

## Exam I Solutions

Spring 1991

#1 (a)  $|\bar{S}_{3\phi}| = \sqrt{3} \times 200 \times 10 = 2000\sqrt{3} \text{ VA}$

$$\angle \bar{S}_{3\phi} = +\cos^{-1} 0.8 = +36.87^\circ \quad \bar{S}_{3\phi} = P_{3\phi} + jQ_{3\phi}$$

$$Q_{3\phi} = 2000\sqrt{3} \sin 36.87^\circ = 1200\sqrt{3} \quad Q_{1\phi} = 400\sqrt{3}$$

Each capacitor must supply  $Q_{1\phi}$  so:  $400\sqrt{3} = 200^2 \times 2\pi 60 C$

$$C = 45.9 \mu\text{F}$$

(b) At unity power factor,  $|\bar{S}_{3\phi}| = P_{3\phi} = 2000\sqrt{3} \times 0.8$

$$|\bar{I}| = \frac{1600\sqrt{3}}{\sqrt{3} \times 200} = 8 \text{ A}$$

#2 (a)  $|\bar{Z}_{02}| = \frac{5}{83.3} = .06 \Omega \quad V_{2 \text{ rated}} = 120 \text{ V} \quad I_{2 \text{ rated}} = 83.3 \text{ A}$

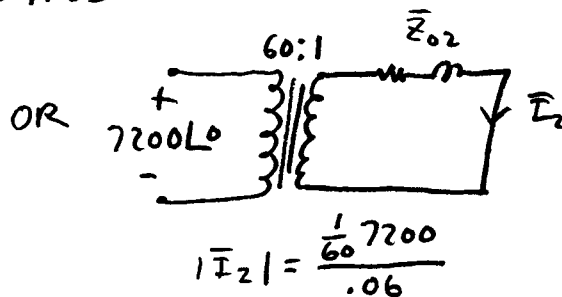
$$\% Z = \frac{.06}{120/83.3} \times 100$$

$$\% Z = 4.165$$

(b)  $I_{2 \text{ rated}} = 83.3 \text{ A} \quad \frac{\% Z}{100} = .04165$

$$|\bar{I}_{2 \text{ SC}}| = \frac{83.3}{.04165} = 2000 \text{ A}$$

rated voltage



#3 Using rated hp. as full load,

$$T_{FL} = \frac{2 \times 746}{1180 \frac{2\pi}{60}} = 12.07 \text{ NM}$$

$$s_{FL} = \frac{1200 - 1180}{1200} = .01667$$

Estimate using linear  $T$  vs slip  $T_{FL} \approx \frac{3 \times (\frac{230}{\sqrt{3}})^2 \cdot .01667}{\frac{2\pi 60}{3} r_r'} \stackrel{\text{must}}{=} 12.07$

This gives  $r_r' \approx .58 \Omega$

$$P_{\text{rotor start}} = 3 \times |\bar{I}_r'|^2 r_r' \quad (s=1)$$

$$T_{\text{start}} = \frac{3 \times |\bar{I}_r'|^2 \cdot .58}{\frac{2\pi 60}{3}} \stackrel{\text{must}}{=} 8$$

$$|\bar{I}_r'| = 24 \text{ A}$$

$$\text{Estimate } |\bar{I}_{as}| \approx |\bar{I}_r'| \approx 24 \text{ A}$$

#4 when supply phase sequence is reversed  $s = \frac{1200 - (-1200)}{1200} = 2$

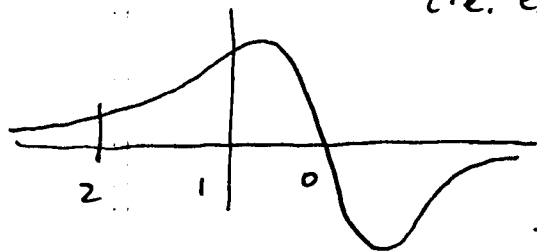
(a) A crude estimate would neglect everything except  $r_r'$

$$\frac{230}{\sqrt{3}} \angle 0^\circ \Rightarrow |\bar{I}_{as}|_{\text{reversal}} = \frac{230/\sqrt{3}}{0.7/2} = 379 \text{ A}$$

$$T_{\text{shaft reversal}} = \frac{3 \times (\frac{230}{\sqrt{3}})^2 \times 2}{(\frac{2\pi 60}{3}) 0.7} = 1200 \text{ NM}$$

(b) These are both very high estimates. The actual current and torque would be limited by  $r_s$   $X_{ls}$   $X_{lr}'$

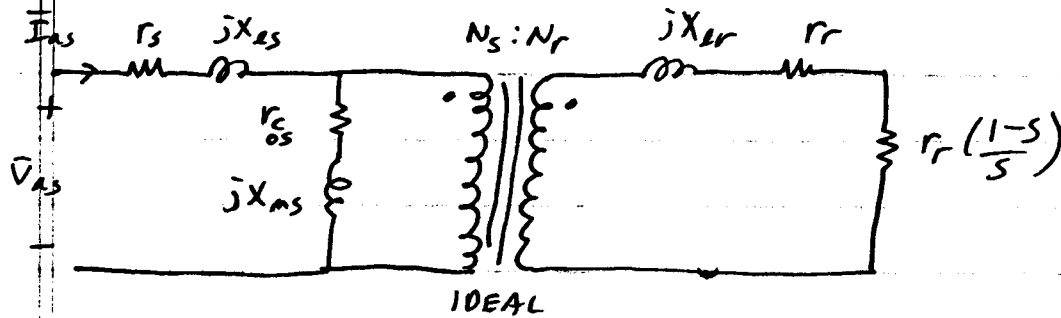
i.e. estimate  $r_s \approx 0.7$   $X_{ls} \approx X_{lr}' \approx 1 \Omega$  (about same as  $r_r'$  at least)



$$|\bar{I}_{as}| = \frac{230/\sqrt{3}}{\sqrt{(0.7 + \frac{0.7}{2})^2 + 2^2}} = 58 \text{ A}$$

$$T_{\text{shaft reversal}} = \frac{3 \times 58^2 \times (0.7)}{\frac{2\pi 60}{3}} = 28 \text{ NM}$$

(Probably still too high)



$$f_r = s f_s \quad s = \frac{RPM_{sync} - RPM_{shaft}}{RPM_{sync}} \quad P = \# \text{ poles / phase}$$

$$T_{TO_{shaft}} = \frac{P_{TO_{shaft}}}{\omega_{shaft}} = \frac{P_{TO_{rotor}}}{\omega_s} \approx \frac{3 |\bar{V}_{as}|^2 r_r' s}{\omega_s [(s r_s + r_r')^2 + s^2 (X_{es} + X_{er}')^2]} \quad \left( \begin{array}{l} \text{neglects} \\ r_{cos} + jX_{ms} \end{array} \right)$$

↑  
m.r./s.

$$S_{max} \approx \frac{r_r'}{\sqrt{r_s^2 + (X_{es} + X_{er}')^2}} \quad T_{max} \approx \frac{\frac{3}{2} |\bar{V}_{as}|^2}{\omega_s [r_s + \sqrt{r_s^2 + (X_{er}' + X_{es})^2}]} \quad \left( \begin{array}{l} \text{neglects} \\ r_{cos} + jX_{ms} \end{array} \right)$$

$$RPM_{\text{stator mmf w.r.t. stator}} = \frac{120 f_s}{P} = RPM_{sync}$$

$$RPM_{\text{rotor mmf w.r.t. rotor}} = \frac{120 f_r}{P}$$

$$\% Z = \frac{|\bar{Z}_{01}|}{V_{rated}/I_{rated}} \times 100$$

$$\% VR = \frac{|\bar{V}_{load_{NL}}| - |\bar{V}_{load_{FL}}|}{|\bar{V}_{load_{FL}}|} \times 100 \quad \left. \begin{array}{l} \text{with} \\ |\bar{V}_{source}| \\ \text{fixed} \end{array} \right\}$$

$$RPM_{\text{rotor mmf w.r.t. stator}} = RPM_{\text{rotor mmf w.r.t. rotor}} + RPM_{shaft} = \frac{120 f_r}{P} + RPM_{shaft}$$

$$= \frac{120 s f_s}{P} + RPM_{shaft} = \left( \frac{RPM_{sync} - RPM_{shaft}}{RPM_{sync}} \right) RPM_{sync} - RPM_{shaft}$$

$$= RPM_{sync}$$