

TAM 212 – Dynamics

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Recap

- Rigid Bodies in Contact, Gears

Today

- Rigid Body Acceleration, Gears

stick = no relative velocity at contact

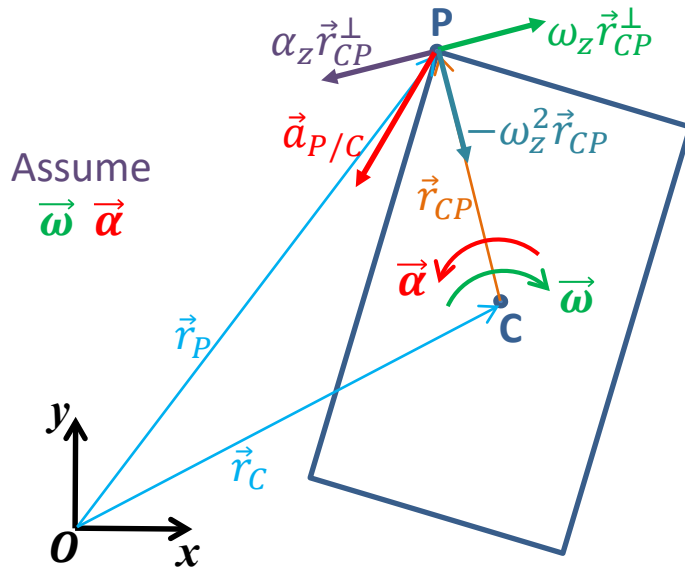
$$\vec{v}_A = \vec{v}_B \quad v_{An} = v_{Bn}$$

slip = relative velocity at contact

$$\vec{v}_A \neq \vec{v}_B \quad v_{An} = v_{Bn}$$

Gears:

$$\frac{\omega_{1z}}{\omega_{2z}} = -\frac{r_2}{r_1}$$



$$\vec{r}_P = \vec{r}_C + \vec{r}_{CP}$$

$$\vec{v}_P = \vec{v}_C + \vec{\omega} \times \vec{r}_{CP}$$

$$\begin{aligned} \vec{a}_P &= \vec{a}_C + \vec{\alpha} \times \vec{r}_{CP} + \vec{\omega} \times (\vec{\omega} \times \vec{r}_{CP}) \end{aligned}$$

For 2D x-y plane:

$$\vec{r}_P = \vec{r}_C + \vec{r}_{CP}$$

$$\vec{v}_P = \vec{v}_C + \omega_z \vec{r}_{CP}^\perp$$

$$\vec{a}_P = \vec{a}_C + \alpha_z \vec{r}_{CP}^\perp - \omega_z^2 \vec{r}_{CP}$$

Standard Sign Conventions

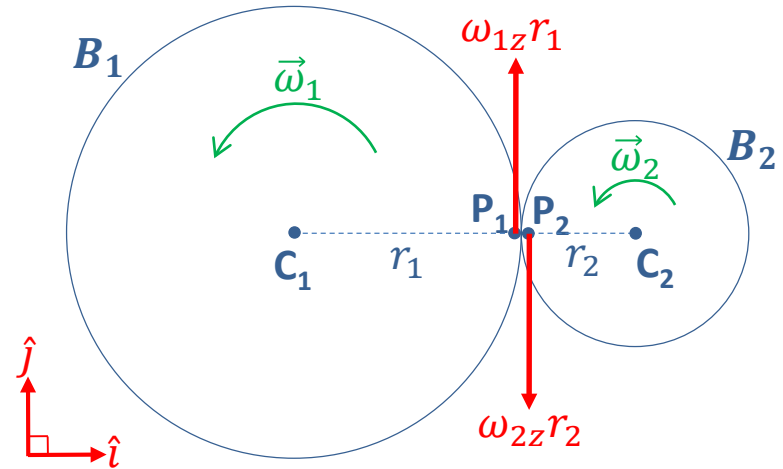
$$\begin{aligned}\vec{v}_{P_1} &= \vec{v}_{C_1} + \vec{\omega}_1 \times \vec{r}_{C_1 P_1} \\ &= 0 + (0, 0, \omega_{1z}) \times (r_1, 0, 0) \\ &= (0, \omega_{1z} r_1, 0)\end{aligned}$$

$$\begin{aligned}\vec{v}_{P_2} &= \vec{v}_{C_2} + \vec{\omega}_2 \times \vec{r}_{C_2 P_2} \\ &= 0 + (0, 0, \omega_{2z}) \times (-r_2, 0, 0) \\ &= (0, -\omega_{2z} r_2, 0)\end{aligned}$$

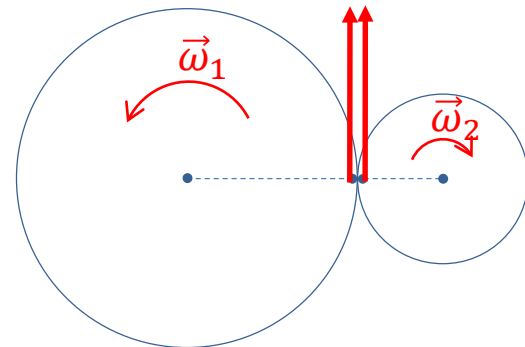
$$\vec{v}_{P_1} = \vec{v}_{P_2}$$

$$\omega_{1z} r_1 = -\omega_{2z} r_2$$

$$\frac{\omega_{1z}}{\omega_{2z}} = -\frac{r_2}{r_1}$$

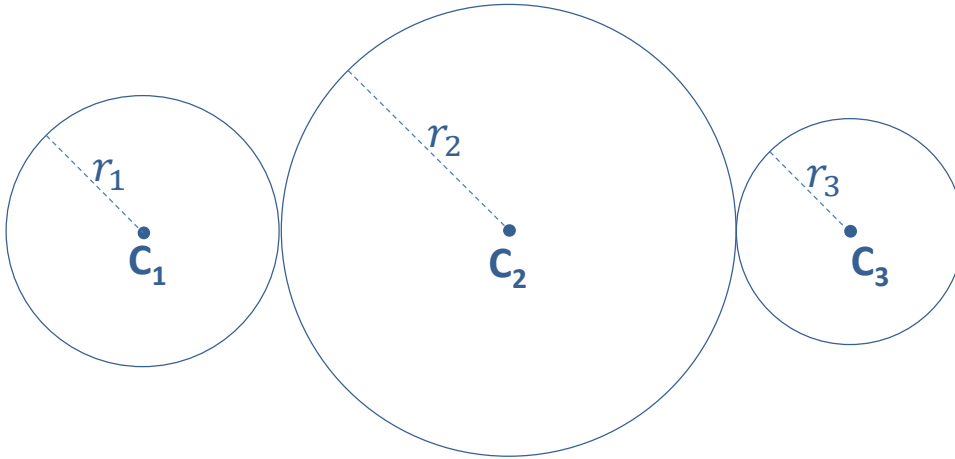


Standard sign convention uses CCW as positive direction for $\vec{\omega}$ and let the resulting sign of ω to determine the actual direction.



Alternative sign convention

Example

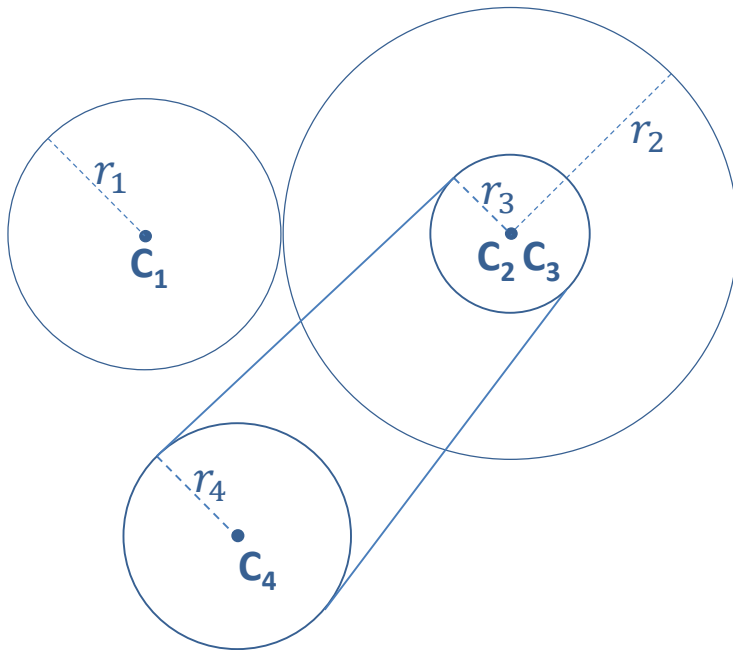


$$\left| \frac{\omega_{3Z}}{\omega_{1Z}} \right| = \begin{array}{l} \text{A. } \frac{r_1}{r_3} \\ \text{B. } \frac{r_3}{r_1} \\ \text{C. } \frac{r_1 r_3}{r_2} \\ \text{D. } \frac{r_2}{r_1 r_3} \end{array}$$

$$\frac{\omega_{3Z}}{\omega_{1Z}} = \boxed{} \text{ —————}$$

- A. Positive sign
- B. Negative sign

Example



$$\left| \frac{\omega_{4Z}}{\omega_{1Z}} \right| = \begin{matrix} \text{A.} & \frac{r_1 r_2}{r_3 r_4} \\ \text{B.} & \frac{r_1 r_4}{r_2 r_3} \\ \text{C.} & \frac{r_2 r_3}{r_1 r_4} \\ \text{D.} & \frac{r_1 r_3}{r_2 r_4} \\ \text{E.} & \frac{r_3 r_4}{r_1 r_2} \end{matrix}$$

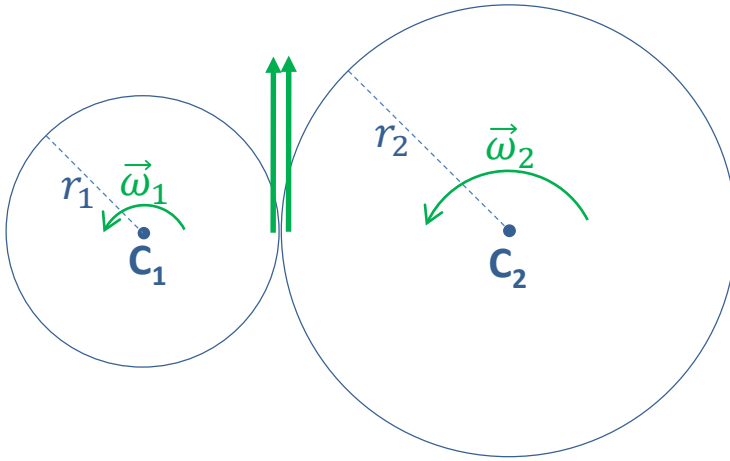
$$\frac{\omega_{4Z}}{\omega_{1Z}} = \boxed{} \text{ —————}$$

- A. Positive sign
- B. Negative sign

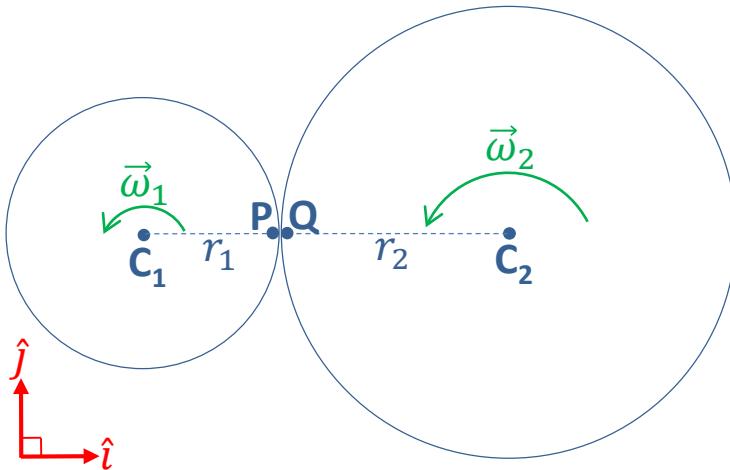
Acceleration in contact (“no slip”)

1. Differentiate velocity expressions

$$\frac{\omega_{2z}}{\omega_{1z}} = -\frac{r_1}{r_2}$$
$$\omega_{1z}r_1 = -\omega_{2z}r_2$$

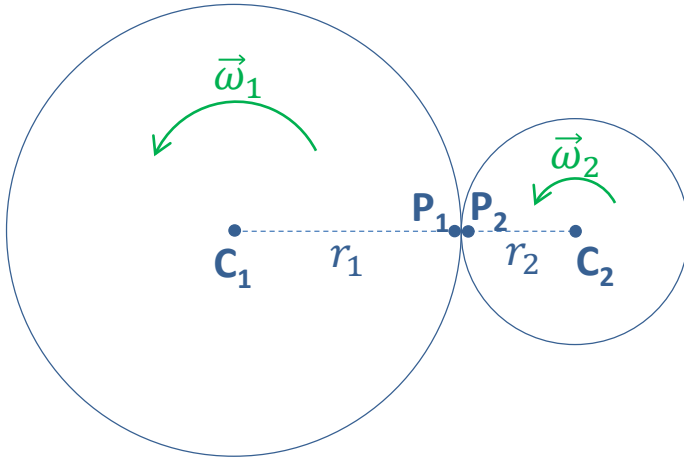


2. Contacting points have equal tangential acceleration



Gear Drives

Gears

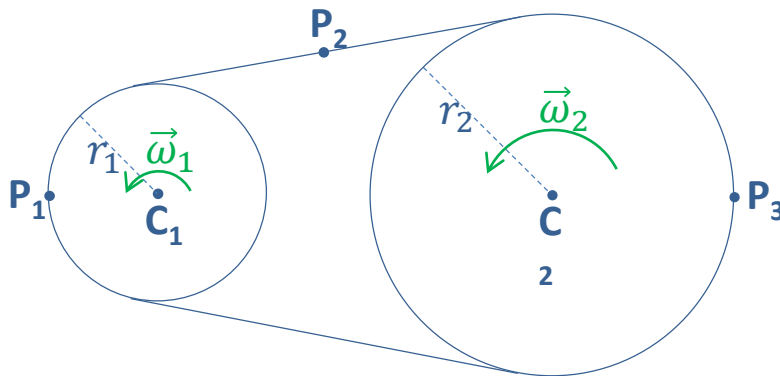


$$\vec{v}_{P_1} = \vec{v}_{P_2} \quad \leftarrow \text{no slip}$$

$$\frac{\omega_{2z}}{\omega_{1z}} = -\frac{r_1}{r_2}$$

larger gear spins slower
opposite directions

Chains

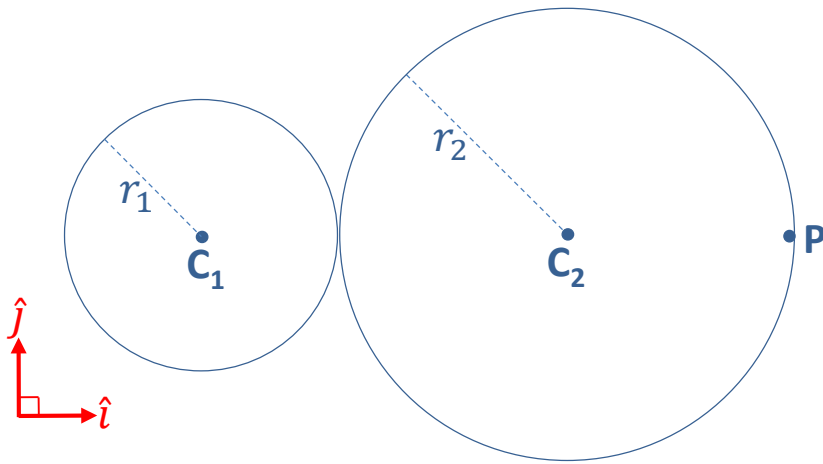


$$v_{P_1} = v_{P_2} = v_{P_3} \quad \leftarrow \text{same speeds}$$

$$\frac{\omega_{2z}}{\omega_{1z}} = \frac{r_1}{r_2}$$

larger gear spins slower
same directions

Example



$$r_1 = 2 \text{ m}$$

$$r_2 = 4 \text{ m}$$

$$\vec{\omega}_1 = 2\hat{k} \text{ rad/s}$$

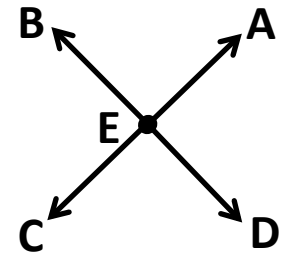
$$\vec{\alpha}_1 = -4\hat{k} \text{ rad/s}^2$$

$$\vec{a}_P = (a_{P_x}, a_{P_y})$$

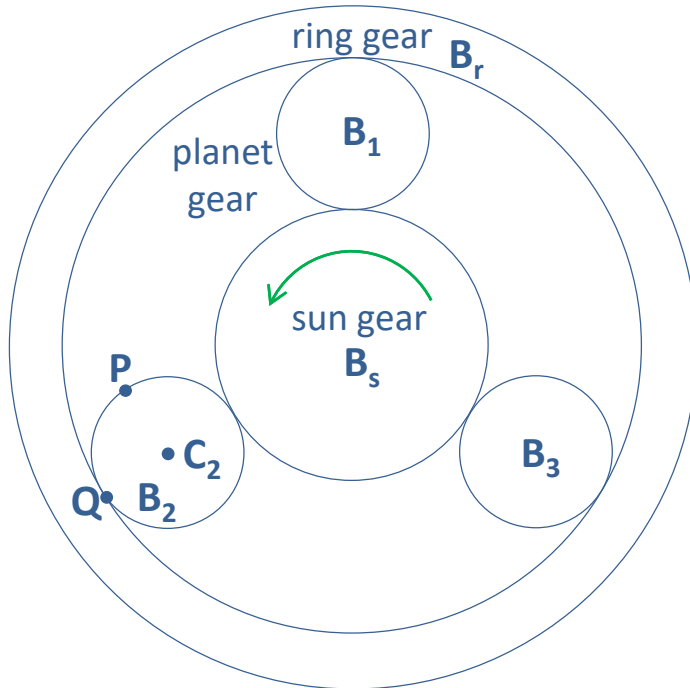
$$|a_{P_x}| = \text{A. 1} \quad \text{B. 2} \quad \text{C. 4} \quad \text{D. 8} \quad \text{E. 16 (m/s}^2\text{)}$$

$$|a_{P_y}| = \text{A. 1} \quad \text{B. 2} \quad \text{C. 4} \quad \text{D. 8} \quad \text{E. 16 (m/s}^2\text{)}$$

What is the direction of $\vec{a}_P$?



Example

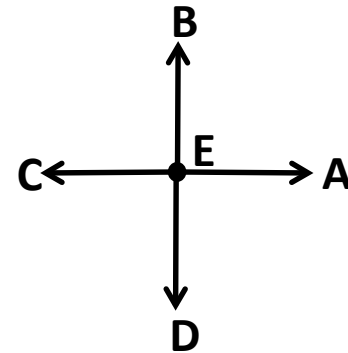


Planetary gears

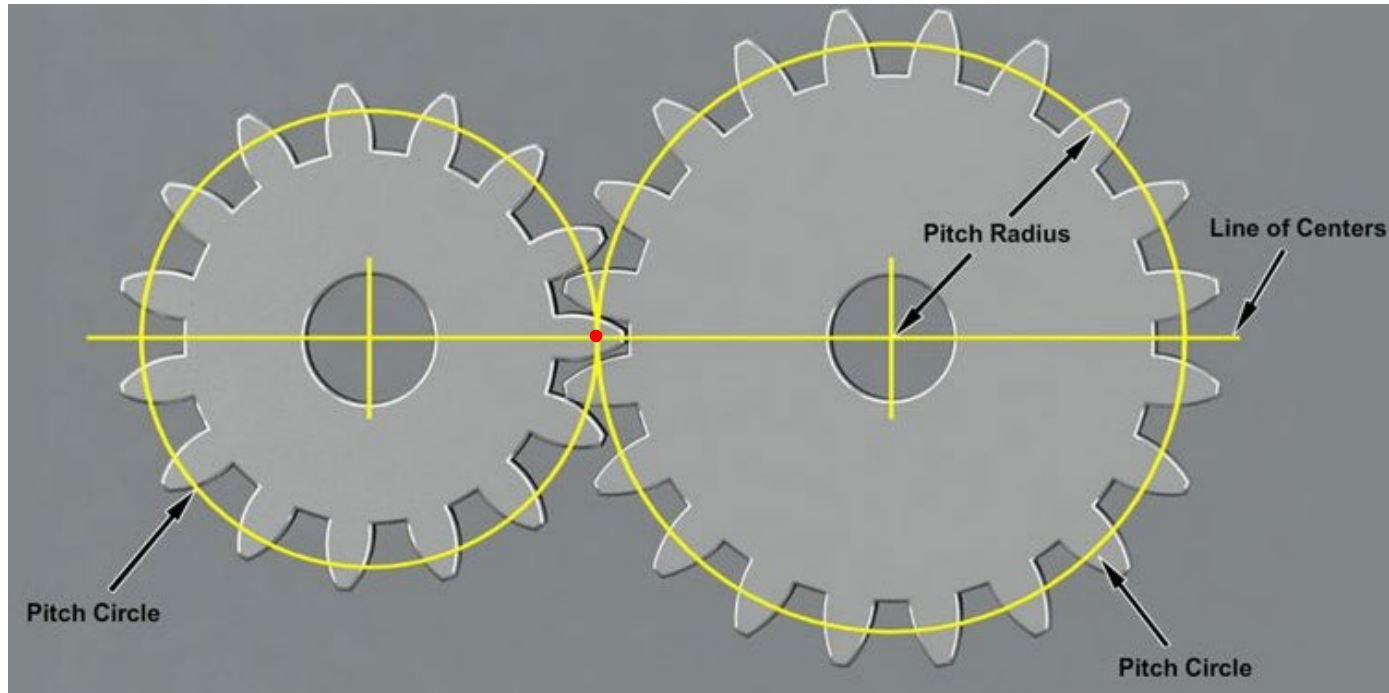
ring fixed

$$\omega_{sZ} = 2 \text{ rad/s}$$

What is the direction of $\vec{v}_P$?



Contact Point



Speed and torque are transmitted at the **contact point**. The contact point is between the gear teeth along a line that passes through the line of centers of the two gears. This is a simplified view of the complex interaction between two gears. In this view, adopted in TAM 212, the contact point between two pitch circles is “not moving” and the transferring of torque is ideal (without losses).