

You may not open the exam book or start your exam until you are told otherwise.

Instructions:

- Read each problem carefully.
- Write legibly and in complete sentences.
- Justify *all* your answers to earn full credit.
- Cross out *anything* you do not want to be graded.
- You *must not* use books or electronics except for
 - a sheet of notes of the size up to letter (8.5×11 inch), double sided;
 - a simple calculator not capable of symbolic computing.
- You have 80 minutes to complete this exam.
- Respond to all *four* problems.

Stay calm and good luck!

Name (Print): YUN HAN

1. (20 points)

- (a) (6 points) Consider a minimum phase transfer function $G(s)$. If a scalar gain K manages to make the local slope ≈ -45 dB per decade at the crossover frequency ω_c in the Bode magnitude plot of $KG(s)$, for a unity *negative* feedback configuration, is the closed-loop system stable? Why or why not? Justify your answer.

[Hint: You can assume the crossover frequency is far away from any breakpoint frequencies so that you can use Bode's Phase-Gain relationship.]

solution: Note, -2 /decade (in absolute units)

$$\longleftrightarrow -40 \text{ dB/decade}$$

$$\begin{aligned} \text{local slope} \cong -45 \text{ dB per decade} &\Rightarrow \text{local slope} = -\frac{45}{20} \\ &= -2.25 \text{ (in abs units)} \end{aligned}$$

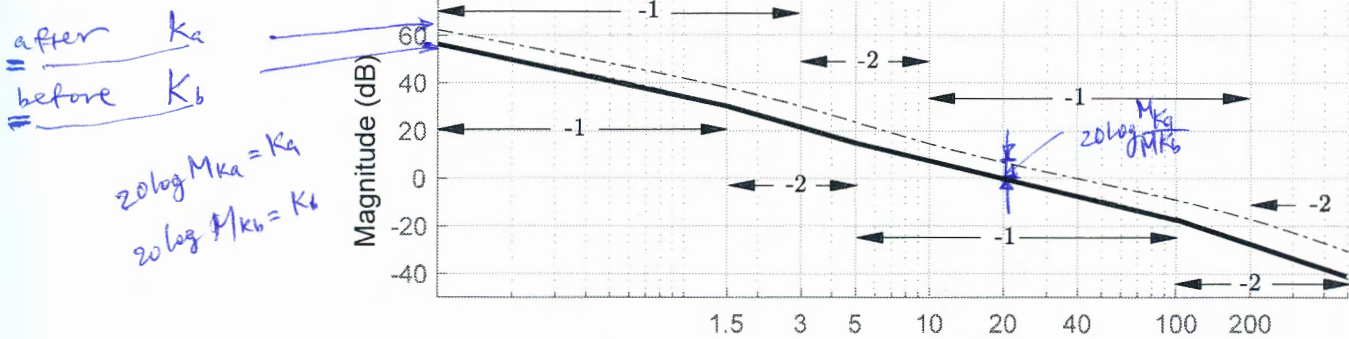
By Bode's Phase-Gain relationship, the phase at crossover frequency

$$\begin{aligned} \text{is about } -2.25 \times \frac{\pi}{2} &= -\left(\frac{2.25}{2}\right) \pi \\ &< (-1) \pi \end{aligned}$$

i.e. $PM < 0^\circ$.

The closed-loop system is not stable.

- (b) (14 points) Consider a system forward path transfer function $G(s)$. The (asymptotic) Bode magnitude plot below shows the magnitude **before** (thick solid line) and **after** (dash dotted line) a controller $G_c(s)$ was added to the forward path (in serial connection). By this Bode plot, what is the transfer function of this controller $G_c(s)$? You can leave $G_c(s)$ in Bode form. -1 and -2 in the figure refer to local slopes. Slopes above the graphs are for the **after** and slopes below for the **before**.



solution: Before $G_c(s)$ was added, $G(s) = \frac{MK_b}{s} \cdot \frac{1}{(\frac{1}{1.5}s+1)} \cdot \frac{1}{(\frac{1}{5}s+1)} \cdot \frac{1}{\frac{1}{100}s+1}$

After $G_c(s)$ was added, $G_c(s)G(s) = \frac{MK_a}{s} \cdot \frac{1}{\frac{1}{3}s+1} \cdot \frac{1}{(\frac{1}{10}s+1)} \cdot \frac{1}{\frac{1}{200}s+1}$

Therefore $G_c(s) = \left(\frac{MK_a}{MK_b} \right) \frac{\frac{1}{1.5}s+1}{\frac{1}{3}s+1} \cdot \frac{1}{(\frac{1}{10}s+1)} \cdot \frac{\frac{1}{100}s+1}{\frac{1}{200}s+1}$

$\left[\begin{array}{l} MK_a \text{ can be calculated by } |G_c(j\omega)G(j\omega)|=1, \quad MK_a \approx 134. \\ MK_b \text{ can be calculated by } |G(j\omega)|=1, \quad MK_b \approx 67. \end{array} \right]$

But we only need the ratio $\left(\frac{MK_a}{MK_b} \right)$.

$\frac{d(\log M)}{d(\log \omega)} = -1$, Note, by geometry, $\frac{d(\log \frac{MK_a}{MK_b})}{d(\log \omega)} = -1$, is the local slope. $\Rightarrow \frac{MK_a}{MK_b} = 2$

so, $G_c(s) = 2 \cdot \frac{(\frac{1}{1.5}s+1)}{(\frac{1}{3}s+1)} \cdot \frac{(\frac{1}{10}s+1)}{(\frac{1}{5}s+1)^2} \cdot \frac{(\frac{1}{100}s+1)}{(\frac{1}{200}s+1)}$

2. (10 points) Consider the unity negative feedback loop with plant

$$G_p(s) = \frac{1}{s(s+8)}$$

Design a Lead Compensator $G_c(s)$ such that the closed-loop system has a pair of poles at $s = -2$.

solution: ① if we can use pole cancellation, $G_c(s) = K \frac{s+8}{s+p}$. then

$$\begin{aligned} 1 + G_c(s)G_p(s) &= 1 + K \frac{s+8}{s+p} \cdot \frac{1}{s(s+8)} \\ &= 1 + K \frac{1}{(s+p)s} \end{aligned}$$

Characteristic polynomial is $s^2 + ps + K$

matching $(s+2)^2 = s^2 + 4s + 4$, we have $K=4$, $p=4$. but $p=4 < 8=8$

rule out

② consider the case there is no pole cancellation, the characteristic polynomial will be 3rd order.

$$1 + G_c(s)G_p(s) = 1 + K \frac{s+z}{s+p} \cdot \frac{1}{s(s+8)}$$

$$\begin{aligned} \text{char. poly.} &= s(s+8)(s+p) + K(s+z) \\ &= s^3 + (8+p)s^2 + (8p+K)s + Kz \end{aligned}$$

$$\begin{aligned} \text{desired char. poly} &= (s+2)^2(s-\alpha) \quad (\alpha \in \mathbb{R}) \\ &= s^3 + (4-\alpha)s^2 + (4-4\alpha)s - 4\alpha \end{aligned}$$

$$\text{matching coefficients, } \left\{ \begin{array}{l} 8+p = 4-\alpha \Rightarrow p = -4-\alpha > 0 \\ 8p+K = 4-4\alpha \Rightarrow K = 36+4\alpha > 0 \\ Kz = -4\alpha \Rightarrow z = \frac{-4\alpha}{36+4\alpha} > 0 \end{array} \right.$$

and lead compensator requires

$$z = \frac{-4\alpha}{36+4\alpha} < -4-\alpha = p$$

There is no such a lead compensator

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$$\Rightarrow \frac{4\alpha}{36+4\alpha} > \alpha+4$$

$$\Rightarrow 4\alpha > (\alpha+4)(36+4\alpha)$$

$$\Rightarrow \alpha^2 + 12\alpha + 36 < 0 \Rightarrow (\alpha+6)^2 < 0 \text{ impossible.}$$

for $\alpha \in \mathbb{R}$.

3. (10 points) Consider the following transfer function

$$G(s) = \frac{(s-4)^2}{(s^2+3s+2)(s-3)}$$

Sketch the root locus of $1 + KG(s)$. According to your root locus plot, is it possible to make $G(s)$ closed-loop stable using positive $K > 0$?

[Hint: 1. At some point, if you need to solve a cubic polynomial equation $s^3 - 12s^2 + 7s + 40 = 0$, you can use the fact that the roots are $s_1 \approx 11.0375$, $s_2 \approx 2.4449$, $s_3 \approx -1.4823$.

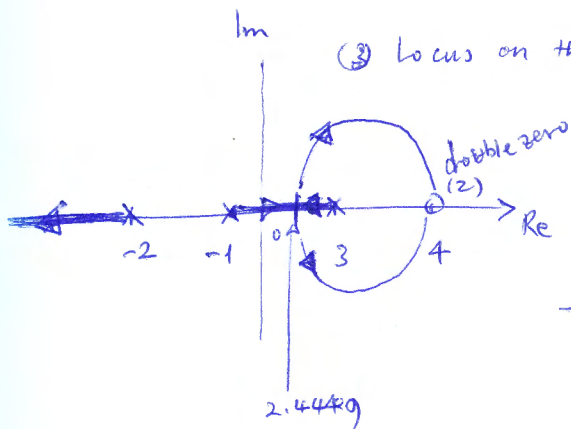
2. You do not have to justify the complex loci form a circle. As a take-home extra credit question, if you can show it actually **does not** form a circle, I will give you +3 points for this question. Take-home response is due 11:59 p.m. today.]

solution: (1) There are 3 open-loop poles

2 open-loop zeros

(2) Therefore one = $(3-2)$ branch of locus ends at infinity (must be real locus by symmetry)

(3) Locus on the real axis, $(-\infty, -2] \cup [-1, 3]$



(4) break point can be obtained from $\frac{d}{ds} G(s) = 0$

$$\frac{d}{ds} G(s) = \frac{-[(s+1)(s+2)(s-3)]'(s-4)^2 + (s+1)(s+2)(s-3) \cdot 2(s-4)}{(\cdot)^2} = 0$$

$$\Rightarrow (s-4) [(s-4)(3s^2-7) - 2(s^3-7s-6)] = 0$$

$$\Rightarrow (s-4)(s^3-12s^2+7s+40) = 0$$

$s_1 = 4,$	$s_2 = 11.0375,$	$s_3 = 2.4449,$	$s_4 = -1.4823$
↑	↑	↑	↑
break in point	not on the locus	break away point	not on the locus

(5) why it does not cross $j\omega$ -axis. Suppose it does,

at some point it has } one real pole ≤ -2
 } two complex poles in LHP \Rightarrow system is stable

but for any $K > 0$ the char. poly fails necessary condition for stability

$$(s^2+3s+2)(s-3) + K(s-4)^2 = s^3 - 7s - 6 + Ks^2 - 8Ks + 16K$$

$$= s^3 - \underbrace{(8K+7)}_{< 0} s^2 + Ks^2 + (16K-6)$$

There is always one RHP closed-loop pole.

4. (20 points) Recall from our lecture, it is known that for a double integrator $G(s) = \frac{1}{s^2}$ as our plant, a scalar control gain K cannot give a strictly stable closed-loop system in a unity negative feedback configuration. Indeed, when $K > 0$, the characteristic equation

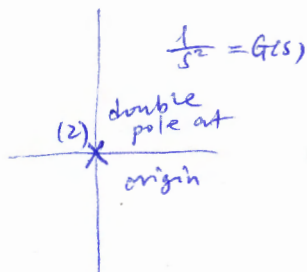
$$s^2 + K = 0$$

gives a pair of conjugate closed-loop poles on the imaginary axis; when $K < 0$, one of the closed-loop poles $s_{1,2} = \pm\sqrt{-K}$ is in the Right Half Plane (RHP). Hence in both cases the closed-loop system is not strictly stable.

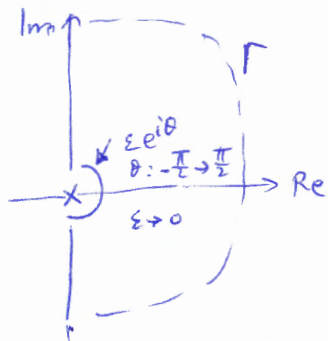
- (a) (10 points) Let $G(s) = \frac{1}{s^2}$ as in the above comment, now apply Nyquist Stability Criterion to $G(s)$ to confirm that there is a one RHP closed-loop pole if $K < 0$. Justify your reasoning.

[Hint: You can consider a modified contour γ to enclose the entire RHP. Remember γ cannot pass origin; so the usual contour—imaginary axis union large semicircular path does not work here.]

solution:



choose modified contour to avoid double pole $s=0$

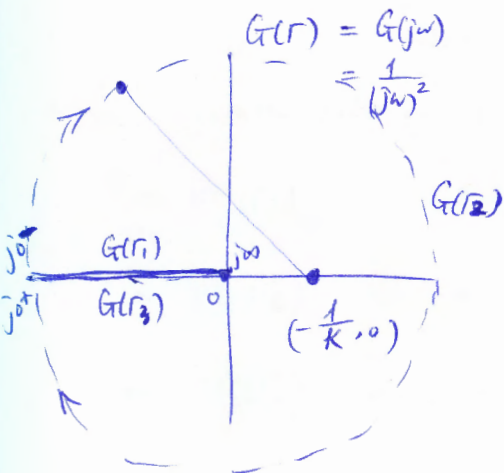


the Nyquist plot of $G(s) = \frac{1}{s^2}$ is the image curve $G(\Gamma)$ under $\frac{1}{s^2}$

$G(\Gamma)$ has three ^{excluding $G(\infty)=0$} components, since Γ has three components

$$\Gamma = \underbrace{[-\infty, +\epsilon e^{i(\frac{\pi}{2})}]}_{\Gamma_1} \cup \underbrace{[+\epsilon e^{i(-\frac{\pi}{2})}, +\epsilon e^{i(\frac{\pi}{2})}]}_{\Gamma_2} \cup \underbrace{[+\epsilon e^{i(\frac{\pi}{2})}, +\infty]}_{\Gamma_3}$$

path, not interval



$G(\Gamma_1)$ and $G(\Gamma_3)$ are negative real axis.

$G(\Gamma_2)$ forms a circular path with phase change

$$(-2) \cdot \left(\frac{\pi}{2} - \left(-\frac{\pi}{2}\right) \right) = -2\pi$$

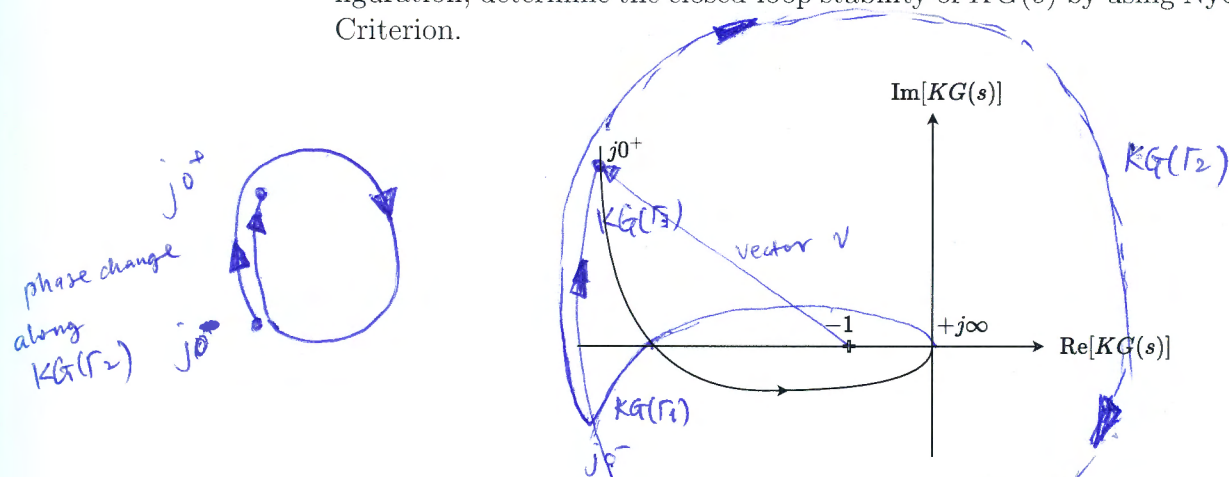
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so the clockwise encirclement around $(-\frac{1}{K}, 0)$ is $1 = N$
there is no open loop pole inside Γ . $P=0 \Rightarrow Z = N+P = 1$.

(b) (10 points) As a follow-up, consider the following forward path transfer function

$$KG(s) = \frac{K(\tau_1 s + 1)(\tau_2 s + 1)}{s^3},$$

where $K, \tau_1, \tau_2 > 0$ all positive. Part of the Nyquist plot of $KG(j\omega)$ is already given below for $\{s = j\omega \in \mathbb{C} \mid 0^+ \leq \omega \leq +\infty\}$. With unity *negative* feedback configuration, determine the closed-loop stability of $KG(s)$ by using Nyquist Stability Criterion.



Solution: similar to (a) choose modified contour to avoid triple pole at origin.

By the Nyquist plot of $KG(j\omega)$, we compute the encirclement about -1

$$\Gamma: \underbrace{(-\infty, +\varepsilon e^{i(-\frac{\pi}{2})})}_{\Gamma_1} \cup \underbrace{(+\varepsilon e^{i(-\frac{\pi}{2})}, +\varepsilon e^{i(\frac{\pi}{2})})}_{\Gamma_2} \cup \underbrace{(+\varepsilon e^{i(\frac{\pi}{2})}, +\infty)}_{\Gamma_3}$$

To complete the Nyquist plot, first take the conjugate of $KG(\Gamma_3)$ (given)

we get the portion corresponding to $KG(\Gamma_1)$. Then

$KG(\Gamma_2)$ corresponds to the large dashed circular path.

Join the point $(-1, 0)$ with a point on the Nyquist plot, say this is a vector v .

on $KG(\Gamma_3)$: $\omega: 0^+ \rightarrow +\infty$, net phase change of vector v is $+270^\circ$

on $KG(\Gamma_1)$: $\omega: -\infty \rightarrow 0^-$, net phase change of vector v is $+270^\circ$

on $KG(\Gamma_2)$: $\omega: 0^- \rightarrow 0^+$ along the path $\varepsilon e^{i(-\frac{\pi}{2})}$ to $\varepsilon e^{i(\frac{\pi}{2})}$. net phase change is $(-3) \left(\frac{\pi}{2} - (-\frac{\pi}{2}) \right) = -540^\circ$

so the encirclement (clockwise) about $(-1, 0)$ is $0 = N$

No open loop poles $\Rightarrow P=0$ so $Z = N + P = 0$, closed loop system is stable.