

15 Inductance — solenoid, shorted coax

- Given a current conducting path C , the magnetic flux Ψ linking C can be expressed as a function of current I circulating around C .
- If the function is linear, i.e., if we have a *linear flux-current relation*

$$\rightarrow \Psi = LI,$$

then constant

$$\rightarrow L = \frac{\Psi}{I}$$

is termed the self-inductance¹ of path C , an elementary **inductor**.

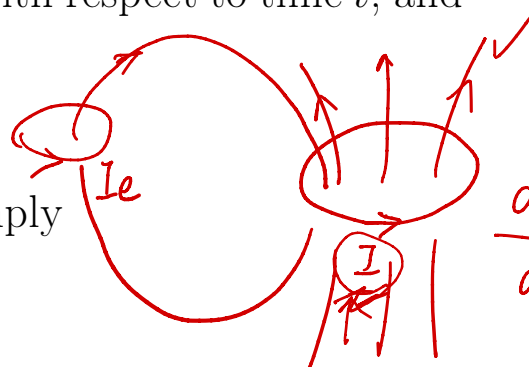
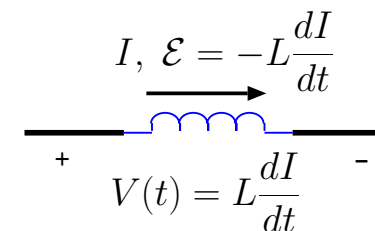
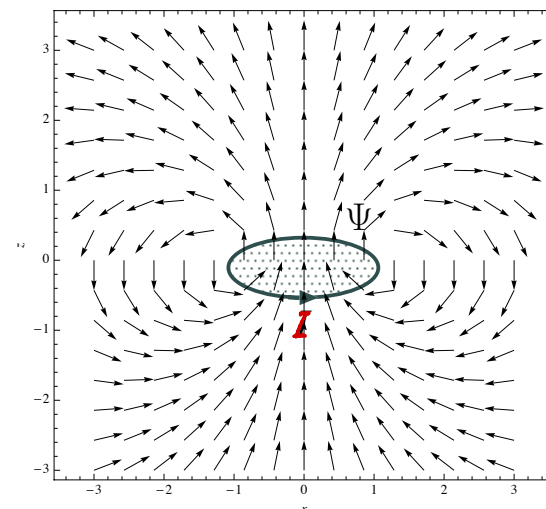
- Differentiating the flux-current relation with respect to time t , and using the fact that

$$\mathcal{E} = -\frac{d\Psi}{dt},$$

we find that the emf of inductor L is simply

$$\mathcal{E} = -L\frac{dI}{dt},$$

which is a voltage rise across the inductor in the direction of current I (with $L\frac{dI}{dt}$ denoting the voltage drop in the same direction as used in circuit courses).



$$\frac{d\Psi}{dt} = L \frac{dI}{dt} = -\mathcal{E}.$$

$$\Psi = L I + M I_e$$

$$\frac{d\Psi}{dt} = L \frac{dI}{dt} + M \frac{dI_e}{dt} = -\mathcal{E}.$$

$\mathcal{E} = RI.$

¹A mutual inductance M_{12} , by contrast, relates the flux linking coil C_2 to a current I_1 flowing in a second coil C_1 .

- For an inductor consisting of n -loops, the emf \mathcal{E} measured around n -loops is naturally

$$L = \frac{\Psi}{I} \text{ single } \mathcal{E} = n \left(-\frac{d\Psi}{dt} \right) = -\frac{d}{dt} n\Psi \equiv -L \frac{dI}{dt}$$

implying an inductance

$$L \equiv \frac{n\Psi}{I} \leftarrow n\Psi = LI.$$

$$L \frac{dI}{dt} + M \frac{dI_e}{dt} = -RI.$$

$$L \frac{dI}{dt} + RI = -M \frac{dI_e}{dt}$$

$$L \frac{dI}{dt} + RI = 0. \text{ source free}$$

$$I_e \uparrow M \uparrow L \downarrow. \quad \checkmark RI = -M \frac{dI_e}{dt}.$$

Example 1: An n -turn coil has a resistance $R = 1 \Omega$ and inductance of $1 \mu\text{H}$. If it is conducting 3 A of current at $t = 0$, determine $I(t)$ for $t > 0$.

Solution: Current flow in the resistive n -turn coil will be driven by emf $\mathcal{E} = -L \frac{dI}{dt}$ matching the voltage drop RI . Hence

$$-L \frac{dI}{dt} = RI \leftrightarrow \frac{dI}{dt} + \frac{R}{L} I = 0 \Rightarrow I(t) = I(0) e^{-\frac{R}{L} t} = 3e^{-10^6 t} \text{ A}.$$

- As illustrated by above example, current I around a resistive loop C will in general be obtained by solving a *differential equation* constructed using the emf of the loop.

- $I = \frac{\mathcal{E}}{R}$ used last lecture assumes that emf produced by the induced current is small compared to an externally produced emf.

- We continue with typical inductance calculations.

- Notice that the stored energy of the solenoid is

$$\frac{1}{2}\mu_o|H_z|^2 = \frac{1}{2}\mu_o\mathbf{H} \cdot \mathbf{H}$$

times its volume $A\ell$ occupied by the field \mathbf{H} inside the solenoid. That suggests that

$$w = \frac{1}{2}\mu_o\mathbf{H} \cdot \mathbf{H}$$

can be interpreted as stored magnetostatic energy per unit volume in general.

- Also both inductance L and stored energies W and w would have μ replacing μ_o in material media with permeabilities

$$\mu = (1 + \chi_m)\mu_o$$

and magnetic susceptibilities χ_m , in analogy with the concepts of permittivity $\epsilon = (1 + \chi_e)\epsilon_o$ and electrical susceptibility χ_e .

- Permeability and magnetic susceptibility notions will be examined in a future lecture.

Inductance of shorted coax: Consider a coaxial cable of some length ℓ which is “shorted” at one end (with a wire connecting the inner and outer conductors), so that a steady current I can flow on the inner conductor of radius a to return on the interior surface of the outer conductor at radius b after having circulated through the short. We will next determine the inductance L of such an inductor after first computing the magnetic flux density B_ϕ that will be produced by the inner conductor current I . In B_ϕ calculation we will assume $\ell \gg b$ so that an “infinite coax” approximation can be invoked.

- Expanding the integral form of Ampere’s law

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_o I_C$$

as

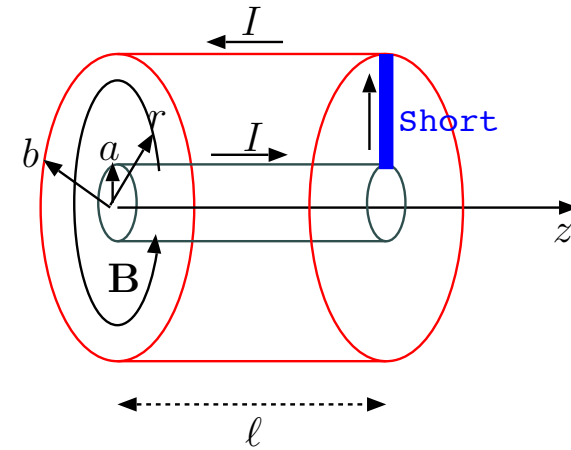
$$B_\phi 2\pi r = \mu_o I$$

over a circular integration contour C of a radius $r > a$, we find that the magnetic flux density in the interior of the coax cable is

$$B_\phi = \frac{\mu_o I}{2\pi r}.$$

- Therefore, the magnetic flux linked by the closed current path I (see figure in the margin) is

$$\Psi = \int_S \mathbf{B} \cdot d\mathbf{S} = \ell \frac{\mu_o}{2\pi} I \int_a^b \frac{dr}{r} = \ell \frac{\mu_o}{2\pi} \ln \frac{b}{a} I.$$



Shorted coax circulates a current I linking a magnetic flux Ψ confined to a region bounded by the outer conductor of the coax.

Clearly, we have a linear relation $\Psi = LI$, with

$$L \equiv \frac{\ln \frac{b}{a}}{2\pi} \ell \mu_o,$$

which is the inductance of a shorted coax of a finite length ℓ .

– The inductance of the coax per unit length is

$$\mathcal{L} = \frac{\ln \frac{b}{a}}{2\pi} \mu_o,$$

which should be contrasted with capacitance per unit length

$$\mathcal{C} = \frac{2\pi}{\ln \frac{b}{a}} \epsilon_o$$

of the same coax configuration.

Notice how \mathcal{L} and \mathcal{C} are proportional to ϵ_o and μ_o , respectively, having proportionality constants which are inverses of one another.

Inductance of shorted parallel plates: If a pair of parallel plates of areas $A = W\ell$ and separation d were shorted at one end, we would obtain effectively an inductor with a per length inductance

$$\mathcal{L} = \frac{d}{W}\mu_o$$

that accompanies per length capacitance

$$\mathcal{C} = \frac{W}{d}\epsilon_o$$

of the same parallel plate configuration. This follows from a generalization of our finding above that the proportionality constants of \mathcal{L} and \mathcal{C} are arithmetic inverses of one another.