

Plan of the Lecture

- ▶ **Review:** Proportional-Integral-Derivative (PID) control
- ▶ **Today's topic:** introduction to Root Locus design method

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Reading: FPE, Chapter 5

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Reading: FPE, Chapter 5

Note!! The way I teach the Root Locus differs a bit from what the textbook does (good news: it is simpler). Still, **pay attention in class!!**

Course structure so far:

modeling	—	examples
↓		
analysis	—	transfer function, response, stability
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design	—	some simple examples given

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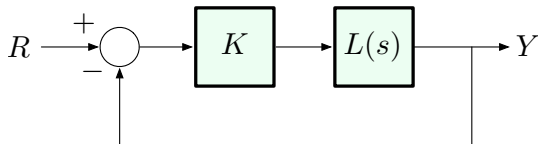
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We will focus on design from now on.

The Root Locus Design Method

(invented by Walter R. Evans in 1948)

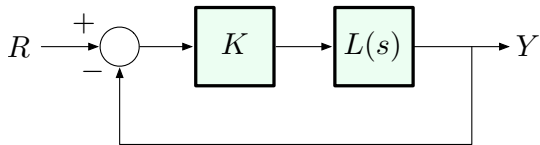
Consider this unity feedback configuration:



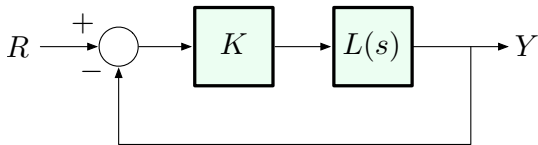
where

- ▶ K is a constant gain
- ▶ $L(s) = \frac{b(s)}{a(s)}$, where $a(s)$ and $b(s)$ are some polynomials

The Root Locus Design Method

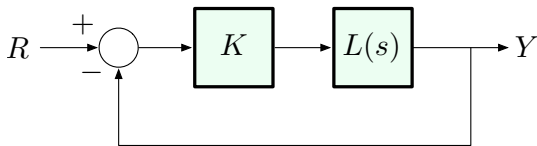


The Root Locus Design Method



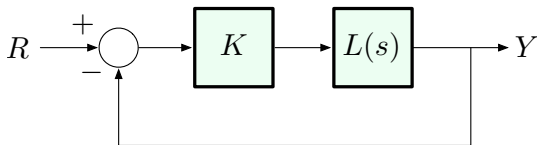
Closed-loop transfer function:

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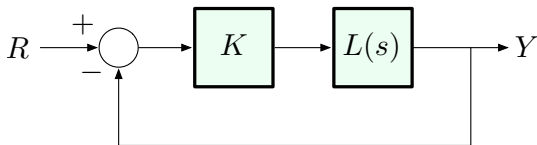
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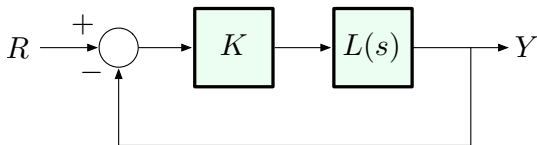


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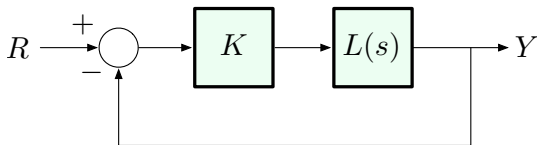


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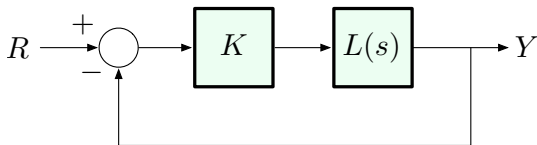
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$$\underbrace{a(s) + Kb(s)}_{\text{characteristic polynomial}} = 0$$

characteristic equation

A Comment on Change of Notation

Note the change of notation:

$$\text{from } H(s) \text{ or } G(s) = \frac{q(s)}{p(s)} \quad \text{to } L(s) = \frac{b(s)}{a(s)}$$

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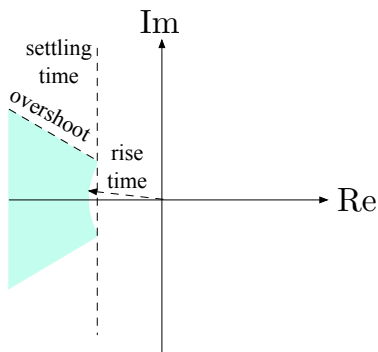
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As long as we can represent the poles of the closed-loop transfer function as roots of the equation $1 + KL(s) = 0$ for *some choice* of K and $L(s)$, we can apply the RL method.

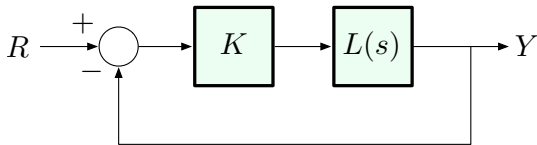
Towards Quantitative Characterization of Stability

Qualitative description of stability: Routh test gives us a range of K to guarantee stability.



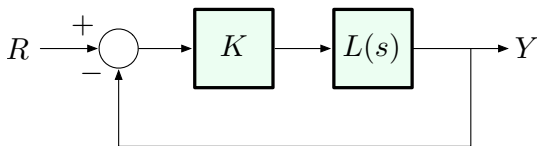
For what values of K do we best satisfy given design specs?

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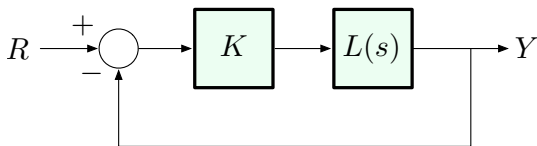
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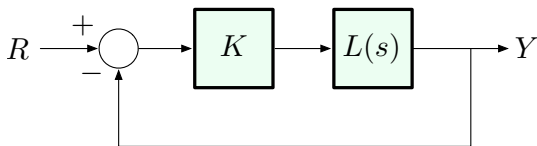


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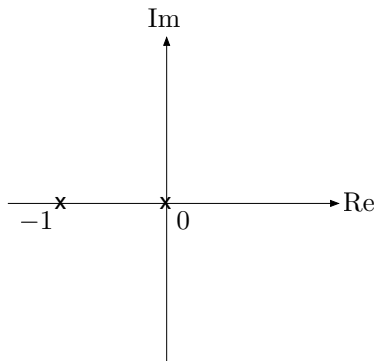
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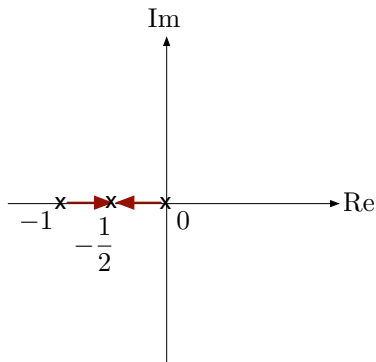
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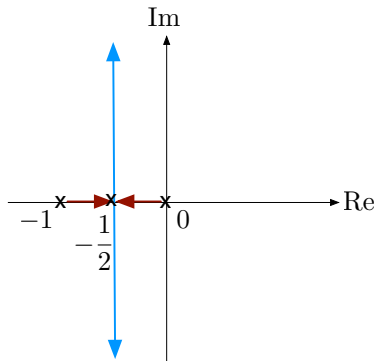
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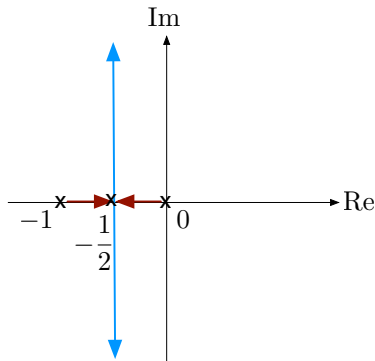


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($s = -1/2$ is the *point of breakaway* from the real axis)

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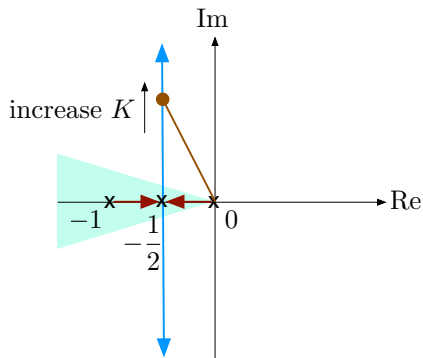
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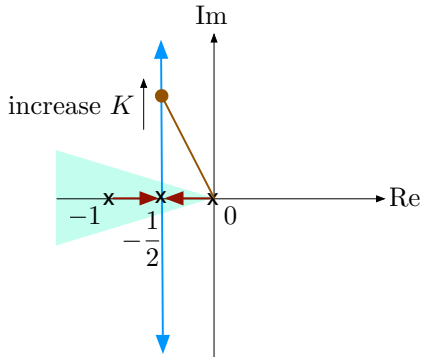
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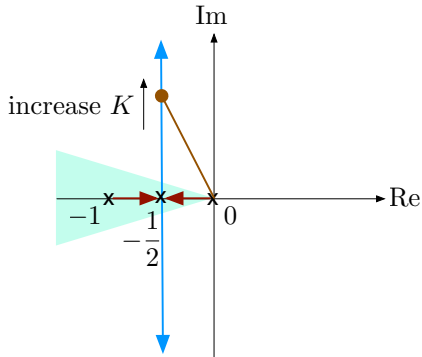
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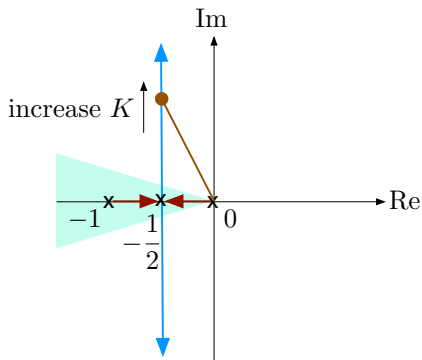


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Our goal: develop simple rules for (approximately) sketching the root locus in the general case.

Equivalent Characterization of RL: Phase Condition

Recall our original definition: The *root locus* for $1 + KL(s)$ is the set of all closed-loop poles, i.e., the roots of

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This gives us an equivalent characterization:

The phase condition: The root locus of $1 + KL(s)$ is the set of all $s \in \mathbb{C}$, such that $\angle L(s) = 180^\circ$, i.e., $L(s)$ is real and negative.

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Today, we will cover mostly Rules A–C (and a bit of D).

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$$1 + K \frac{b(s)}{a(s)} = 1 + K \frac{s^m + b_1 s^{m-1} + \dots + b_{m-1} s + b_m}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n} = 0$$

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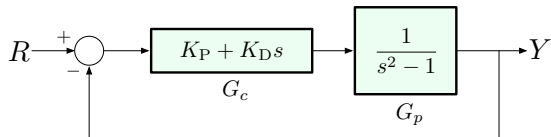
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Note: if $n > m$, we have n branches, but only m zeros. The remaining $n - m$ branches go off to infinity (end at “zeros at infinity”).

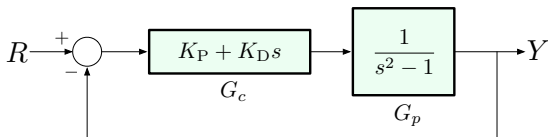
Example

PD control of an unstable 2nd-order plant



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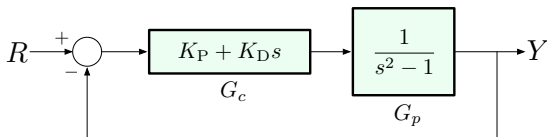
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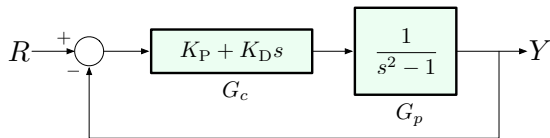
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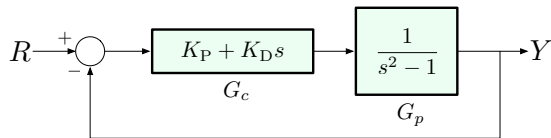
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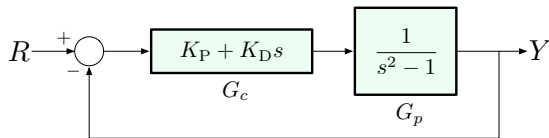


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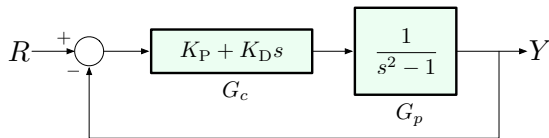
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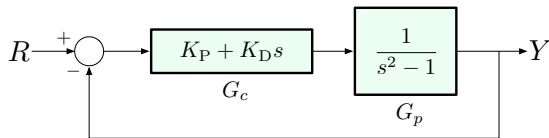
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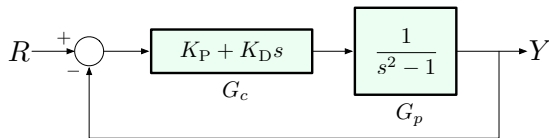
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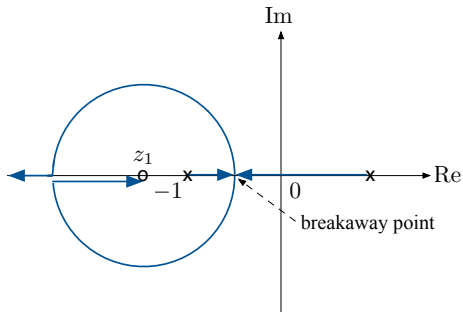
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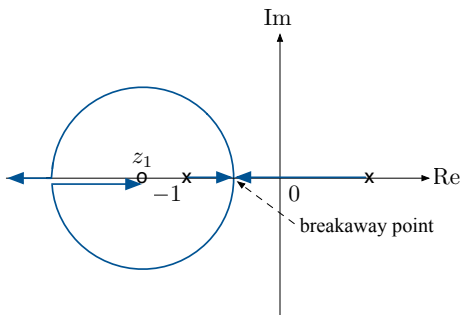
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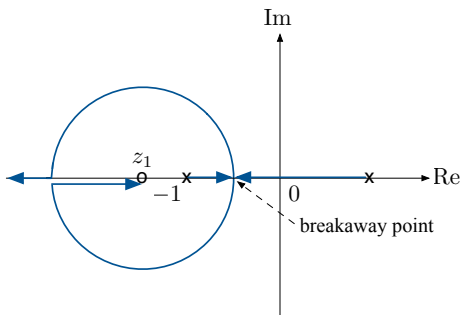
So the root locus will look something like this:



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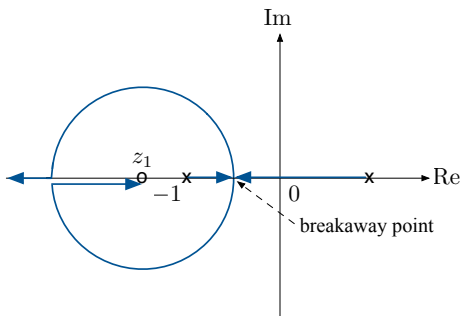


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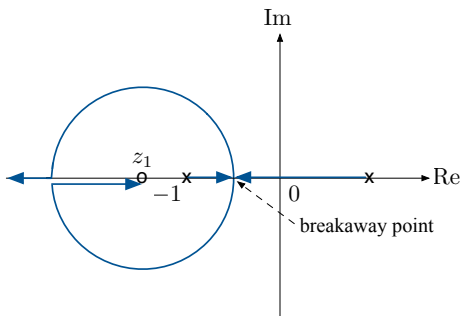
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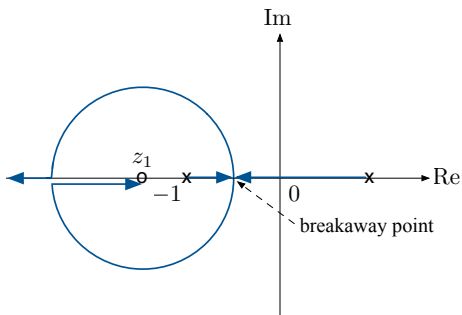


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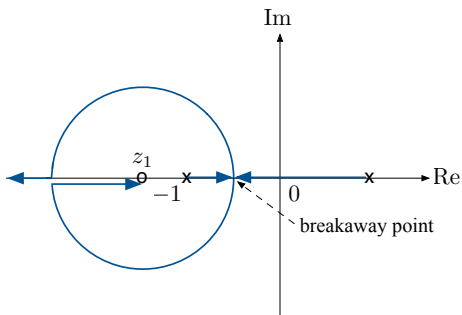
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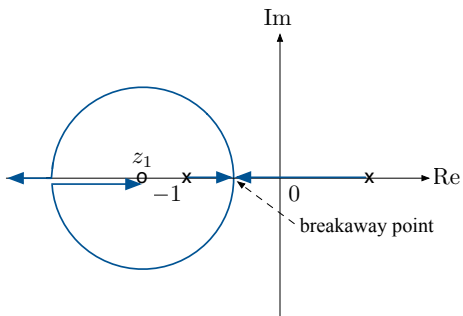
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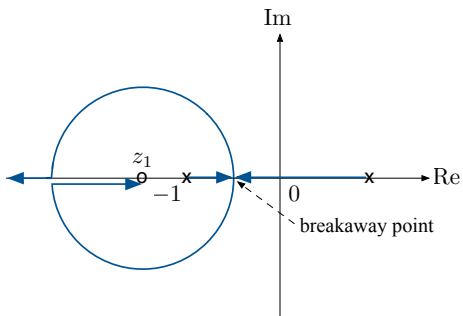
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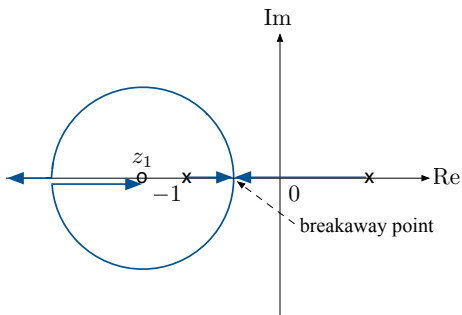


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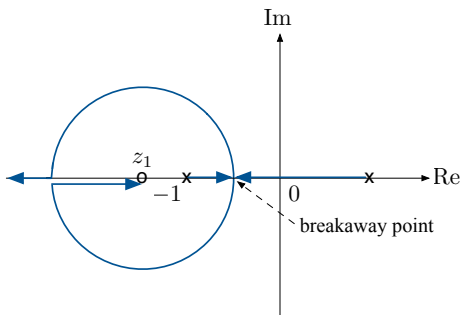
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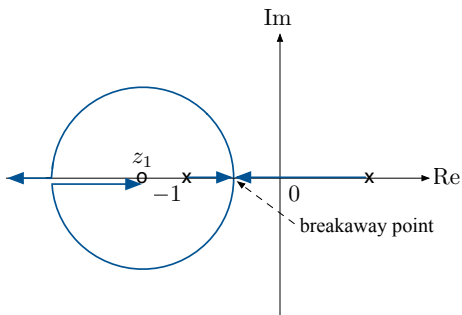


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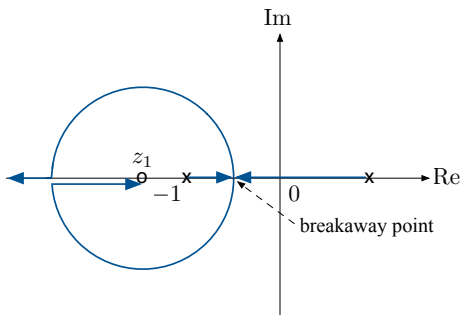
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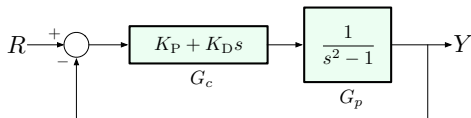
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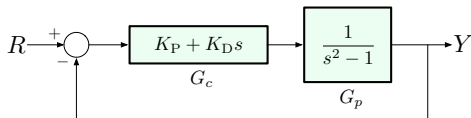
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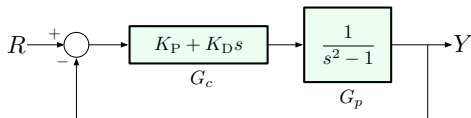


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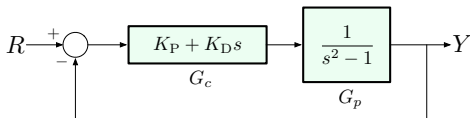
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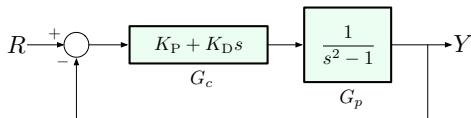
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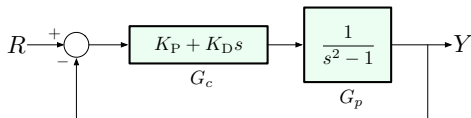
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$$\text{Relate to 2nd-order response: } \omega_n^2 = 9, \quad 2\zeta\omega_n = 5 \implies \zeta = 5/6$$

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But: Rules A–C cannot tell the whole story. How do we know which way the branches go, and which pole corresponds to which zero?

Main Points

- ▶ When zeros are in LHP, *high gain* can be used to stabilize the system (although one must worry about zeros at infinity).
- ▶ If there are zeros in RHP, high gain is always disastrous.
- ▶ PD control is effective for stabilization because it introduces a zero in LHP.

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Rules D–F!!

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Example

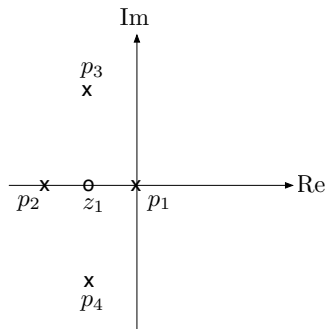
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Example, continued

Three more rules:

- ▶ Rule D: real locus
- ▶ Rule E: asymptotes
- ▶ Rule F: $j\omega$ -crossings

Example, continued

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- ▶ Rule D: real locus
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Rules D and E are both based on the fact that

$$1 + KL(s) = 0 \text{ for some } K > 0 \iff L(s) < 0$$

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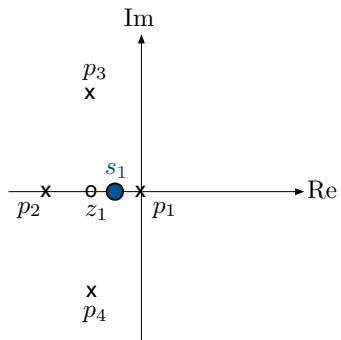
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— this sum must be $\pm 180^\circ$ for *any* s that lies on the RL.

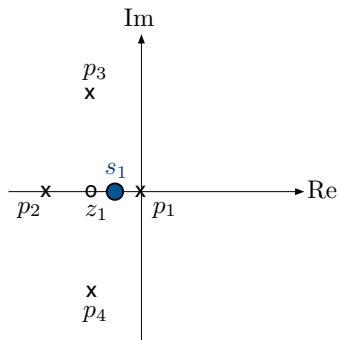
Rule D: Real Locus

So, we try test points:



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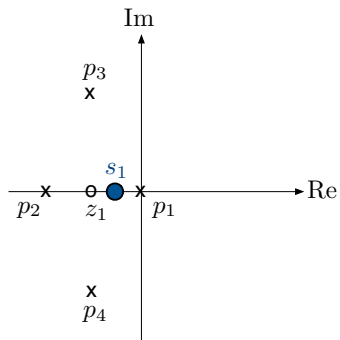
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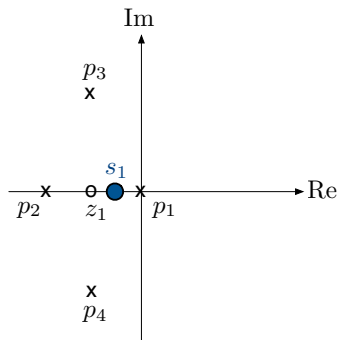


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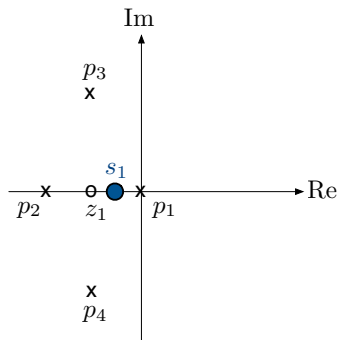
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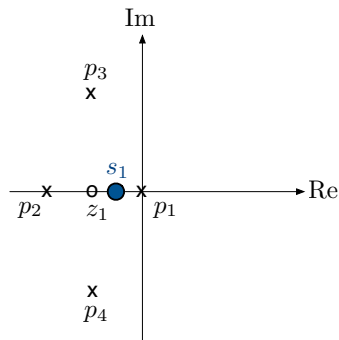
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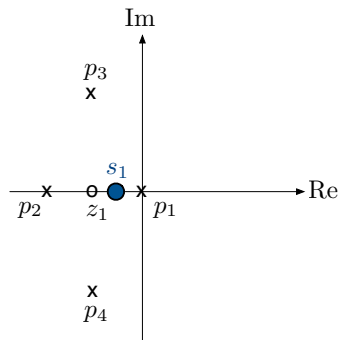
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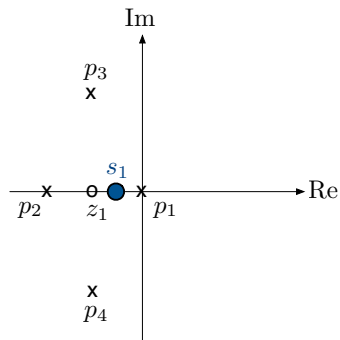
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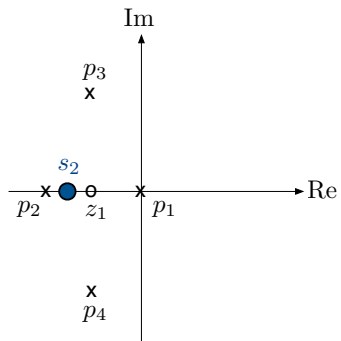
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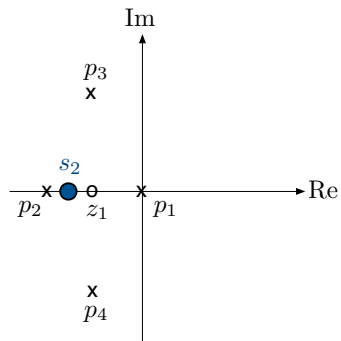
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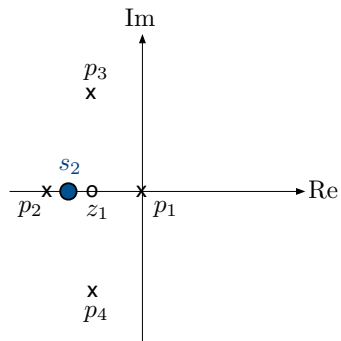
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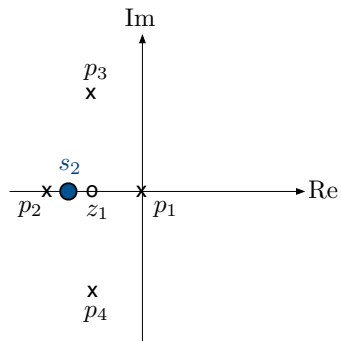


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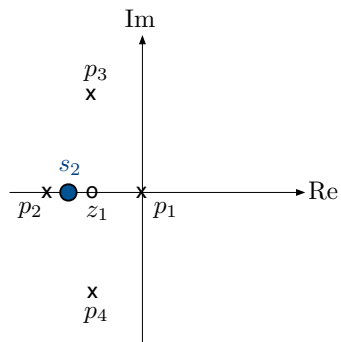
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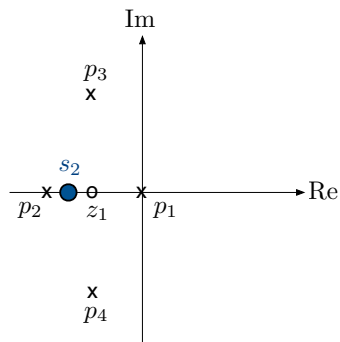
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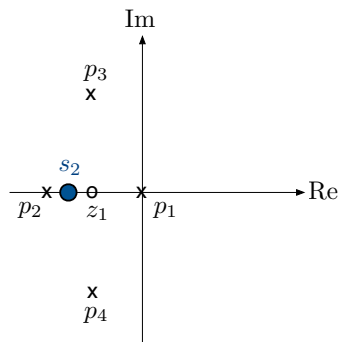
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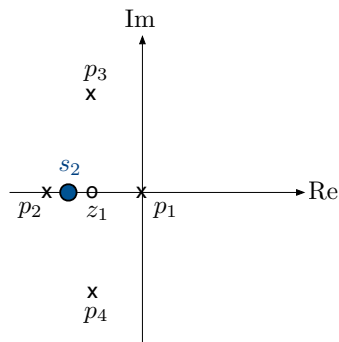
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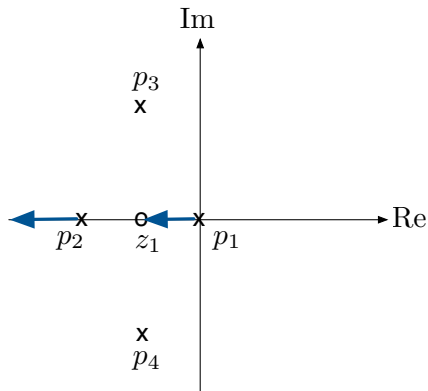
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Rule D: If s is *real*, then it is on the RL of $1 + KL$ if and only if there are an odd number of *real open-loop poles and zeros* to the right of s .

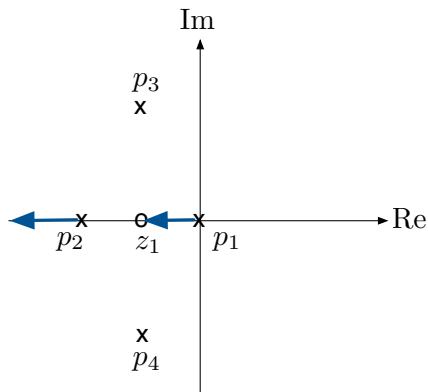
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We will cover Rules E and F, and complete the RL for this example, in the next lecture.