

ECE486: Control Systems

- ▶ **Lecture 11A:** Introduction to Root Locus design method

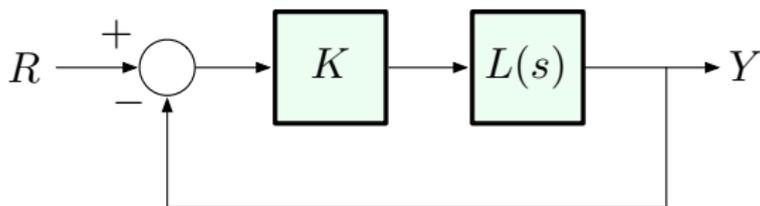
Goal: introduce the Root Locus method as a way of visualizing the locations of closed-loop poles of a given system as some parameter is varied.

Reading: FPE, Chapter 5

The Root Locus Design Method

(invented by Walter R. Evans in 1948)

Consider this unity feedback configuration:

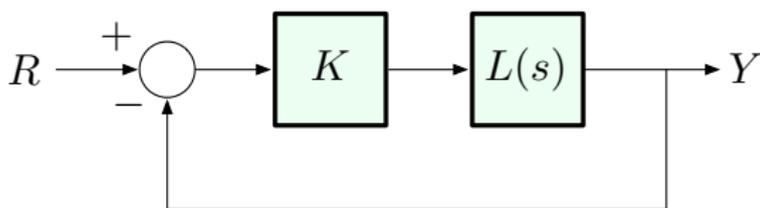


where

- ▶ K is a constant gain
- ▶ $L(s) = \frac{b(s)}{a(s)}$, where $a(s)$ and $b(s)$ are some polynomials

Problem: How to choose K to stabilize the closed-loop system?

The Root Locus Design Method



Closed-loop transfer function: $\frac{Y}{R} = \frac{KL(s)}{1 + KL(s)}$, $L(s) = \frac{b(s)}{a(s)}$

Closed loop poles are solutions of:

$$1 + KL(s) = 0 \quad \Leftrightarrow \quad L(s) = -\frac{1}{K}$$

$$\Updownarrow$$

$$1 + \frac{Kb(s)}{a(s)} = 0$$

$$\Updownarrow$$

$$\underbrace{a(s) + Kb(s)} = 0$$

characteristic
polynomial

characteristic equation

A Comment on Change of Notation

Note the change of notation:

$$\text{from } G(s) = \frac{q(s)}{p(s)} \quad \text{to } L(s) = \frac{b(s)}{a(s)}$$

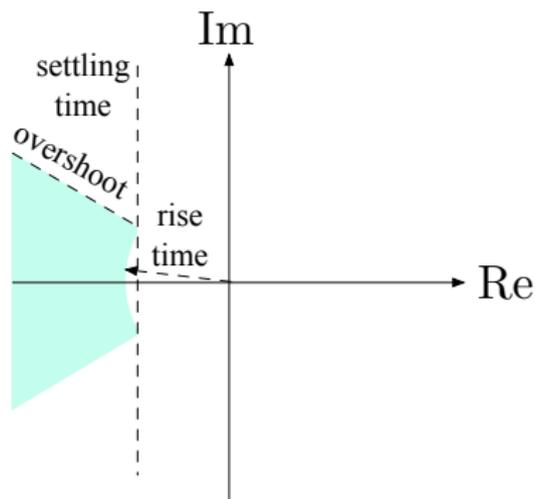
— the RL method is quite general, so $L(s)$ is not necessarily the *plant* transfer function, and K is not necessary *feedback gain* (could be *any parameter*).

E.g., $L(s)$ and K may be related to plant transfer function and feedback gain through some transformation.

As long as we can represent the poles of the closed-loop transfer function as roots of the equation $1 + KL(s) = 0$ for *some choice* of K and $L(s)$, we can apply the RL method.

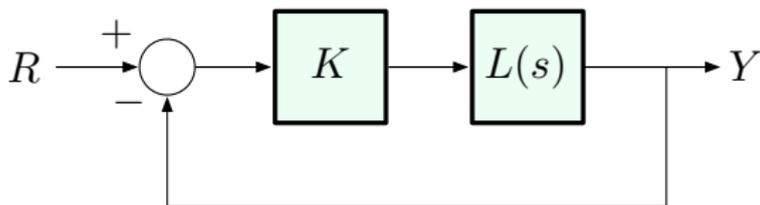
Towards Quantitative Characterization of Stability

Qualitative description of stability: Routh test gives us a range of K to guarantee stability.



For what values of K do we best satisfy given design specs?

Root Locus and Quantitative Stability



Closed-loop transfer function: $\frac{Y}{R} = \frac{KL(s)}{1 + KL(s)}$, $L(s) = \frac{b(s)}{a(s)}$

For what values of K do we best satisfy given design specs?

Specs are encoded in pole locations, so:

The *root locus* for $1 + KL(s)$ is the set of all closed-loop poles, i.e., the roots of

$$1 + KL(s) = 0,$$

as K varies from 0 to ∞ .

A Simple Example

$$L(s) = \frac{1}{s^2 + s} \quad b(s) = 1, \quad a(s) = s^2 + s$$

Characteristic equation: $a(s) + Kb(s) = 0$

$$s^2 + s + K = 0$$

Here, we can just use the quadratic formula:

$$s = -\frac{1 \pm \sqrt{1 - 4K}}{2} = -\frac{1}{2} \pm \frac{\sqrt{1 - 4K}}{2}$$

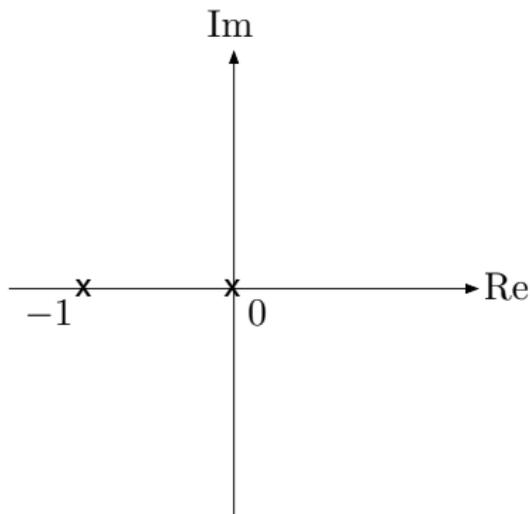
$$\text{Root locus} = \left\{ -\frac{1}{2} \pm \frac{\sqrt{1 - 4K}}{2} : 0 \leq K < \infty \right\} \subset \mathbb{C}$$

Example, continued

$$\text{Root locus} = \left\{ -\frac{1}{2} \pm \frac{\sqrt{1-4K}}{2} : 0 \leq K < \infty \right\} \subset \mathbb{C}$$

Let's plot it in the s -plane:

- ▶ start at $K = 0$ the roots are $-\frac{1}{2} \pm \frac{1}{2} \equiv -1, 0$
note: these are poles of L (open-loop poles)



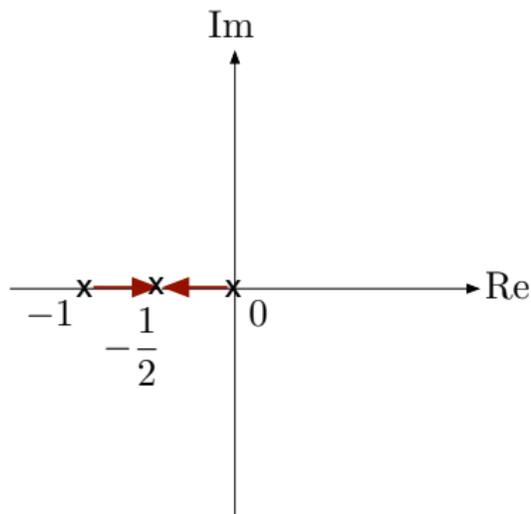
Example, continued

$$\text{Root locus: } \left\{ -\frac{1}{2} \pm \frac{\sqrt{1-4K}}{2} : 0 \leq K < \infty \right\} \subset \mathbb{C}$$

► as K increases from 0, the poles start to move

$$1 - 4K > 0 \quad \implies \quad 2 \text{ real roots}$$

$$K = 1/4 \quad \implies \quad 1 \text{ real root } s = -1/2$$

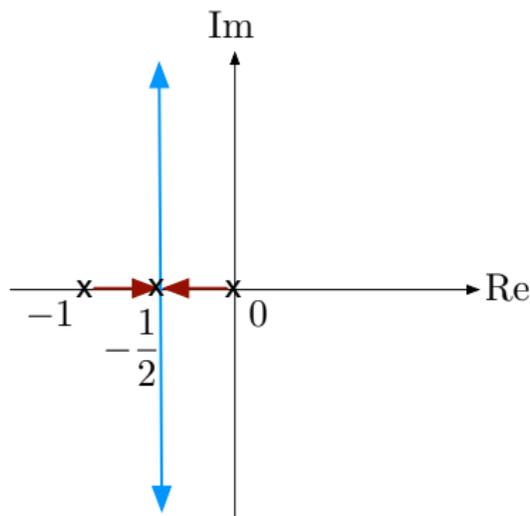


Example, continued

$$\text{Root locus: } \left\{ -\frac{1}{2} \pm \frac{\sqrt{1-4K}}{2} : 0 \leq K < \infty \right\} \subset \mathbb{C}$$

► as K increases from 0, the poles start to move

$$K > 1/4 \quad \implies \quad 2 \text{ complex roots with } \operatorname{Re}(s) = -1/2$$



($s = -1/2$ is the *point of breakaway* from the real axis)

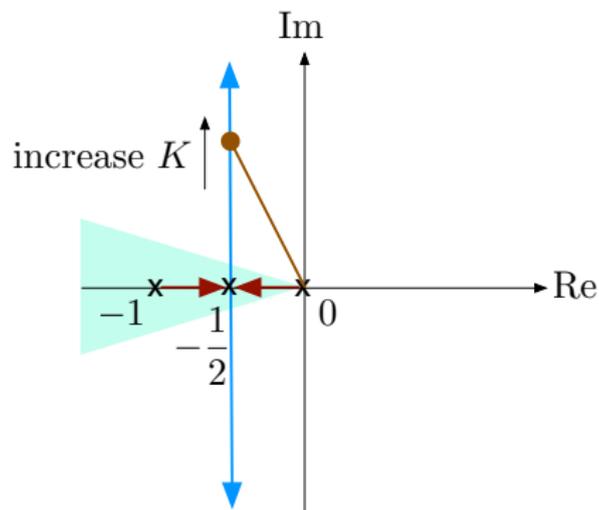
Example, continued

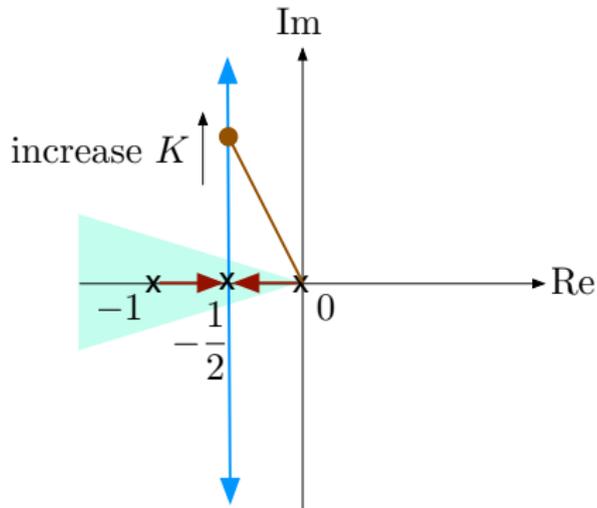
Compare this to admissible regions for given specs:

$$t_s \approx \frac{3}{\sigma} \quad \text{want } \sigma \text{ large, can only have } \sigma = \frac{1}{2} \quad (t_s = 6)$$

$$t_r \approx \frac{1.8}{\omega_n} \quad \text{want } \omega_n \text{ large} \implies \text{want } K \text{ large}$$

$$M_p \quad \text{want to be inside the shaded region} \implies \text{want } K \text{ small}$$





Thus, the root locus helps us *visualize the trade-off* between all the specs in terms of K .

However, for order > 2 , there will generally be no direct formula for the closed-loop poles as a function of K .

Our goal: develop simple rules for (approximately) sketching the root locus in the general case.