

33 TL circuits with half- and quarter-wave transformers

- Last lecture we established that phasor solutions of telegrapher's equations for TL's in sinusoidal steady-state can be expressed as

$$V(d) = V^+ e^{j\beta d} + V^- e^{-j\beta d} \quad \text{and} \quad I(d) = \frac{V^+ e^{j\beta d} - V^- e^{-j\beta d}}{Z_o}$$

in a new coordinate system shown in the margin.

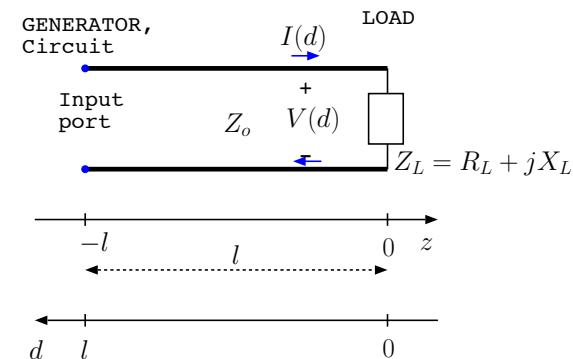
By convention the load is located on the right at $z = 0 = d$, and the TL input connected to a generator or some source circuit is shown on the left at $d = l$.

We have replaced the short termination of the previous lecture with an arbitrary load impedance

$$Z_L = R_L + jX_L.$$

In this lecture we will discuss sinusoidal steady-state TL circuit problems having arbitrary reactive loads but with line lengths l constrained to be integer multiples of $\frac{\lambda}{4}$ (at the operation frequency).

The constraint will be lifted next lecture when we will develop the general analysis tools for sinusoidal steady-state TL circuits.



- In the TL circuit shown in the margin an arbitrary load Z_L is connected to a TL of length $l = \frac{\lambda}{2}$ at the source frequency.

Given that

$$e^{\pm j\beta \frac{\lambda}{2}} = e^{\pm j \frac{2\pi}{\lambda} \frac{\lambda}{2}} = e^{\pm j\pi} = -1,$$

the general phasor relations

$$V(d) = V^+ e^{j\beta d} + V^- e^{-j\beta d} \quad \text{and} \quad I(d) = \frac{V^+ e^{j\beta d} - V^- e^{-j\beta d}}{Z_o}$$

imply

$$V_{in} \equiv V\left(\frac{\lambda}{2}\right) = -V^+ - V^- = -V(0) = -V_L,$$

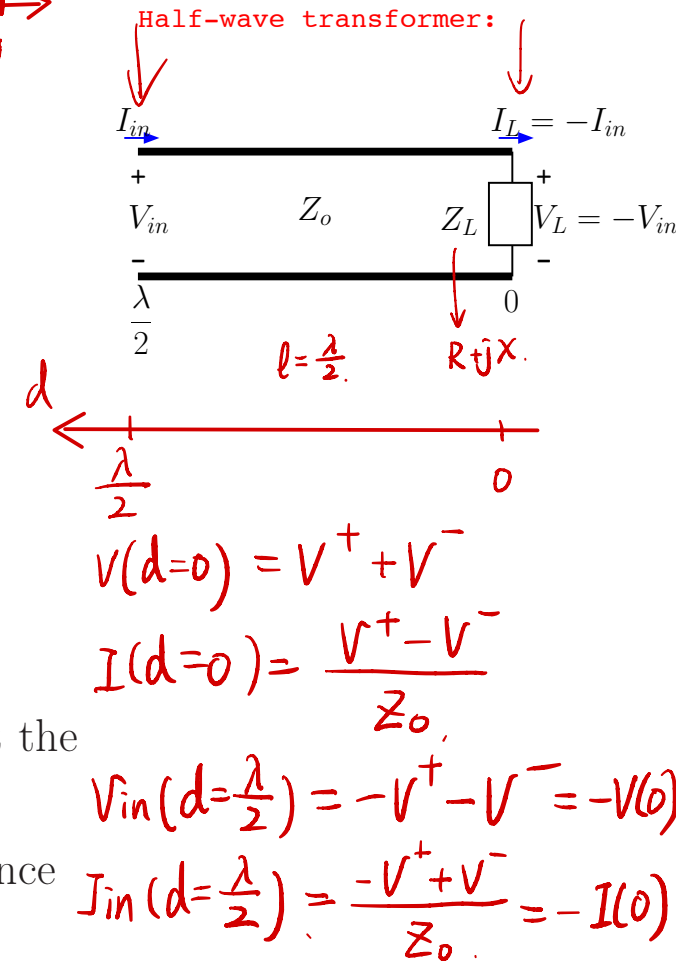
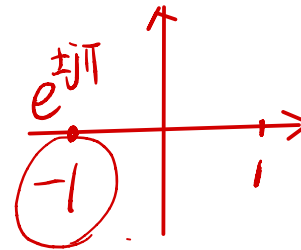
$$I_{in} \equiv I\left(\frac{\lambda}{2}\right) = \frac{-V^+ + V^-}{Z_o} = -I(0) = -I_L.$$

We conclude that a $\frac{\lambda}{2}$ -transformer

- inverts the algebraic sign of its voltage and current inputs at the load end (and vice versa), and
- has an input impedance identical with the load impedance since

$$Z_{in} \equiv \frac{V_{in}}{I_{in}} = \frac{-V_L}{-I_L} = Z_L.$$

These very simple results are easy to remember and use.



- In the TL circuit shown in the margin an arbitrary load Z_L is connected to a TL of length $l = \frac{\lambda}{4}$ at the source frequency.

Given that

$$e^{\pm j\beta \frac{\lambda}{4}} = e^{\pm j \frac{2\pi}{\lambda} \frac{\lambda}{4}} = e^{\pm j \frac{\pi}{2}} = \pm j,$$

general phasor relations

$$V(d) = V^+ e^{j\beta d} + V^- e^{-j\beta d} \quad \text{and} \quad I(d) = \frac{V^+ e^{j\beta d} - V^- e^{-j\beta d}}{Z_o}$$

imply

$$V_{in} \equiv V\left(\frac{\lambda}{4}\right) = jV^+ - jV^- = jI(0)Z_o = jI_L Z_o,$$

$$V(d=0) = V^+ + V^-$$

$$I(d=0) = \frac{V^+ - V^-}{Z_o}$$

$$V_L = -j I_{in} Z_o$$

$$= -j \frac{V_{in} Z_L}{Z_o}$$

We conclude that a $\frac{\lambda}{4}$ -transformer

– has an input impedance

$$Z_{in} \equiv \frac{V_{in}}{I_{in}} = \frac{jI_L Z_o}{jV_L/Z_o} = \frac{Z_o^2}{V_L/I_L} = \frac{Z_o^2}{Z_L},$$

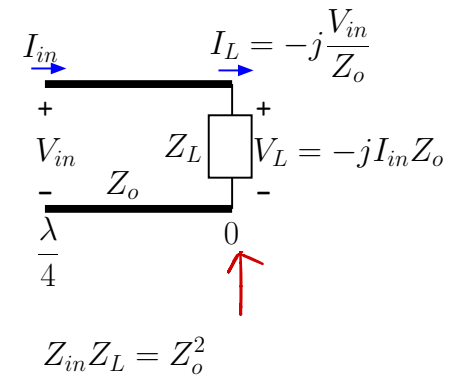
– and provides a load current

$$I_L = -j \frac{V_{in}}{Z_o},$$

proportional to input voltage V_{in} but independent of load impedance Z_L .

$Z_L = \text{short.} \Rightarrow Z_{in} = \infty \text{ open.}$
 $Z_L = \text{open.} \Rightarrow Z_{in} = 0 \text{ short.}$
 $Z_L = j\omega L \Rightarrow Z_{in} = \frac{Z_o^2}{j\omega L} = -j \frac{Z_o^2}{\omega L}$

Quarter-wave transformer:



Quarter-wave current-forcing equation:

$$I_L = -j \frac{V_{in}}{Z_o}$$

Load voltage

$$V_L = Z_L I_L$$

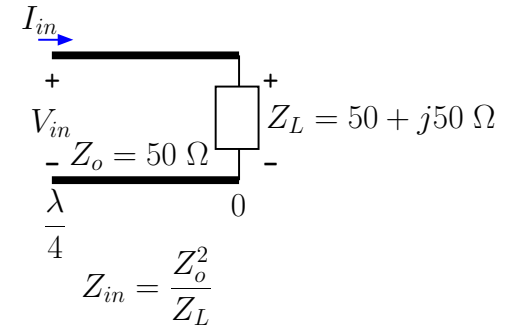
once I_L is available from above equation.

Example 1: Given $Z_L = 50 + j50 \Omega$, what is Z_{in} for a $\frac{\lambda}{4}$ transformer with $Z_o = 50 \Omega$?

Solution: It is

$$Z_{in} = \frac{Z_o^2}{Z_L} = \frac{50^2}{50 + j50} = \frac{50}{1 + j1} = \frac{50}{1 + j1} \frac{1 - j1}{1 - j1} = 25 - j25 \Omega.$$

Notice that an *inductive* Z_L has been turned into a *capacitive* Z_{in} by $\frac{\lambda}{4}$ transformer.



Example 2: The load and the transformer of Example 1 are connected to a source with voltage phasor $V_g = 100\angle 0^\circ$ V at the input port. What is the load current I_L and what is the average power absorbed by the load?

Solution: Since $V_{in} = V_g = 100\angle 0^\circ$ V, the current-forcing formula for the quarter-wave transformer implies

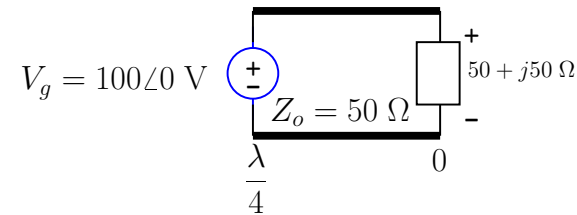
$$I_L = -j \frac{V_{in}}{Z_o} = -j \frac{100}{50} = -j2 \text{ A.}$$

To find the average power absorbed, we first note that load voltage

$$V_L = Z_L I_L = (50 + j50)(-j2) = 100 - j100 \text{ V.}$$

Thus,

$$P_L = \frac{1}{2} \text{Re}\{V_L I_L^*\} = \frac{1}{2} \text{Re}\{(100 - j100)(j2)\} = 100 \text{ W.}$$



Example 3: Load $Z_L = 100 \Omega$ is connected to a T.L. with length $l = 0.75\lambda$. At the generator end, $d = 0.75\lambda$, a source with open circuit voltage $V_g = j10 \text{ V}$ and Thevenin impedance $Z_g = 25 \Omega$ is connected. Determine V_L and I_L if $Z_o = 50 \Omega$.

Solution: First we determine input impedance Z_{in} by noting that $Z_L = 100 \Omega$ transforms to itself, namely 100Ω at $d = 0.5\lambda$, but then it transforms from $d = 0.5\lambda$ to 0.75λ as

$$Z_{in} = \frac{Z_o^2}{Z(0.5\lambda)} = \frac{50^2}{100} = 25 \Omega.$$

Hence, using voltage division, we find,

$$V_{in} = V_g \frac{Z_{in}}{Z_g + Z_{in}} = j10 \frac{25}{25 + 25} = j5 \text{ V}.$$

Next, using half-wave transformer rule, we notice that

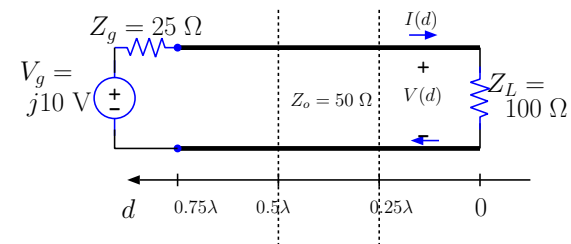
$$V(0.25\lambda) = -V_{in} = -j5 \text{ V},$$

and finally applying the quarter-wave current forcing equation with $V(0.25\lambda)$ we get

$$I_L = -j \frac{V(0.25\lambda)}{Z_o} = -j \frac{-j5}{50} = -0.1 \text{ A}.$$

Clearly, then, the load voltage is

$$V_L = Z_L I_L = (100 \Omega)(-0.1 \text{ A}) = -10 \text{ V}.$$



Example 4: In the circuit shown in the margin, $Z_{L1} = 50 \Omega$, $Z_{L2} = 100 \Omega$, and $Z_{o1} = Z_{o2} = 50 \Omega$. Determine I_{L1} and I_{L2} if $V_{in} = 5 \text{ V}$. Both T.L. sections are quarter-wave transformers.

Solution: Using the current-forcing equation, we have

$$I_{L1} = I_{L2} = -j \frac{V_{in}}{Z_o} = -j \frac{5}{50} = -j0.1 \text{ A}.$$

Consequently,

$$V_{L1} = I_{L1} Z_{L1} = -j0.1 \text{ A} \times 50 \Omega = -j5 \text{ V}$$

and

$$V_{L2} = I_{L2} Z_{L2} = -j0.1 \text{ A} \times 100 \Omega = -j10 \text{ V}.$$

Thus, total avg power absorbed is

$$\begin{aligned} P &= \frac{1}{2} \text{Re}\{V_{L1} I_{L1}^*\} + \frac{1}{2} \text{Re}\{V_{L2} I_{L2}^*\} \\ &= \frac{1}{2} \text{Re}\{-j5 \times j0.1\} + \frac{1}{2} \text{Re}\{-j10 \times j0.1\} = 0.75 \text{ W}. \end{aligned}$$

