## Q1. (30 points):

A balanced, 3-phase, 60 HZ, 3-wire, impedance load is served by a balanced, 3-phase, 3-wire, ABC sequence source. A voltmeter between two lines reads 275 Volts. An ammeter in one line reads 13 Amps. A wattmeter connected to read the power "into" the A-B lines reads 1650 Watts.

- a. Find the power factor of the load.
- b. Find the total 3-phase real power absorbed by the load.
- c. A capacitor bank is used to correct the load power factor to unity. Compute the power readings in the two wattmeter method.
- d. Draw a schematic showing how a wattmeter can be used to 'measure' the reactive power consumed by the balanced 3-phase load, with appropriate polarity markings on the voltage and current measurements.

$$\begin{array}{lll}
Q. & V_{LL} = 15 \text{ A} \\
P_1 = V_{LL} I_L \cos(6 + 30^\circ) = 1650 \\
& \cos(6 + 30^\circ) = \frac{1650}{125 \times 13} = 0.4615 \implies 67.51^\circ \\
\theta = 32.51^\circ \\
P_2 = \cos(6) = \boxed{0.8433} \\
b. & P_3 \phi = \sqrt{3} V_{LL} I_L \cos(6) = \sqrt{3} \times 275 \times 13 \times 0.8433 \\
& = \boxed{5.222} \text{ W}$$

$$6 & C. & \theta = 0. & P_1 = P_2 = V_{LL} I_L \cos(30^\circ) = \frac{P_3 \phi}{2} = \boxed{2611} \text{ W}$$

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$$C_{3} \phi = \sqrt{3} P_{WM}$$

## Q2. (35 points):

The following test results were found for a single-phase 60 HZ 30 KVA transformer with voltage ratings 4160/480 Volts:

Open-circuit test:  $V_L = 480 \text{ V}$ ,  $I_L = 4 \text{ A}$ ,  $P_2 = 380 \text{ W}$ Short-circuit test:  $V_H = 142 \text{ V}$ ,  $I_H = 7.2 \text{ A}$ ,  $P_1 = 440 \text{W}$ 

- (a) Compute all the parameters of the approximate equivalent circuit with the shunt elements moved directly across the source.
- (b) Draw the approximate equivalent circuit and label all impedances with per unit values.
- (c) Find the high side voltage when the transformer is delivering rated kVA at 0.87 lagging power factor to a load on the low voltage side with a 480V across the load.

$$R_{Q_{1}} = \frac{V_{1}^{2}}{P_{2}} = |606.3 \Omega \quad G_{0} = \sqrt{V_{123}^{2}} - P_{2}^{2} = \sqrt{(y_{0} + y_{1}^{2} - 38)^{2}} = 1882 \text{ VM} \times \text{M}_{12} = \frac{V_{1}^{2}}{Q_{0}} = 124.$$

$$R_{CH} = \frac{(u_{1} h)^{2}}{48} R_{CL} = \frac{9 (h_{1})^{2}}{16} R_{CL} = \frac{455 40 \Omega}{12} \times \text{M}_{12} + \frac{(u_{1} h)^{2}}{49} N_{12} = \frac{913.6 \Omega}{12}$$

$$P_{0}f_{1H} = \frac{P_{1}}{P_{1}} = \frac{P_{1} 428 \Omega}{12} \Omega \quad G_{1} = \sqrt{V_{11} H_{1}^{2}} - P_{1}^{2} = 922.9 \text{ Var} \times x_{02.4} = \frac{2}{14} = \frac{17.80 \Omega}{12}$$

$$R_{C,p_{1}} = \frac{R_{CH}}{2H_{1} hae} = \frac{178.9}{30 \times 10^{3}} \times \frac{2}{16} N_{1} + \frac{15.9}{2H_{1} hae} = \frac{15.9}{15.9}$$

$$R_{0}p_{1} = \frac{R_{CE} H}{2H_{1} hae} = \frac{19.9}{24.30} \times \frac{12.9}{12} \times \frac{15.9}{24.30} = \frac{10.938}{12}$$

$$V_{1} = \frac{1220^{\circ}}{12} \quad \theta = arcos_{1}(a_{1}) - 28.54^{\circ} = 0.87 - j_{0}.493$$

$$V_{1}p_{1} = V_{2}p_{1} + (R_{0}, p_{1} + 1) \times s_{2}p_{1}) \cdot \overline{I}_{2}, p_{1}} = 1 + (0.0147 + j_{1} = 0.308) \cdot (0.87 - j_{0}.493)$$

$$= 1.02797 + j_{1} = 0.9185 = 1.0282 \times 1.089^{\circ} \quad |V_{1}| = 1.0282 \times (468 = |u_{1}|^{2}) \times |V_{1}|$$

Q4. (35 points)

8/6

A reluctance machine with a 6/4 configuration has the following parameters.

> Rotor outer radius = 6 cm Air gap, g = 1mmRotor pole angle =  $\pi/6$  radians stator pole angle =  $\pi/8$  radians Axial length = 10 cm

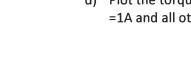
Number of total turns per phase = 40 Assume rotor and stator cores have extremely high permeability. Assume infinite reluctance when there is no stator/rotor pole overlap. Ignore saturation and fringing flux.

- a) Starting from the position shown, what should the sequence of excitation be to obtain a clockwise rotation?
- b) How fast would the rotor spin (in revolutions per minute) if single phase excitation is applied at the rate of one pulse per millisecond?

STATOR

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- c) Plot the phase-A inductance as a function of rotor position  $\theta$ , as the rotor is rotated clockwise from  $\theta$ =0 to  $\theta$ =60 degrees.
- d) Plot the torque as the rotor is rotated clockwise from  $\theta$ =0 to  $\theta$ =60 degrees with Phase A current =1A and all other currents set to zero.



(a) A - B - C - D

(b) | pulse/ms = 1 step/ms ≥ fs = 1000 steps/sec S = mNr = 6 × 4 = 24 steps/rev

reluctions. 
$$R_g = \frac{2g}{\mu_0 \cdot (\alpha RD)}$$
  $2my = \frac{N_{ph}^2}{R_g} = \frac{\mu_0 \cdot \alpha RD N_{ph}^2}{2g} = \frac{1.256 k \times 10^{-3} \times 0.06 \times \alpha \log \times 40^{-2}}{2 \times 1 \times 10^{-3}} = \frac{2.369 \text{ m}}{2 \times 1 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 1 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 1 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 1 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 1 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-2}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3} \times 10^{-3}}{2 \times 10^{-3}} = \frac{1.256 k \times 10^{-3}}{2 \times 10^{-3}} = \frac$