## The Battery Disconnect Unit

• A junction box assembly:



### **Contactor Function**

- Contactors connect and disconnect the HV battery to the DC HV Bus (often called the Link), under normal operating conditions.
- Contactors are expected to ride through an electrically abusive event (stay closed), and allow the associated fuse to activate.
  - The contactor is not necessarily expected to be fully functional after the event.
- The contactors must be sized for adequate voltage tolerance, per HV systems standards.
- Under normal operation the contactors must be able to handle the following currents over the full design life of the system:
  - Full DC RMS operating current (unlimited time).
  - Continuous current for top speed and fast charge (30 minutes).
  - Peak discharge and charge currents (1 & 10s).

# Fuse Sizing

- A battery will contain a main fuse, which is intended to break the main circuit, in the event of a two-point isolation failure, inside the pack.
- Between the BDU and the PIM, an additional (driveline) fuse may be desired, in order to ensure HV protection at the battery HV connector.
- The fuse rating must be selected so it will survive the total useful life of the battery and activate at a level below where the battery cells will be damaged.



#### Safety design of short circuit protection is needed

#### First cell venting :

- This safety concept is based on gas flow management inside an airtight pack : pack pressure increases (due to cell thermal runaway) and is released only through pack venting valves. No explosion, no fire before a required duration time.

- Two main risks have to be covered : Hot gas temperature & electrical short circuits/arcing.



- Cells with high energy density allow higher vehicle range but are more sensitive/reactive to thermal runaway, increasing thermal propagation risk :

- LFP (450Wh/l) < NCM622 (540Wh/l) < NCM811 (620Wh/l)

- A bigger cell size will generate higher quantity of gas to be managed : Gas volume = f(cell capacity)
- Some counter-measures are available but to the detriment of weight, volume, range and vehicle cost.
- **Regulatory constraints** will need to be accommodated in coming years : **Increased duration** before any user hazard, thermal propagation test **in parking mode** for example.

#### Propagation to neighbor cells :



- Assume a 60Ah cell. It is LFP/C chemistry, so has a nominal voltage of 3.25V, and operates between 3.7V and 2.5V. Assume it has a nominal discharge resistance of 1mohm and has a specific energy of 160Wh/kg.
- Determine the maximum power this cell can deliver, if fully charged.
- 1. We assume  $P_{max}$  is at  $V_{max}/2$ ;  $V_{max} = 3.7V$ , so  $P_{max} @ 3.7/2=1.85V = V_{load}$
- 2.  $P_{cell} = V_{load} \times (V_{max} V_{load}) / R_{cell} = 1.85 \times (3.7 1.85) / (1mohm/1000mohm/ohm) = 3,423W or 3.42kW$
- Compare this to a NMC/C cell, that operates between 4.2V and 2.8V:
- 1.  $V_{load} = 4.2/2 = 2.1V$
- 2.  $P_{cell} = 2.1 \text{ x} (4.2-2.1)/(1/1000) = 4,410 \text{W} \text{ or } 4.41 \text{kW}$



- What would the equivalent C-rate be, for the LFP/C cell?
- 1. I = P/V = 3,423W/2.1V = 1,630A
- 2. 1,630A/60Ah = 27C
- How much heat would be generated by the cell?
- 1.  $P_{heat} = I^2 \times R = (1,630A)^2 \times 1mohm/1000mohm/ohm = 2,657W = 2.7kW$
- If the cell was to discharge at the rate shown how heat energy would be generated?
- 1. 60Ah/1,630A = 0.37h = 133s
- 2. 2.7kW x 133s = 358kJ
- What would be the adiabatic temperature rise, if the cell had a specific heat capacity of 1.5kJ/kg\*K?
- 1. Cell weight is 60Ah x 3.25V/160Wh/kg = 1.22kg
- 2. Temperature rise = 358kJ/(1.5kJ/kg\*K x 1.22kg) = 196K (or °C)
- What do you suspect would be the cell failure mode?
- 1. Separator melt, electrolyte flashpoint, and possible phosphate decomposition.

- If the anode were to react and combust how much energy could it produce in this cell?
- 1. 60Ah x 3.25V = 195Wh x 3600J/Wh = 702kJ
- 2. 702kJ/4.9kJ/g for  $Li_6C = 143g$  anode
- 3. 63.6kJ/g anode combustion x 143g = 9,095kJ combustion energy
- Why would this be unlikely to happen in this particular cell?
- 1. The chemistry is LFP/C, and oxygen is not liberated by the cathode, so this particular reaction will not happen.
- If we would want to prevent the initial cell to go into thermal runaway what is the safe temperature threshold you think should be maintained?
- 1. Looking at the reactions temperature table: 85°C to 130°C.
- Assume the cell is a prismatic can 220mm wide x 102mm high x 22mm thick, not accounting for terminals, what would the bulk heat transfer coefficient (W/m<sup>2</sup>\*K)need to be to hold this temperature?
- 1. Use 130°C for this case. Assume 25°C ambient = 105°C Trise.
- 2. Area of cell is 220 x 102 x 2 + 102x22 x 2 + 220x22 x 2 = 193,511 mm<sup>2</sup> or 0.194 m<sup>2</sup>
- 3. 2.7kW heat generation, so HTC =  $2700W/(0.194m2 \times 105K) = 133W/m^{2*}K$

- Calculate the minimum DC isolation resistance for a 76V system. For a 920V system.
- 1. (76V+1000V) x 500ohm/V = 538kohm
- 2. (920V + 1000V) x 500ohm/V = 960kohm
- A thermal fuse is used to prevent excessive currents from leading to thermal events within the high-power systems.
- Use the fuse table to determine what minimum amperage rating should be used to protect the cell from a 2s maximum power short.
- 1. 1,630A is a 200A rated fuse.

