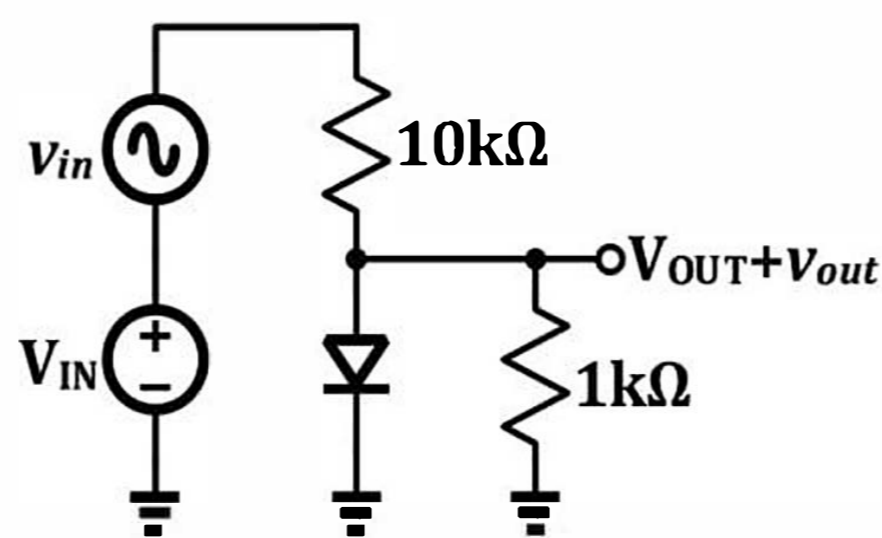


1. Consider the circuit shown in the figure below. Assume $V_T=25\text{mV}$, $V_{IN}=10\text{V}$, $v_{in}=0.1\text{V}$.
- Using constant voltage model for the diode with $V_{D0}=0.7\text{V}$, compute diode current, I_{D0} , and its incremental resistance, r_d .
 - Sketch incremental model and calculate amplitude of the incremental output voltage, v_{out1} , and incremental diode current, i_{d1} .
 - Recompute incremental diode current, i_{d2} , by including the second order term in the Taylor series expansion of diode current (you may use v_{out1} as incremental output voltage). Recompute new incremental output voltage, v_{out2} , using the newly calculated incremental diode current, i_{d2} . Calculate error voltage, $v_e = v_{out1} - v_{out2}$.
 - Repeat parts (b) and (c) for $v_{in} = 5\text{V}$.

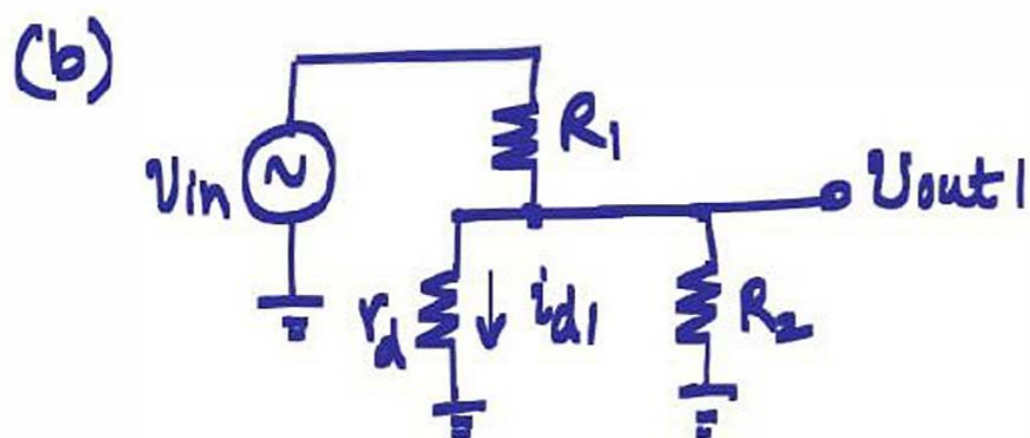


$$(a) \quad I_{R1} = \frac{V_{IN} - V_{D0}}{R_1} = \frac{10 - 0.7}{10\text{k}} = 0.93\text{mA}$$

$$I_{R2} = \frac{V_{D0}}{R_2} = \frac{0.7}{1\text{k}} = 0.7\text{mA}$$

$$I_{D0} = I_{R1} - I_{R2} \Rightarrow I_{D0} = 0.23\text{mA}$$

$$r_d = \frac{V_T}{I_{D0}} = \frac{25\text{mV}}{0.23\text{mA}} \Rightarrow r_d = 108.7\ \Omega$$



$$v_{out1} = v_{in} \cdot \frac{r_d \parallel R_2}{R_1 + r_d \parallel R_2}$$

$$\Rightarrow v_{out1} = 970\ \mu\text{V}$$

$$i_{d1} = \frac{v_{out1}}{r_d} \Rightarrow i_{d1} = 8.92\ \mu\text{A}$$

(c) Second term in the Taylor series is equal to :

$$\Delta i_{d2} = \frac{1}{2} \frac{d^2 I_D}{dV_D^2} \cdot (V_{D0} + \Delta V_D - V_{D0})^2 = \frac{1}{2} \cdot \frac{I_D}{V_T^2} \cdot \exp\left(\frac{V_{D0}}{V_T}\right) \cdot \Delta V_D^2$$

$$\Rightarrow \Delta i_{d2} \approx \frac{1}{2} \cdot \frac{I_{D0}}{V_T^2} \cdot \Delta V_D^2$$

$$\text{Using } \Delta V_D = V_{out1} : \Delta i_{d2} = \frac{1}{2} \cdot \frac{0.25 \text{ mA}}{(25 \text{ mV})^2} \cdot (970 \mu\text{V})^2 = 0.173 \mu\text{A}$$

$$i_{d2} = i_{d1} + \Delta i_{d2} \Rightarrow i_{d2} = 9.093 \mu\text{A}$$

$$V_{out2} = i_{d2} \times r_d \Rightarrow V_{out2} = 988.41 \mu\text{V} \Rightarrow \text{Assuming } r_d \text{ is constant}$$

$$V_e = V_{out2} - V_{out1} \Rightarrow V_e = 18.4 \mu\text{V} = 1.9\%$$

(d) Since V_{IN} (& operating point) did not change, r_d remains unchanged

$$V_{out1} = \frac{5 \times 98}{10\text{k} + 98} \Rightarrow V_{out1} = 48.5 \text{ mV}$$

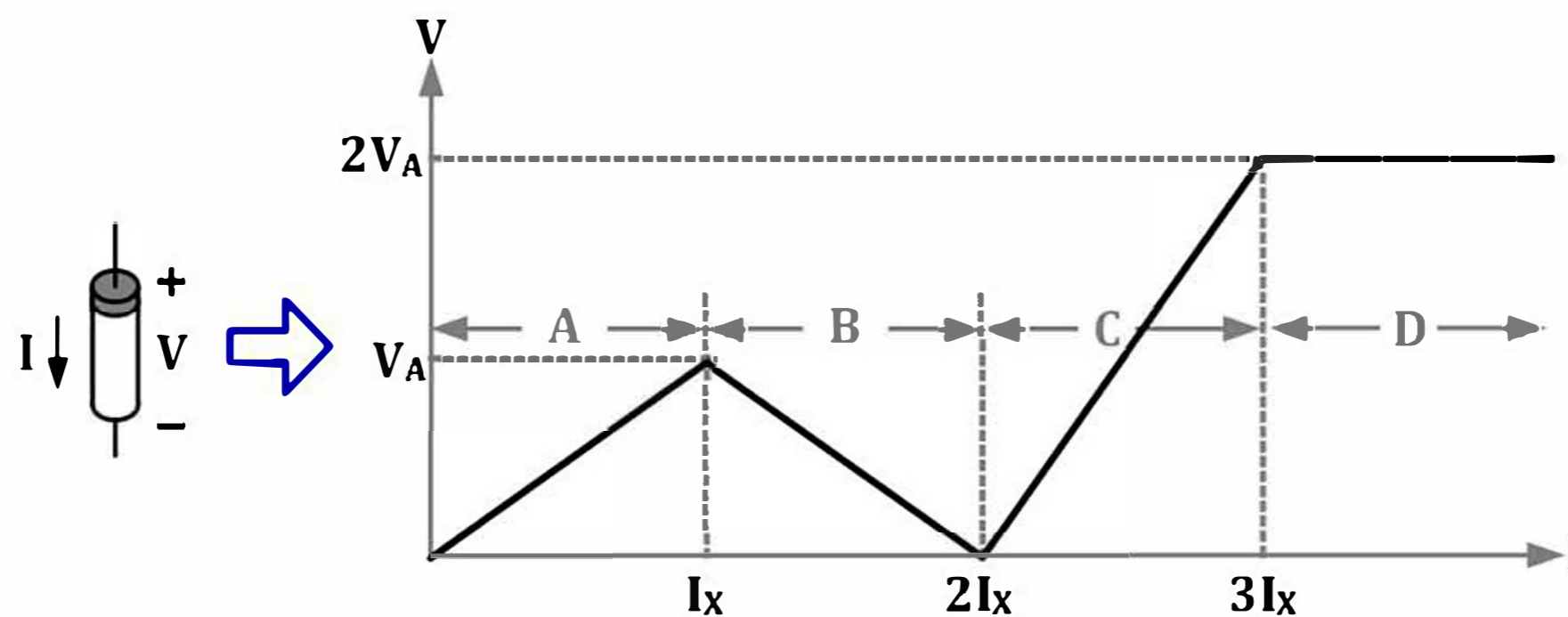
$$i_{d1} = \frac{V_{out1}}{r_d} \Rightarrow i_{d1} = 446 \mu\text{A}$$

$$\Delta i_{d2} = 432.8 \mu\text{A} \Rightarrow i_{d2} = 878.8 \mu\text{A}$$

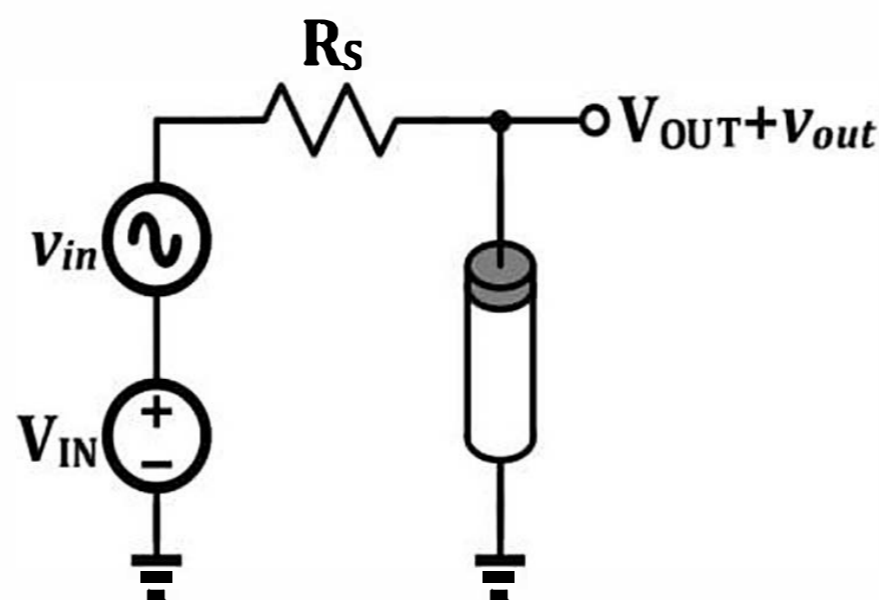
$$V_{out2} = i_{d2} \times r_d \Rightarrow V_{out2} = 95.5 \text{ mV}$$

$$V_e = V_{out2} - V_{out1} \Rightarrow V_e = 47 \text{ mV} = 97\%$$

2. Consider a device whose I-V characteristic is shown below:



- Find “incremental resistance” of the device in all regions of operation.
- Sketch the incremental model of the circuit shown below.



- Determine the region (A, B, C, or D) in which the device should be operated to maximize incremental gain, $A_v = \left| \frac{v_{out}}{v_{in}} \right|$.
- Compute the error in incremental voltage, v_{out} , (in regions A, B and C) if the second order term is included in the Taylor series expansion. Explain your answer.

(a) $r = \frac{dV}{dI}$ in regim A: $\frac{V_A}{I_x}$
in regim B: $-\frac{V_A}{I_x}$
in regim C: $\frac{2V_A}{I_x}$
in regim D: 0

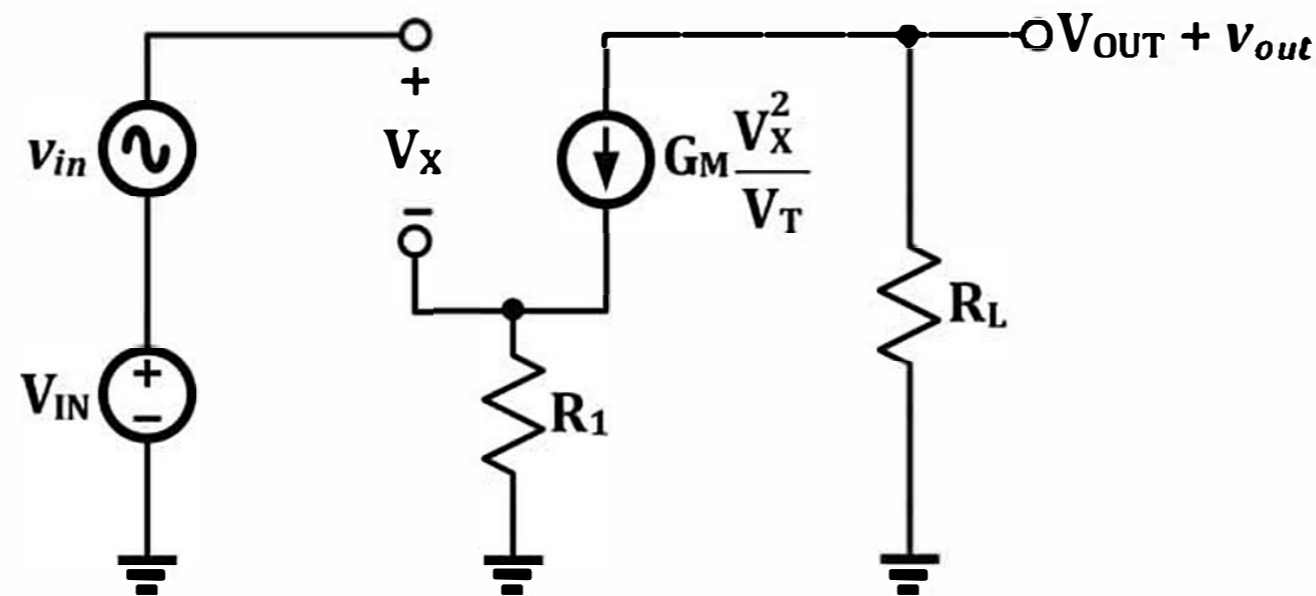
(b)

(c) $v_{out} = \frac{r}{R+r} \cdot v_{in}$
 $\Rightarrow A_v = \frac{r}{R+r}$ is maximum when r is negative

\Rightarrow The device must be biased in region B

(d) Error is zero because of piecewise linear V-I characteristics

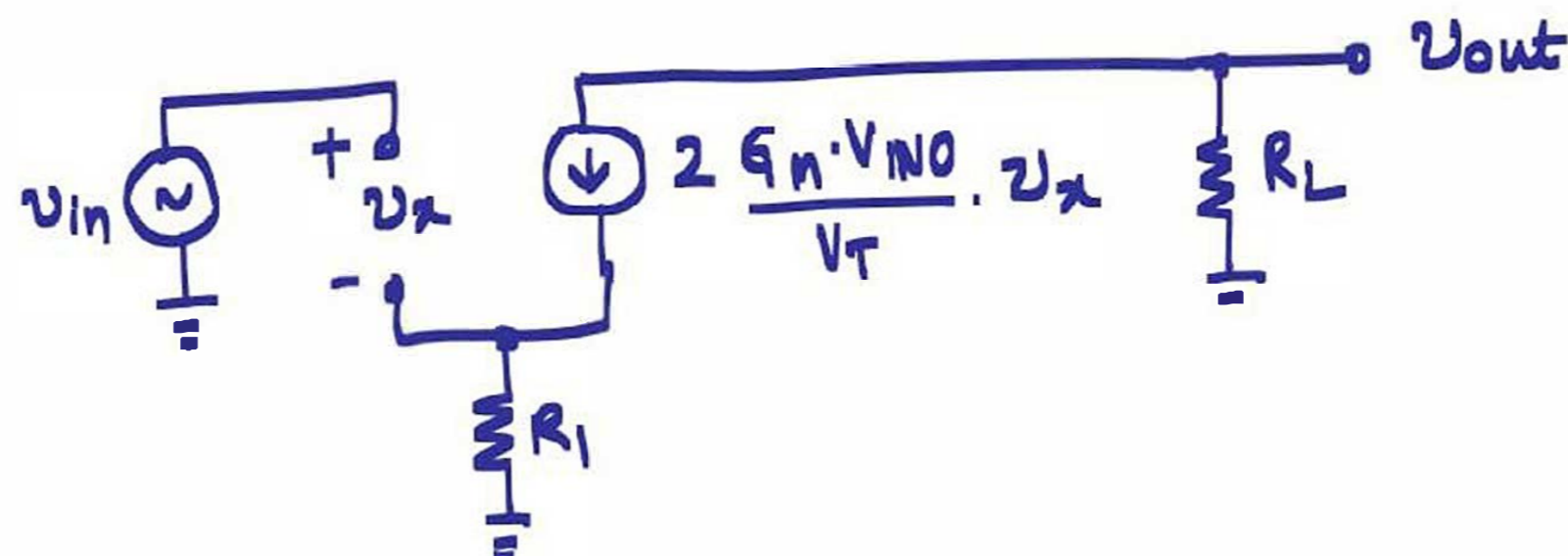
3. Consider the circuit that uses a non-linear voltage controlled current source shown below.



- Draw incremental model. Note V_T is a constant with units of Volts.
- Determine incremental output voltage, v_{out} , in terms of incremental input voltage, v_{in} , and circuit parameters, G_M , R_1 and R_L .
- What value of R_1 maximizes incremental gain, $A_v = \left| \frac{v_{out}}{v_{in}} \right|$.

$$(a) \quad I_x = f(v_x) = \frac{G_M \cdot v_x^2}{V_T} ; \quad f'(v_x) \Big|_{v_x = V_{INO}} = \frac{2 G_M \cdot V_{INO}}{V_T}$$

$$\Rightarrow I_x \approx \frac{G_M \cdot V_{INO}^2}{V_T} + \frac{2 G_M \cdot V_{INO}}{V_T} \cdot v_x$$



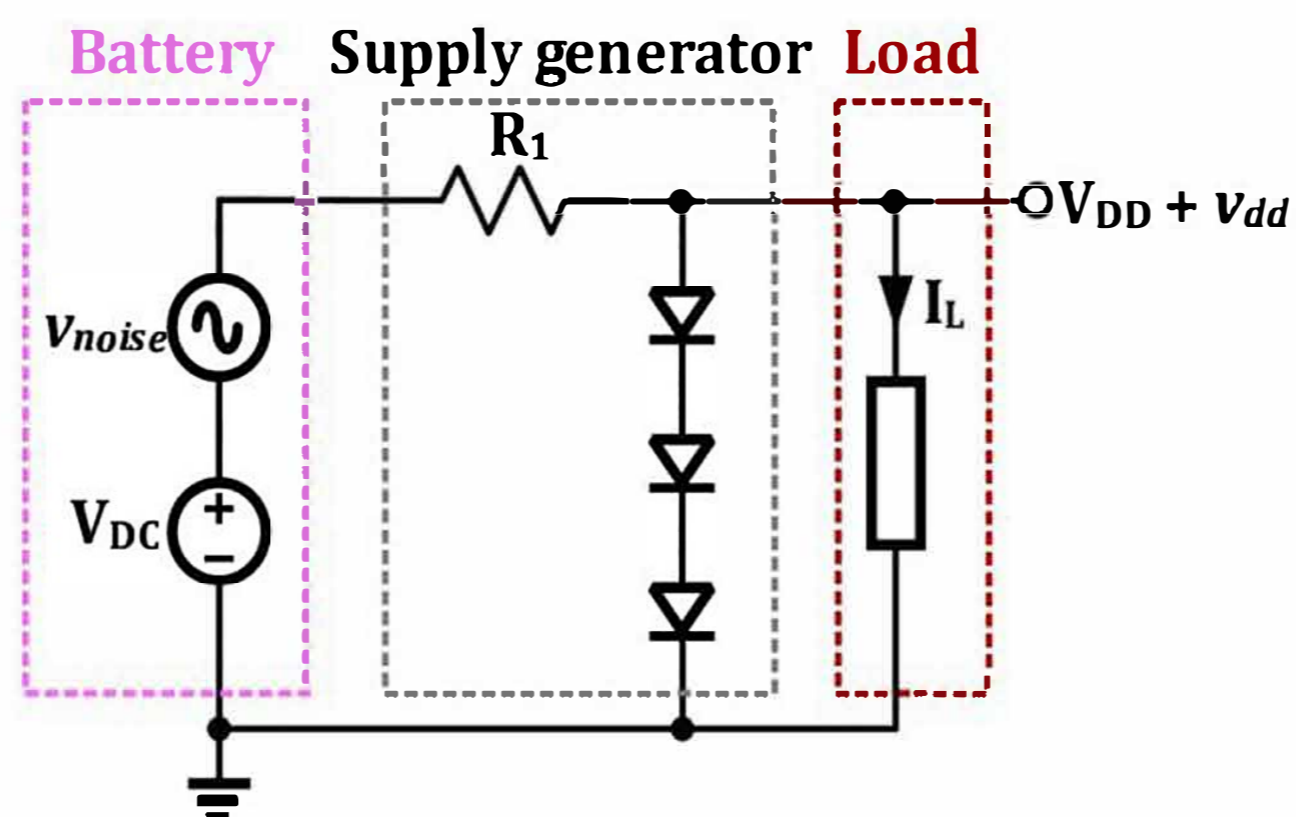
$$(b) \quad v_{in} = v_x + \frac{2 \cdot G_M \cdot V_{INO}}{V_T} v_x \cdot R_1 \Rightarrow v_x = \frac{v_{in}}{1 + \frac{2 G_M V_{INO} \cdot R_1}{V_T}}$$

$$v_{out} = - \frac{2 G_M \cdot V_{INO}}{V_T} \cdot v_x \cdot R_L$$

$$\Rightarrow A_v = \frac{v_{out}}{v_{in}} = - \frac{2 G_M \cdot V_{INO} / V_T \cdot R_L}{1 + \frac{2 G_M V_{INO} \cdot R_1}{V_T}}$$

(c) For maximum gain : $R_1 = 0$

4. Diodes can be used to generate desired supply voltage, V_{DD} , from a battery voltage as shown below.



The battery is modeled as a DC voltage source, V_{DC} in series with another voltage source, v_{noise} , that models small noise in the battery voltage. I_L is the current drawn by the load, which could be your iPad.

- Assuming nominal DC voltage of the battery, $V_{DC} = 5V$, $R_1 = 320\Omega$, and constant voltage model of the diode with $V_{D0} = 0.6V$, calculate the DC supply voltage, V_{DD} under no load condition (i.e. $I_L = 0$).
- Calculate perturbations in the supply voltage, v_{dd} , caused by noise in the battery voltage under no load condition.
- Repeat parts (a) and (b) when a load is connected to the supply, which draws a current of $I_L = 2mA$.
- Repeat parts (a) and (b) when battery discharges to $V_{DC} = 4.5V$.

$$(a) \quad V_{DD} = 3V_{D0} \Rightarrow \boxed{V_{DD} = 1.8V}$$

$$(b) \quad I_{R1} = \frac{5 - 1.8}{320} = 10mA = I_{D0}$$

$$r_d = \frac{V_T}{I_{D0}} = \frac{25m}{10m} = 2.5\Omega$$

$$v_{dd} = \frac{3 \cdot r_d}{R_1 + 3 \cdot r_d} = \frac{3 \times 2.5}{320 + 3 \times 2.5} \cdot v_{noise}$$

$$\Rightarrow \boxed{v_{dd} = 0.023 v_{noise} \approx \frac{v_{noise}}{43}} \Rightarrow \text{Noise is attenuated when it appears at the output}$$

(c) $I_{D0} = I_{R1} - I_L = 8 \text{ mA}$ $V_{D0} = 1.8 \text{ V} \Rightarrow V_{D0}$ is independent of I_L

$$r_d = \frac{25 \text{ m}}{8 \text{ m}} = 3.125 \Omega$$

$$v_{dd} = \frac{9.375}{329.375} \cdot v_{\text{noise}} \Rightarrow v_{dd} = 0.028 v_{\text{noise}} \approx \frac{v_{\text{noise}}}{35}$$

(d) $V_{D0} = 3V_{D0} = 1.8 \text{ V} \Rightarrow V_{D0}$ is independent of battery voltage

$$I_{R1} = I_{D0} = \frac{4.5 - 1.8}{320} = 8.44 \text{ mA}$$

$$r_d = \frac{25}{8.44} = 2.96 \text{ m}\Omega$$

$$v_{dd} = \frac{3 \times 2.96}{320 + 3 \times 2.96} \cdot v_{\text{noise}}$$

$$\Rightarrow v_{dd} = 0.027 \cdot v_{\text{noise}} \approx \frac{v_{\text{noise}}}{37}$$

5. A non-linear device has its output current, i_O , related to its input voltage, v_I , by $i_O = I_T e^{(v_I/V_T)}$, where I_T and V_T are constant current and voltage, respectively.

- Write the Taylor series expansion of i_O at an input voltage of $v_I = v_i + V_I$.
- Assuming $I_T = 1\text{A}$, $V_T = 25\text{mV}$ and $V_I = 1\text{V}$, plot i_O versus v_i .
- Plot the error between the exact i_O and Taylor series approximated i_O versus v_i .

Solution

- The Taylor series expansion of exponential is given as

$$e^x = 1 + x + x^2 + \dots$$

Assuming that V_I is a constant and we write the Taylor series expansion with respect to v_i (i.e we try to capture the change of i_O vs. v_i around a fixed V_I biasing), we have the following

$$i_O = I_T e^{\frac{V_I}{V_T}} \left[1 + \frac{v_i}{V_T} + \frac{1}{2!} \left(\frac{v_i}{V_T} \right)^2 + \dots \right]$$

Note that Taylor series expansion contains an *infinite* number of terms.

