

13 Current sheet, solenoid, vector potential and current loops

In the following examples we will calculate the magnetic fields $\mathbf{B} = \mu_o \mathbf{H}$ established by some simple current configurations by using the integral form of static Ampere's law.

$$\oint_C \vec{B} \cdot d\vec{\ell} = \mu_o I_C.$$

Example 1: Consider a uniform **surface current density** $\mathbf{J}_s = J_s \hat{z}$ A/m flowing on $x = 0$ plane (see figure in the margin) — the current sheet extends infinitely in y and z directions. Determine \mathbf{B} and \mathbf{H} .

Solution: Since the current sheet extends infinitely in y and z directions we expect \mathbf{B} to depend only on coordinate x . Also, the field should be the superposition of the fields of an infinite number of current filaments, which suggests, by right-hand-rule, $\mathbf{B} = \hat{y}B(x)$, where $B(x)$ is an odd function of x . To determine $B(x)$, such that $B(-x) = -B(x)$, we apply Ampere's law by computing the circulation of \mathbf{B} around the rectangular path C shown in the figure in the margin. We expand

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_o I_C$$

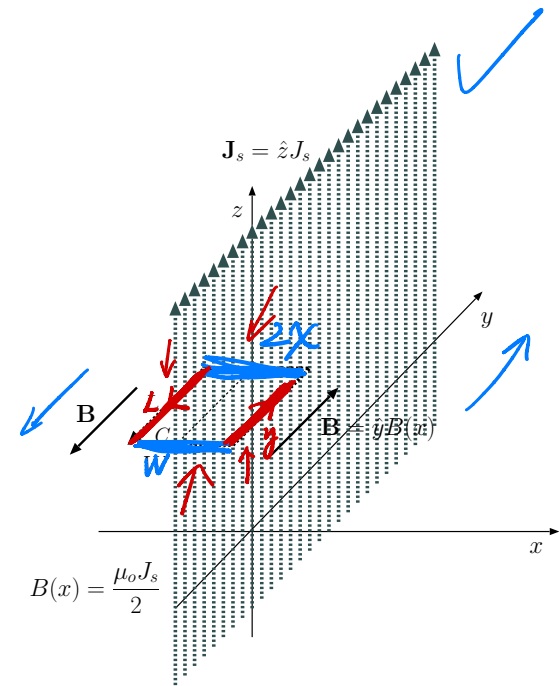
as

$$B(x)L + 0 - B(-x)L + 0 = \mu_o J_s L,$$

from which we obtain

$$B(x) = \frac{\mu_o J_s}{2} \Rightarrow \mathbf{B} = \hat{y} \frac{\mu_o J_s}{2} \text{sgn}(x) \text{ and } \mathbf{H} = \hat{y} \frac{J_s}{2} \text{sgn}(x).$$

$$E(x) = \frac{\rho_s}{2\epsilon_o}$$



As shown in Example 1 magnetic field of a current sheet is independent of distance $|x|$ from the current sheet. Also \mathbf{H} changes discontinuously across the current sheet by an amount J_s .

$$\vec{H} = \frac{J_s}{2} \hat{y} \quad \vec{H} = -\frac{J_s}{2} \hat{y} \quad H = \frac{J_s}{2}$$

the \mathbf{H} field, which is tangential to the surface current density, jumps by the amount of surface current that you go through.

$$\vec{D} \leftarrow \vec{D} \quad D = \frac{\rho_s}{2}$$

$$\vec{H} \leftarrow \vec{H} \quad \vec{H} \rightarrow \vec{H} \quad J_s \hat{z}$$

Example 2: Consider a slab of thickness W over $-\frac{W}{2} < x < \frac{W}{2}$ which extends infinitely in y and z directions and conducts a uniform current density of $\mathbf{J} = \hat{z}J_o$ A/m². Determine \mathbf{H} if the current density is zero outside the slab.

Solution: Given the geometric similarities between this problem and Example 1, we postulate that $\mathbf{B} = \hat{y}B(x)$, where $B(x)$ is an odd function of x , that is $B(-x) = -B(x)$. To determine $B(x)$ we apply Ampere's law by computing the circulation of \mathbf{B} around the rectangular path C shown in the figure in the margin. For $x < \frac{W}{2}$, we expand

$$\oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_o I_C$$

as

$$\checkmark B(x)L + 0 - B(-x)L + 0 = \mu_o J_o 2xL \Rightarrow B(x) = \mu_o J_o x.$$

For $x \geq \frac{W}{2}$, the expansion gives

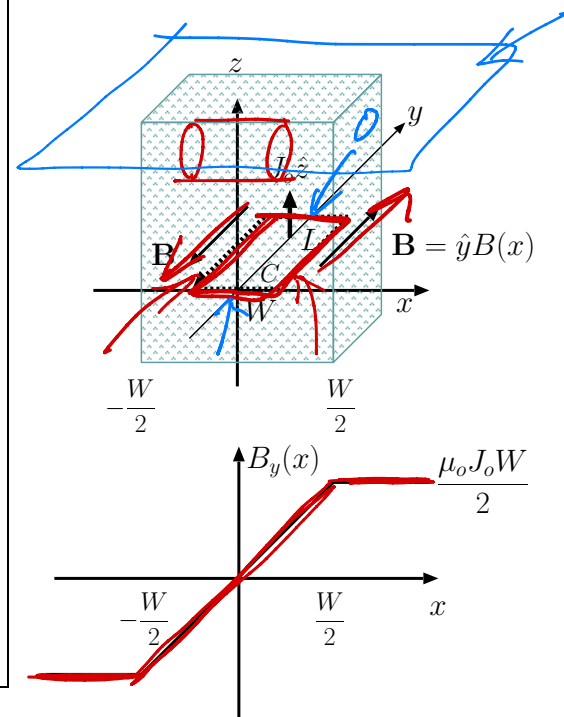
$$\checkmark B(x)L + 0 - B(-x)L + 0 = \mu_o J_o WL \Rightarrow B(x) = \mu_o J_o \frac{W}{2}.$$

Hence, we find that

$$\checkmark \mathbf{H} = \begin{cases} \hat{y}J_o x, & |x| < \frac{W}{2} \\ \hat{y}J_o \frac{W}{2} \text{sgn}(x), & \text{otherwise.} \end{cases}$$

Note that the solution plotted in the margin shows no discontinuity at $x = \pm \frac{W}{2}$ or elsewhere.

$$\vec{B} = \mu_o \vec{H}.$$



The figure in the margin depicts a finite section of an infinite solenoid. A solenoid can be constructed in practice by winding a long wire into a

multi loop coil as depicted. A solenoid with its loop carrying a current I in $\hat{\phi}$ direction (as shown), produces effectively a surface current density of $\mathbf{J}_s = IN\hat{\phi}$ A/m, where N is the number density (1/m) of current loops in the solenoid. In Example 3 we compute the magnetic field of the infinite solenoid using Ampere's law.

Example 3: An infinite **solenoid** having N loops per unit length is stacked in z -direction, each loop carrying a current of I A in counter-clockwise direction when viewed from the top (see margin). Determine **H**.

Solution: Assuming that $\mathbf{B} = 0$ outside the solenoid, and also \mathbf{B} is independent of z within the solenoid, we find that Ampere's law indicates for the circulation C shown in the margin A.

$$\checkmark \oint_C \mathbf{B} \cdot d\mathbf{l} = \mu_o I_C \Rightarrow \underbrace{LB}_{A/m} = \underbrace{\mu_o I N L}_{m}$$

This leads to

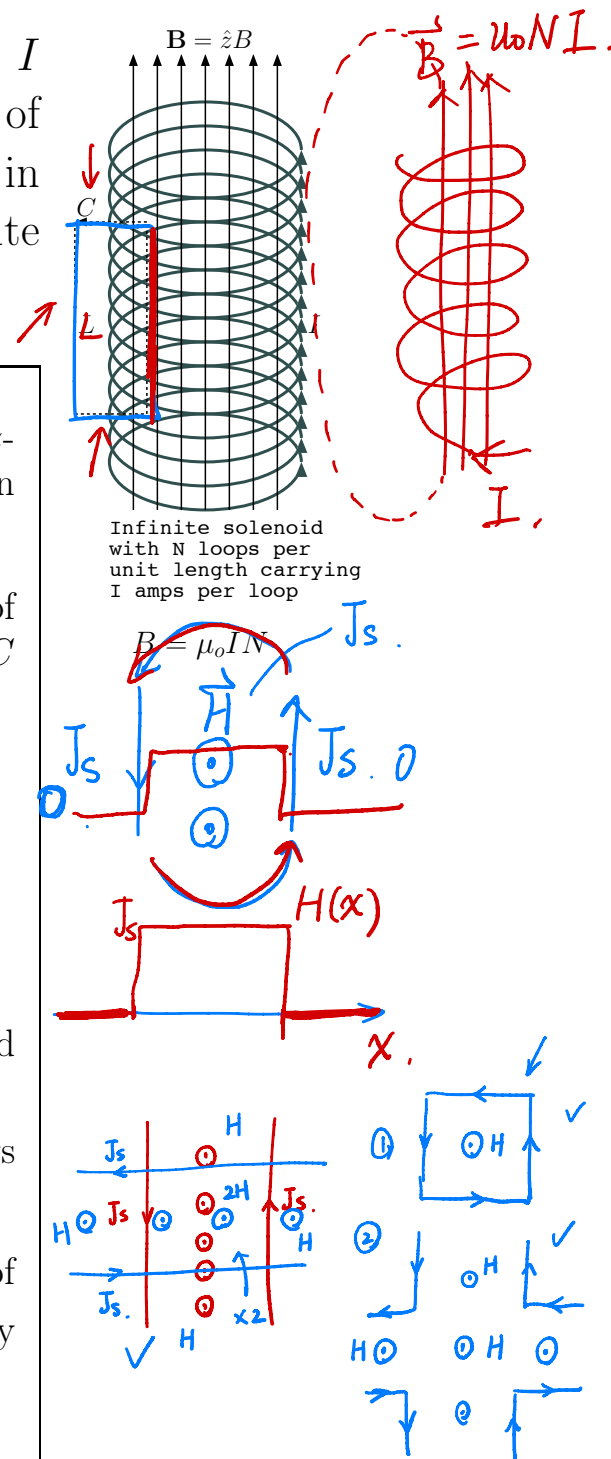
$$B = \mu_o \underline{IN} \quad \text{and} \quad \mathbf{H} = \underline{\hat{z}IN}$$

for the field within the solenoid.

The assumption of zero magnetic flux density $\mathbf{B} = 0$ for the exterior region is justified because:

(a) if the exterior field is non-zero, then it must be independent of x and y (follows from Ampere's law applied to any exterior path C with $I_C = 0$), and

(b) the finite interior flux $\Psi = \mu_o I N \pi a^2$ can only be matched with the flux of the infinitely extended exterior region when the *constant* exterior flux density (because of (a)) is vanishingly small.



- **Static electric fields:** *Curl-free* and are governed by

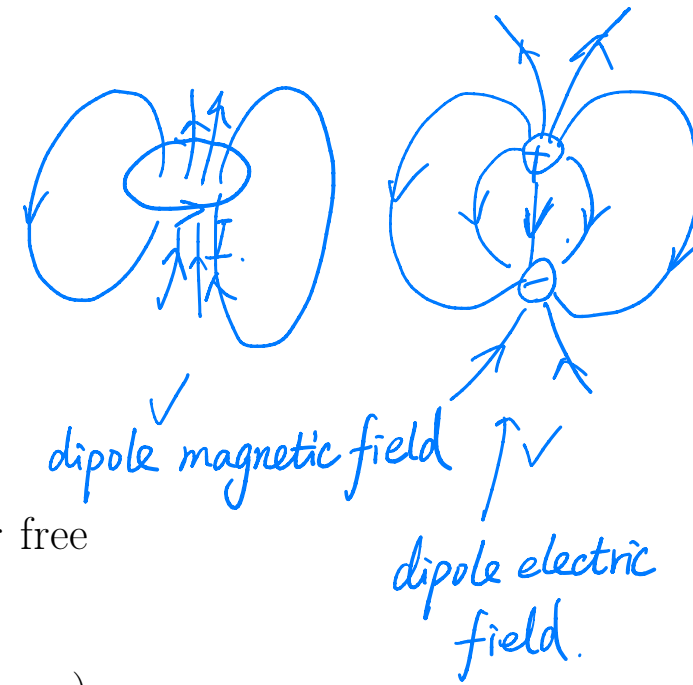
$$\nabla \times \mathbf{E} = 0, \quad \nabla \cdot \mathbf{D} = \rho \quad \text{where} \quad \mathbf{D} = \epsilon \mathbf{E}$$

with $\epsilon = \epsilon_r \epsilon_0$.

- **Static magnetic fields:** *Divergence-free* and are governed by

$$\star \quad \nabla \cdot \mathbf{B} = 0, \quad \nabla \times \mathbf{H} = \mathbf{J} \quad \text{where} \quad \mathbf{B} = \mu \mathbf{H}$$

with $\mu = \mu_r \mu_0$ — relative *permeabilities* μ_r other than unity (for free space) will be explained later on.



Mathematically, we can generate a **divergence-free** vector field $\mathbf{B}(x, y, z)$ as

$$\nabla \cdot (\mathbf{B} = \nabla \times \mathbf{A}) \quad \leftarrow$$

by taking the curl of any vector field $\mathbf{A} = \mathbf{A}(x, y, z)$ (just like we can generate a curl-free \mathbf{E} by taking the gradient of any scalar field $-V(x, y, z)$).

Verification: Notice that

$$\begin{aligned} \nabla \cdot \nabla \times \mathbf{A} &= \frac{\partial}{\partial x}(\nabla \times \mathbf{A})_x + \frac{\partial}{\partial y}(\nabla \times \mathbf{A})_y + \frac{\partial}{\partial z}(\nabla \times \mathbf{A})_z = \left\{ \begin{array}{ccc} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{array} \right\} \\ &= \frac{\partial}{\partial x} \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) - \frac{\partial}{\partial y} \left(\frac{\partial A_z}{\partial x} - \frac{\partial A_x}{\partial z} \right) + \frac{\partial}{\partial z} \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right) = 0. \end{aligned}$$

- If $\mathbf{B} = \nabla \times \mathbf{A}$ represents a magnetostatic field, then \mathbf{A} is called magnetostatic potential or **vector potential**.

- Vector potential \mathbf{A} can be used in magnetostatics in similar ways to how electrostatic potential V is used in electrostatics.
 - In electrostatics we can assign $V = 0$ to any point in space that is convenient in a given problem.
 - In magnetostatics we can assign $\nabla \cdot \mathbf{A}$ to any scalar that is convenient in a given problem.
- For example, if we make the assignment¹

$$\star \checkmark \quad \nabla \cdot \mathbf{A} = 0, \quad \text{and} \quad \checkmark \nabla \times \vec{A} = \vec{B}$$

Coulomb gauge.

then we find that

$$\checkmark \nabla \times \mathbf{B} = \nabla \times \nabla \times \mathbf{A} = \nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A} = -\nabla^2 \mathbf{A}.$$

This is a *nice and convenient* outcome, because, when combined with

$$\nabla \times \mathbf{H} = \mathbf{J} \quad \Rightarrow \quad \nabla \times \mathbf{B} = \mu_o \mathbf{J},$$

it produces

$$\text{solve } \checkmark \nabla^2 \mathbf{A} = -\mu_o \mathbf{J}, \quad \text{for } \vec{A}. \quad \text{then } \vec{B} = \nabla \times \vec{A}. \quad \leftarrow$$

which is the magnetostatic version of Poisson's equation

$$\text{solve } \checkmark \nabla^2 V = -\frac{\rho}{\epsilon_o} \quad \text{for } V. \quad \text{then } \vec{E} = -\nabla V.$$

¹With this assignment — known as *Coulomb gauge* — \mathbf{A} acquires the physical meaning of “potential momentum per unit charge”, just as scalar potential V is “potential energy per unit charge” (see Konopinski, *Am. J. Phys.*, 46, 499, 1978).

- In analogy with solution

$$\checkmark \rightsquigarrow V(\mathbf{r}) = \int \frac{\rho(\mathbf{r}')}{4\pi\epsilon_0|\mathbf{r} - \mathbf{r}'|} d^3\mathbf{r}' \quad \frac{\rho}{\epsilon_0}$$

of Poisson's equation, it has a solution

$$\Delta \rightsquigarrow \underline{\mathbf{A}(\mathbf{r}) = \int \frac{\mu_0 \mathbf{J}(\mathbf{r}')}{4\pi|\mathbf{r} - \mathbf{r}'|} d^3\mathbf{r}'} \quad \downarrow \mu_0 \cdot \vec{J}$$

Given *any* static² current density $\mathbf{J}(\mathbf{r})$, the above equation can be used to obtain the corresponding vector potential \mathbf{A} that simultaneously satisfies

$$\nabla \cdot \mathbf{A} = 0 \quad \text{and} \quad \underline{\nabla \times \mathbf{A} = \mathbf{B}}.$$

Once \mathbf{A} is available, obtaining $\mathbf{B} = \nabla \times \mathbf{A}$ is then just a matter of taking a curl.

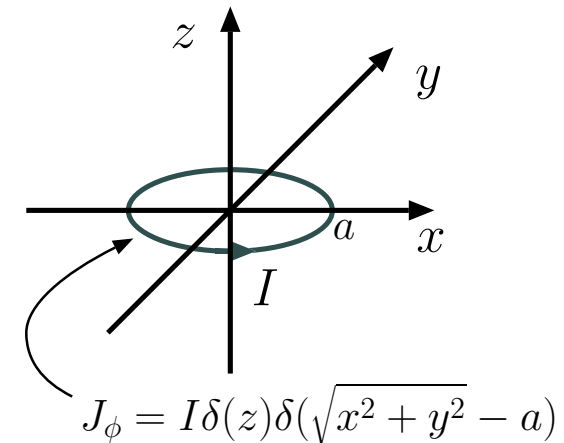
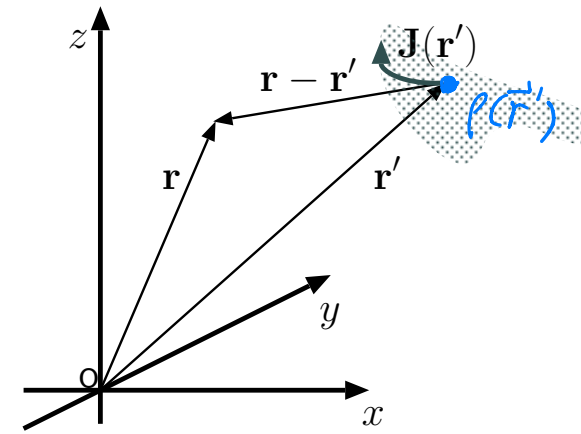
- Magnetic flux density \mathbf{B} of a *single* current loop I can be calculated after determining its vector potential as follows:

- For a loop of radius a on $z = 0$ plane, we can express the corresponding current density as

$$\mathbf{J}(\mathbf{r}') = I\delta(z')\delta(\sqrt{x'^2 + y'^2} - a) \frac{(-y', x', 0)}{\sqrt{x'^2 + y'^2}}$$

where the ratio on the right is the unit vector $\hat{\phi}'$.

- Inserting this into the general solution for vector potential, and performing the integration over z' , we obtain



²Also, in quasi-statics we use $\mathbf{J}(\mathbf{r}', t)$ to obtain $\mathbf{A}(\mathbf{r}, t)$ and $\mathbf{B} = \nabla \times \mathbf{A}$ over regions small compared to $\lambda = c/f$, with f the highest frequency in $\mathbf{J}(\mathbf{r}', t)$.

$$\begin{aligned}
\mathbf{A}(\mathbf{r}) &= \frac{\mu_o I}{4\pi} \int \delta(\sqrt{x'^2 + y'^2} - a) \frac{(-y', x', 0)}{\sqrt{(x - x')^2 + (y - y')^2 + z^2} \sqrt{x'^2 + y'^2}} dx' dy' \\
&= \frac{\mu_o I}{4\pi} \int \delta(r' - a) \frac{(-y', x', 0)}{\sqrt{(x - x')^2 + (y - y')^2 + z^2} r'} r' dr' d\phi' \\
&= \frac{\mu_o I}{4\pi} \int_{-\pi}^{\pi} \frac{(-a \sin \phi', a \cos \phi', 0)}{\sqrt{(x - a \cos \phi')^2 + (y - a \sin \phi')^2 + z^2}} d\phi' \equiv \hat{x} A_x(\mathbf{r}) + \hat{y} A_y(\mathbf{r}).
\end{aligned}$$

- Given that $A_z = 0$, it can be shown that $\mathbf{B} = \nabla \times \mathbf{A}$ leads to

$$B_x = -\frac{\partial A_y}{\partial z}, \quad B_y = \frac{\partial A_x}{\partial z}, \quad B_z = \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y}.$$

- From the expected azimuthal symmetry of \mathbf{B} about the z -axis, it is sufficient to evaluate these on, say, $y = 0$ plane — after some algebra, and dropping the primes, we find, on $y = 0$ plane,

$$B_x = \frac{\mu_o a I}{4\pi} \int_{-\pi}^{\pi} \frac{z \cos \phi}{(x^2 + a^2 + z^2 - 2ax \cos \phi)^{3/2}} d\phi,$$

$$B_y = \frac{\mu_o a I}{4\pi} \int_{-\pi}^{\pi} \frac{z \sin \phi}{(x^2 + a^2 + z^2 - 2ax \cos \phi)^{3/2}} d\phi,$$

and

$$B_z = \frac{\mu_o a I}{4\pi} \int_{-\pi}^{\pi} \frac{a - x \cos \phi}{(x^2 + a^2 + z^2 - 2ax \cos \phi)^{3/2}} d\phi.$$

- We note that $B_y = 0$ since the B_y integrand above is odd in ϕ and the integration limits are centered about the origin. Hence, the field on $y = 0$ plane is given as

$$\mathbf{B} = \hat{x} B_x + \hat{z} B_z$$

with B_x and B_z defined above.

- There are no closed form expressions for the B_x and B_z integrals above for an arbitrary (x, z) .

- However, it can be easily seen that if $x = 0$ (i.e., along the z -axis), $B_x = 0$ (as symmetry would dictate) and

$$B_z = \frac{\mu_o a I}{4\pi} \int_{-\pi}^{\pi} \frac{a}{(a^2 + z^2)^{3/2}} d\phi = \frac{\mu_o I a^2}{2(a^2 + z^2)^{3/2}}.$$

For $|z| \gg a$,

$$B_z \approx \frac{\mu_o I a^2}{2|z|^3},$$

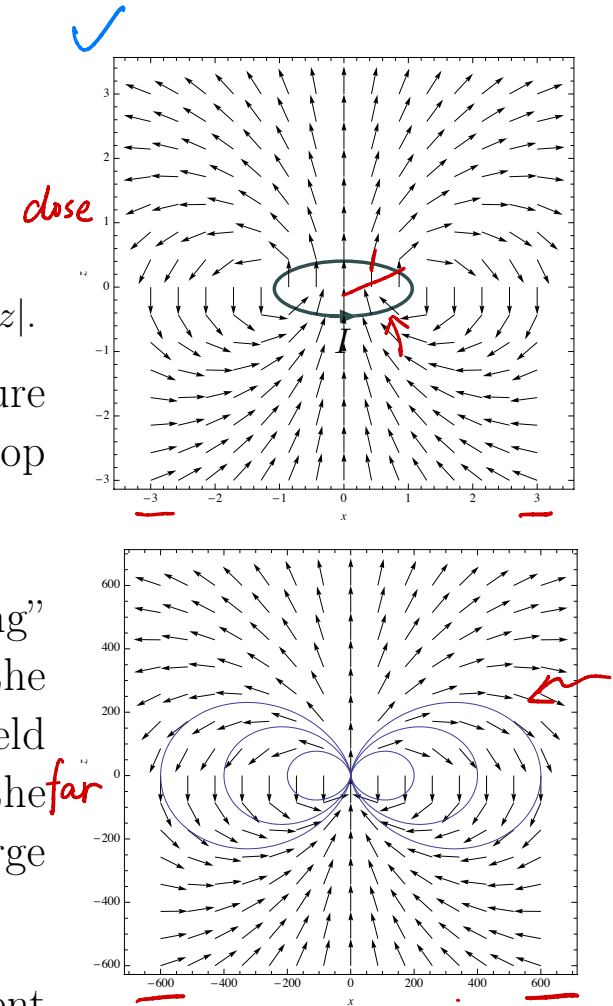
which is positive and varies with the inverse third power of distance $|z|$.

- Also, B_x and B_z integrals can be performed numerically. Figure in the margin depicts the pattern of \hat{B} on $y = 0$ plane for a loop of radius $a = 1$ computed using *Mathematica*.

- Note that circulation $\oint_C \mathbf{B} \cdot d\mathbf{l}$ around each closed field line (“linking” the current loop) equals a fixed value of $\mu_o I$ — this dictates that the average field strength $|\mathbf{B}|$ of a current loop is stronger on shorter field lines closer to the current loop than on longer field lines linking the loop further out. As a result $|\mathbf{B}|$ can be shown to vary as r^{-3} for large r .
- It can be shown that the equations for magnetic *field lines* of a current loop on, say, $y = 0$ plane, can be expressed as

$$r = L \sin^2 \theta$$

in terms of **radial distance** r from the origin and **zenith angle** θ measured from the z axis. Clearly, parameter L in this formula is the



radial distance of the field line on $\theta = 90^\circ$ plane, and the field line formula is accurate only for $r \gg a$. The Earth's magnetic field had such a **magnetic dipole** topology as shown.

- Lorentz force due to the magnetic fields of a pair of current loops — also known as *magnetic dipoles* — turns out to be “attractive” when the current directions agree (see margin). Bar magnets carrying “equivalent” current loops of atomic origins interact with one another in exactly the same way — i.e., as governed by the second term of Lorentz force.

