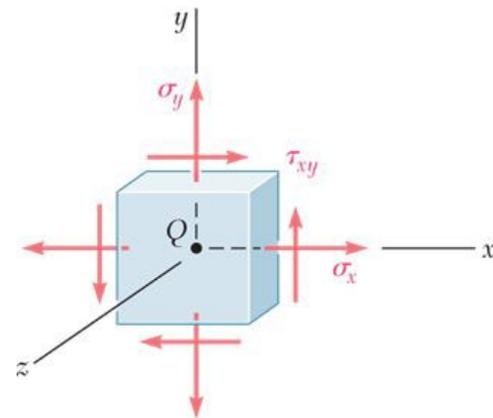
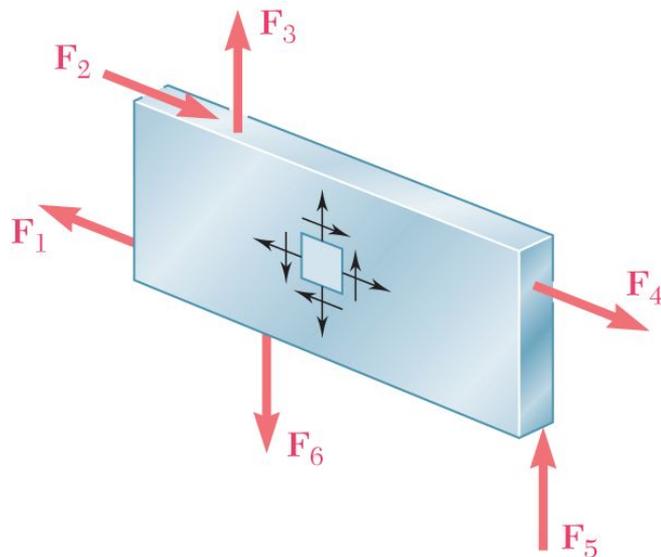
# Plane Stress

- Often, a loading situation involves only loads and constraints acting applied within a two-dimensional plane (e.g. the  $xy$  plane). In this case, any stresses acting in the third plane ( $z$  in this case) are equal to zero:

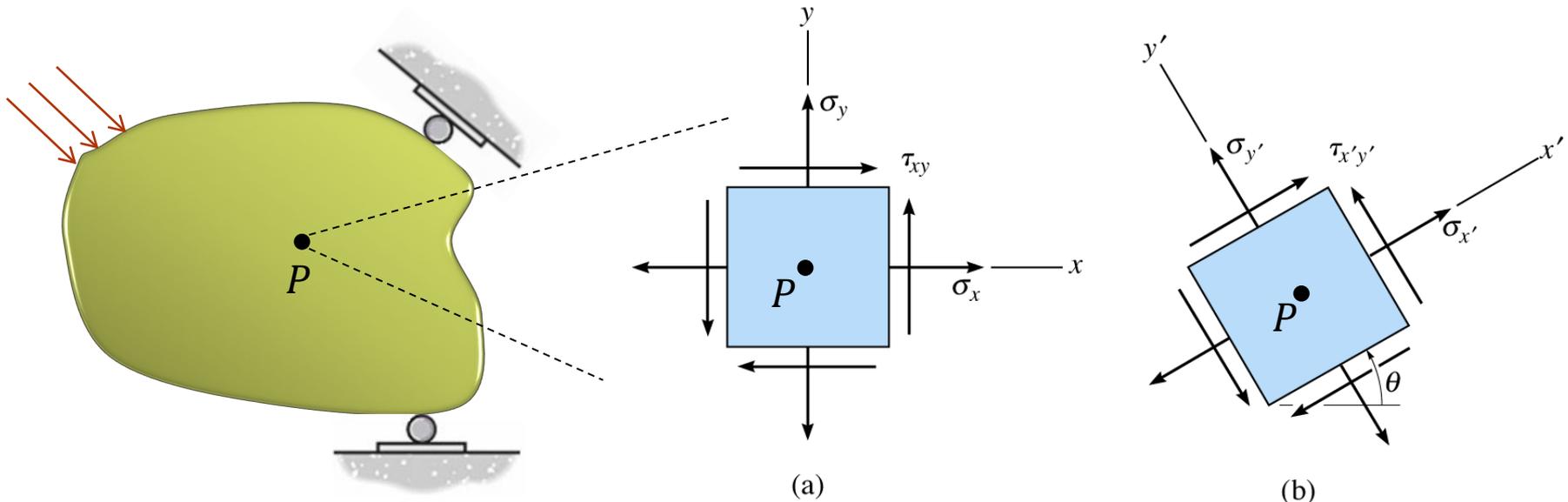
$$\sigma_z = \tau_{zx} = \tau_{zy} = 0$$

- Example:

Thin plates subject to forces acting in the mid-plane of the plate



# Plane Stress Transformation



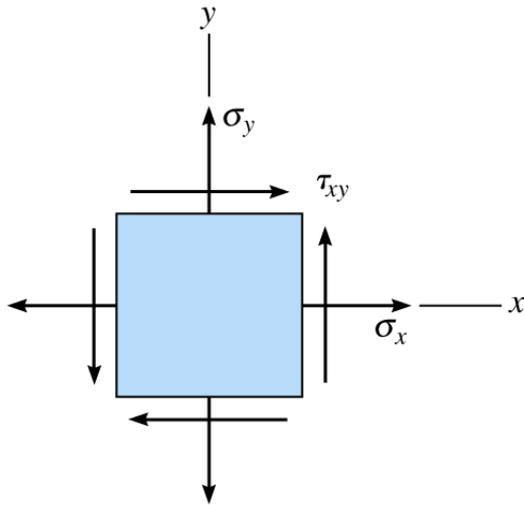
The stress tensor gives the **normal** and **shear stresses** acting on the faces of a cube (square in 2D) whose faces align with a particular coordinate system.

But, the choice of coordinate system is arbitrary. We are free to express the normal and shear stresses on any face we wish, not just faces aligned with a particular coordinate system.

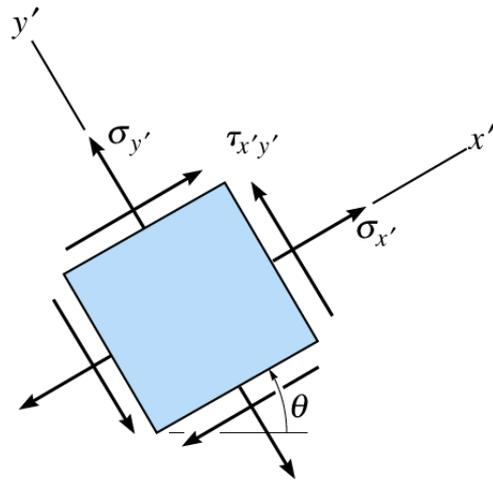
**Stress transformation equations** give us a formula/methodology for taking **known normal and shear stresses** acting on faces in one coordinate system (e.g.  $x$ - $y$  above) and **converting** them to normal and shear stresses on faces aligned with some other coordinate system (e.g.  $x'$ - $y'$  above)



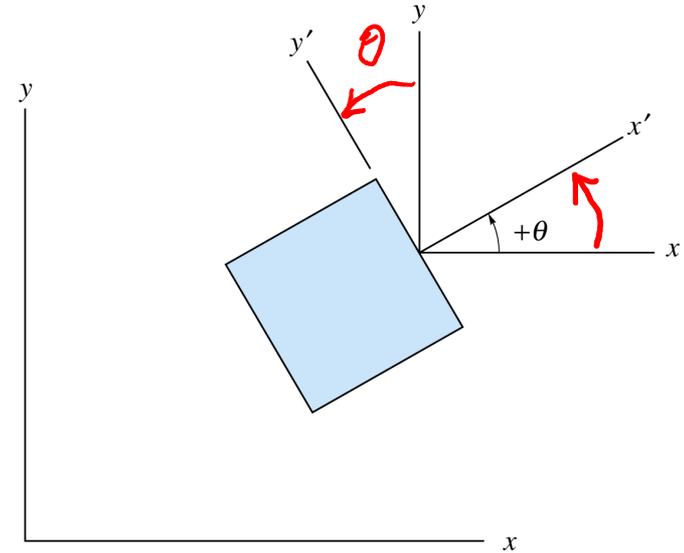
# Plane Stress Transformation



(a)



(b)

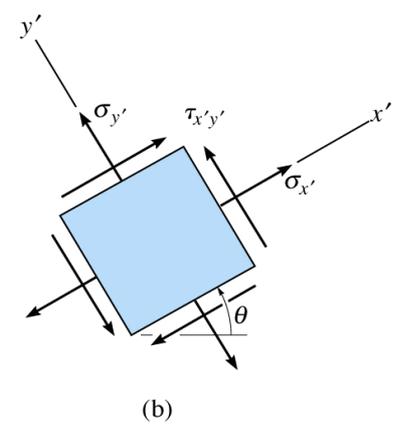
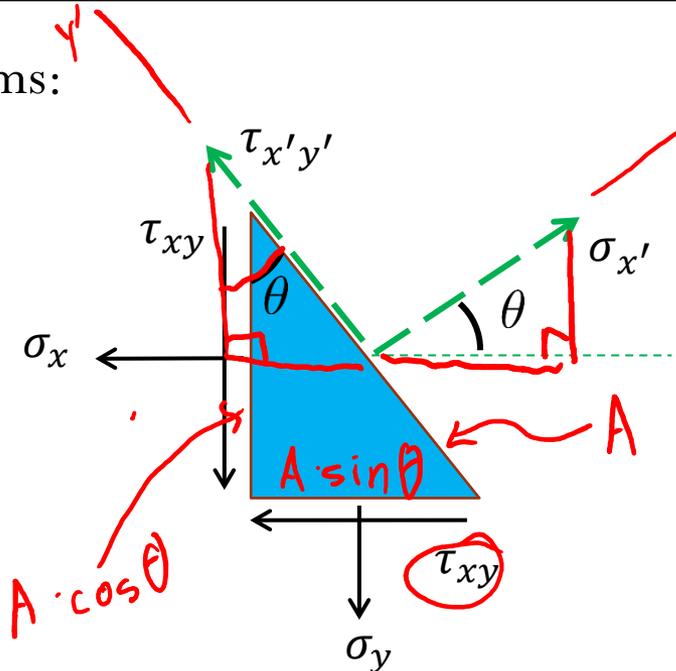
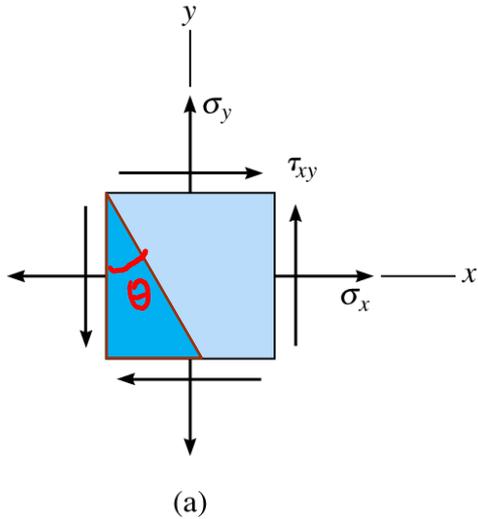


- Sign convention:

- Both the  $x$ - $y$  and  $x'$ - $y'$  system follow the right-hand rule
- The orientation of an inclined plane (on which the normal and shear stress components are to be determined) will be defined using the angle  $\theta$ . The angle  $\theta$  is measured from the positive  $x$  to the positive  $x'$ -axis. It is positive if it follows the curl of the right-hand fingers.



For two-dimensional problems:



$$\sum F_x = 0 \Rightarrow \sigma_x \cdot A \cdot \cos \theta - \tau_{xy} \cdot A \cdot \sin \theta + \sigma_{x'} \cdot \cos \theta \cdot A - \tau_{x'y'} \cdot \sin \theta \cdot A = 0$$

$$\sigma_x \cdot \cos \theta - \tau_{xy} \cdot \sin \theta + \sigma_{x'} \cdot \cos \theta - \tau_{x'y'} \cdot \sin \theta = 0$$

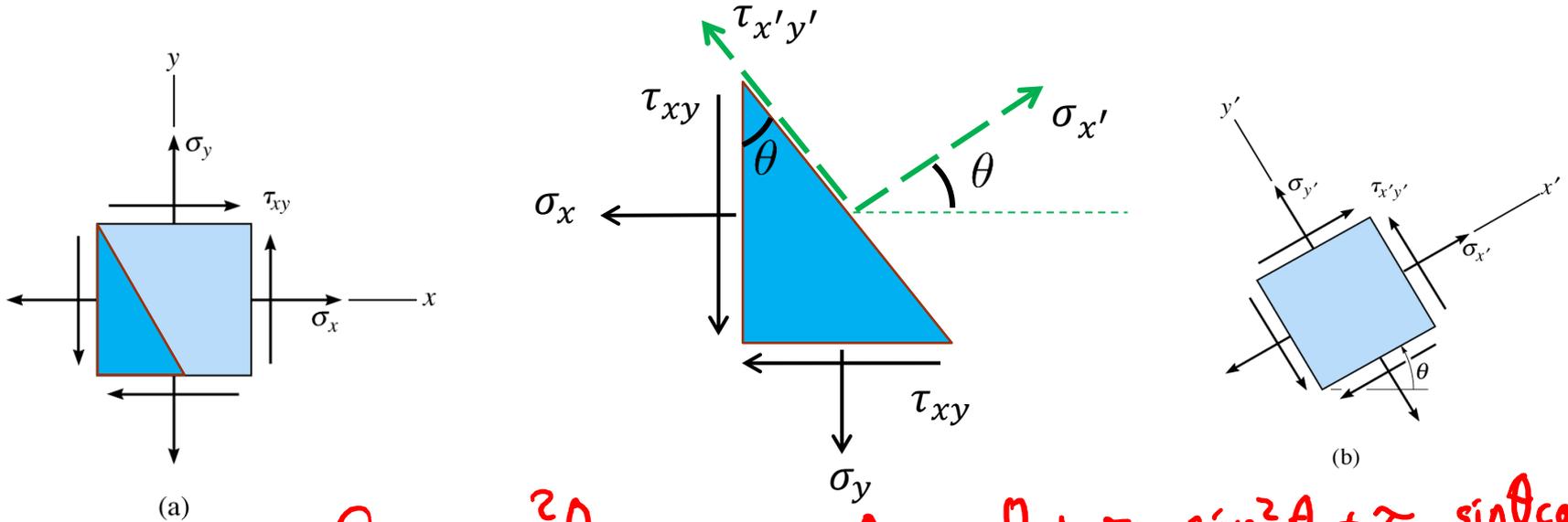
$$\sum F_y = 0 \Rightarrow -\sigma_y \cdot A \cdot \sin \theta - \tau_{xy} \cdot A \cdot \cos \theta + \sigma_{x'} \cdot \sin \theta \cdot A + \tau_{x'y'} \cdot \cos \theta \cdot A = 0$$

$$\sigma_{x'} \cdot \cos \theta - \tau_{x'y'} \cdot \sin \theta = -\sigma_x \cdot \cos \theta + \tau_{xy} \cdot \sin \theta$$

$$\sigma_{x'} \cdot \sin \theta + \tau_{x'y'} \cdot \cos \theta = \sigma_y \cdot \sin \theta + \tau_{xy} \cdot \cos \theta$$



For two-dimensional problems:



$$\begin{Bmatrix} \sigma_{x'} \\ \tau_{x'y'} \end{Bmatrix} = \begin{Bmatrix} \sigma_x \cdot \cos^2 \theta + \tau_{xy} \sin \theta \cdot \cos \theta + \sigma_y \cdot \sin^2 \theta + \tau_{xy} \sin \theta \cos \theta \\ -\sigma_x \cdot \sin \theta \cdot \cos \theta - \tau_{xy} \sin^2 \theta + \sigma_y \cdot \sin \theta \cos \theta + \tau_{xy} \cdot \cos^2 \theta \end{Bmatrix}$$

$$\sigma_{x'} = \sigma_x \cdot \cos^2 \theta + \sigma_y \cdot \sin^2 \theta + 2 \cdot \tau_{xy} \cdot \sin \theta \cdot \cos \theta$$

$$\tau_{x'y'} = (\sigma_y - \sigma_x) \cdot \sin \theta \cdot \cos \theta + \tau_{xy} \cdot (\cos^2 \theta - \sin^2 \theta)$$



We use the following trigonometric relations...

$$\cos^2 \theta = \frac{1 + \cos(2\theta)}{2}$$

$$\sin(2\theta) = 2 \sin \theta \cos \theta$$

$$\sin^2 \theta = \frac{1 - \cos(2\theta)}{2}$$

$$\cos(2\theta) = \cos^2 \theta - \sin^2 \theta$$

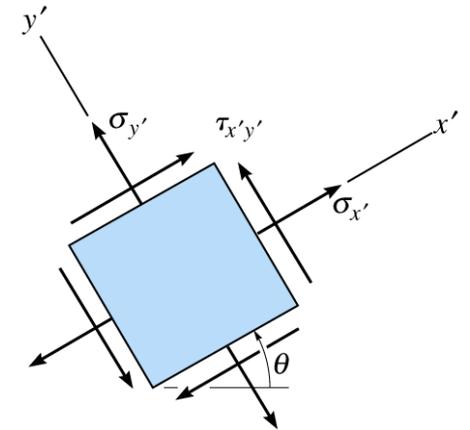
... to get

$$\sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} \quad \left( \frac{\sigma_x - \sigma_y}{2} \right)$$

$$\sigma_{x'} = \left( \frac{\sigma_x + \sigma_y}{2} \right) + \left( \frac{\sigma_x - \sigma_y}{2} \right) \cos(2\theta) + \tau_{xy} \sin(2\theta)$$

$$\tau_{x'y'} = - \left( \frac{\sigma_x - \sigma_y}{2} \right) \sin(2\theta) + \tau_{xy} \cos(2\theta)$$

$$\sigma_{y'} = \left( \frac{\sigma_x + \sigma_y}{2} \right) - \left( \frac{\sigma_x - \sigma_y}{2} \right) \cos(2\theta) - \tau_{xy} \sin(2\theta)$$



(b)

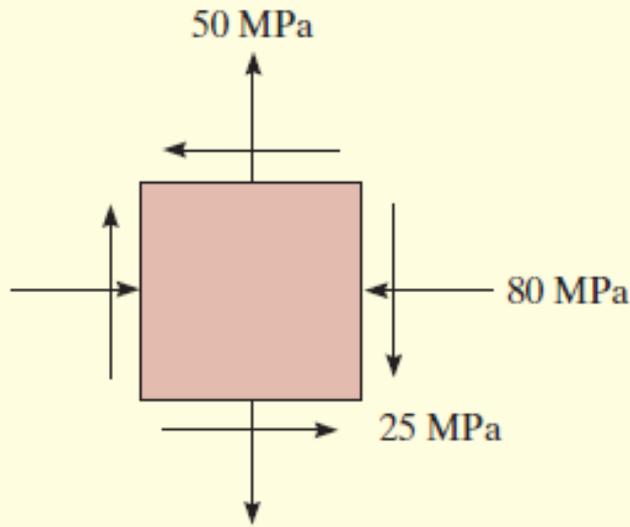
$$\frac{\sigma_{x'} + \sigma_{y'}}{2} = \sigma_{avg}$$

Note that:

$$\frac{\sigma_{x'} + \sigma_{y'}}{2} = \frac{\sigma_x + \sigma_y}{2} = \sigma_{avg}$$



**Example 1:** The state of plane stress at a point is represented by the element shown in the figure below. Determine the state of stress at the point on another element oriented  $30^\circ$  clockwise from the position shown.



$$\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) + \tau_{xy} \sin(2\theta)$$

$$\tau_{x'y'} = -\frac{\sigma_x - \sigma_y}{2} \sin(2\theta) + \tau_{xy} \cos(2\theta)$$

$$\sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos(2\theta) - \tau_{xy} \sin(2\theta)$$

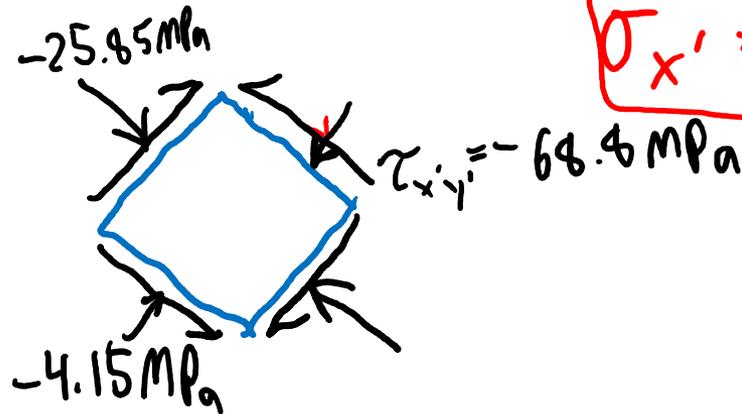
$2\theta = -60^\circ$

$$\sigma_{x'} = \frac{-80 + 50}{2} + \frac{-80 - 50}{2} \left(\frac{1}{2}\right) + (-25) \cdot \left(-\frac{\sqrt{3}}{2}\right) = -25.85$$

MPa

$$\tau_{x'y'} = -68.8 \text{ MPa}$$

$$\sigma_{y'} = -4.15 \text{ MPa}$$



$$\sigma_{x'} = -25.85 \text{ MPa}$$

