Charge Distributions

The geometries that we have looked and determined the associated electric field are all examples of "charge distributions".

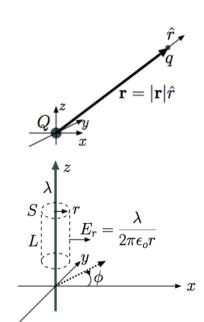
We have made assumptions about how these distributions relate to points charges.

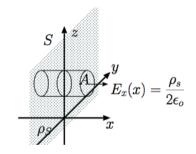
Macroscopic view:

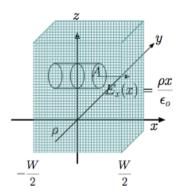
- we are not interested in the fields very close to the charge distribution which is really made up of point charges. We know that the fields near the collection of charges varies quickly, but these variations disappear quickly as you move away from the distribution.

Microscopic view:

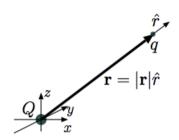
- we are interested in the fine details of structure of the fields and so need to identify the exact placement of each charge and its contribution to the total field.





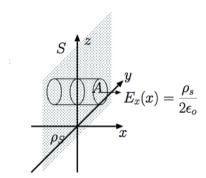


Charge Distributions



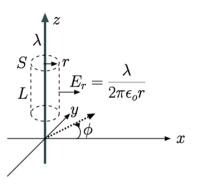
Point Charge at point (x,y,z)

$$Q\delta(x,y,z)$$



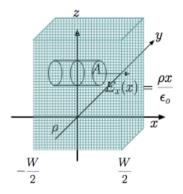
Sheet of charge in y-z plane

$$\rho_s \delta(x)$$



Line Charge along the z-axis

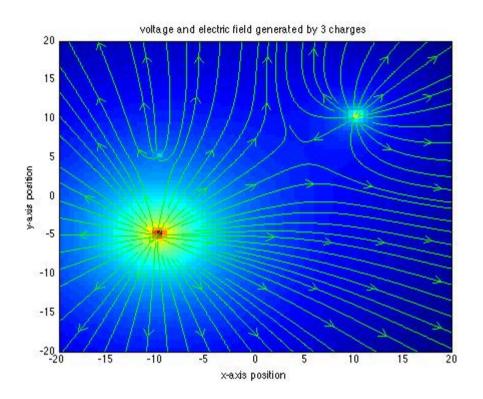
$$\rho_l \delta(x, y)$$

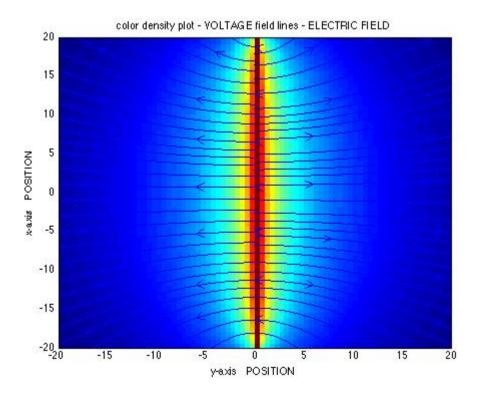


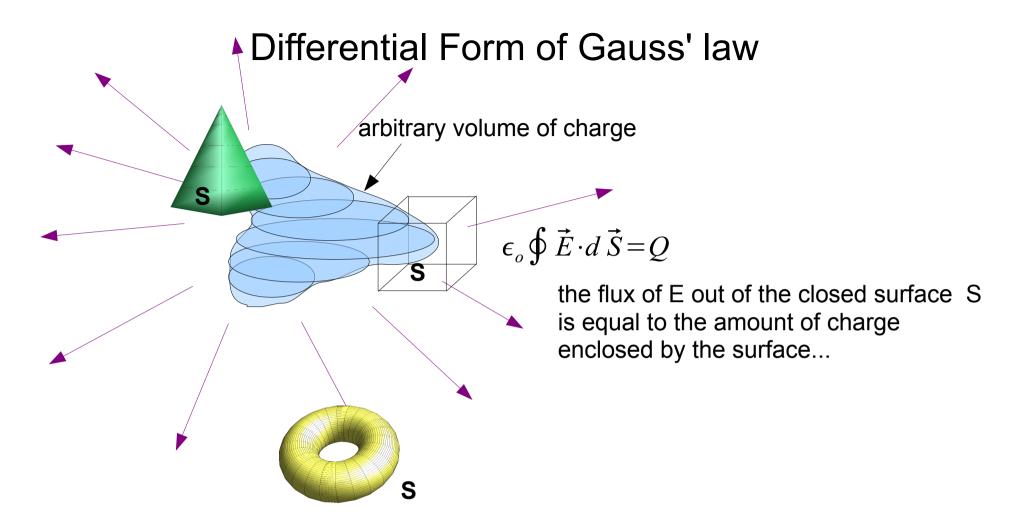
volume of charge

$$\rho_{v}$$

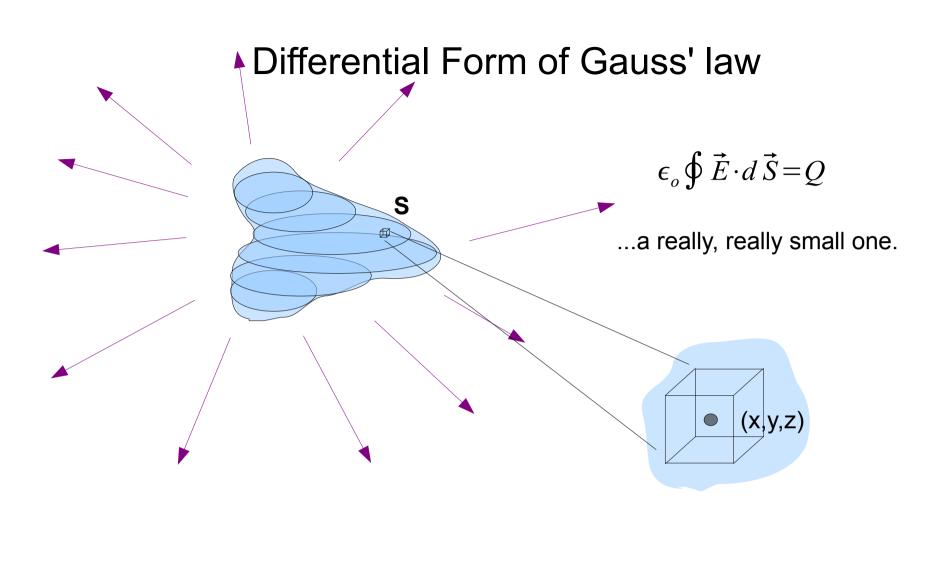
Charge Distributions







...any surface of any shape, even...



$$\vec{E} = E_x(x + \frac{dx}{2}, y, z)\hat{x} + E_y(x + \frac{dx}{2}, y, z)\hat{y} + E_z(x + \frac{dx}{2}, y, z)\hat{z}$$
 Let's compute the election out of each of the 6 factors.

 $d\vec{S} = dy dz \hat{x}_{dx}$

dy

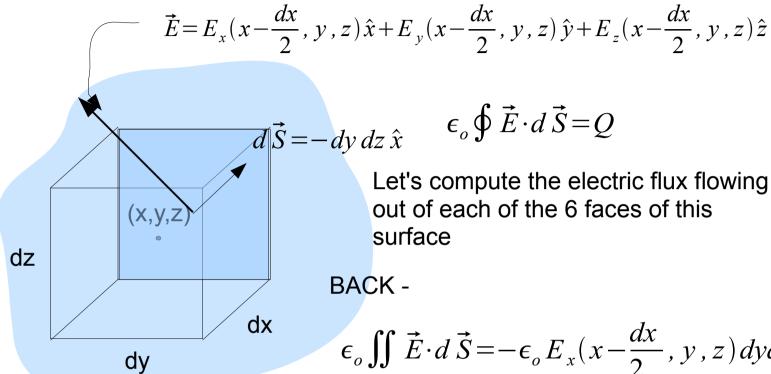
dz

Let's compute the electric flux flowing out of each of the 6 faces of this surface

FRONT -

$$\epsilon_o \iint \vec{E} \cdot d\vec{S} = \epsilon_o E_x (x + \frac{dx}{2}, y, z) dy dz$$

what assumption did we make?



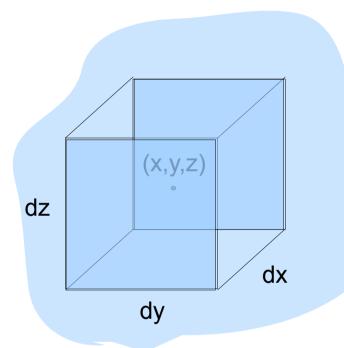
$$\vec{d} \vec{S} = -dy \, dz \, \hat{x} \qquad \epsilon_o \oint \vec{E} \cdot d\vec{S} = Q$$

Let's compute the electric flux flowing out of each of the 6 faces of this surface

BACK -

$$\epsilon_o \iint \vec{E} \cdot d\vec{S} = -\epsilon_o E_x(x - \frac{dx}{2}, y, z) dy dz$$

what assumption did we make?



$$\epsilon_o \oint \vec{E} \cdot d\vec{S} = Q$$

Let's compute the electric flux flowing out of each of the 6 faces of this surface

FRONT -

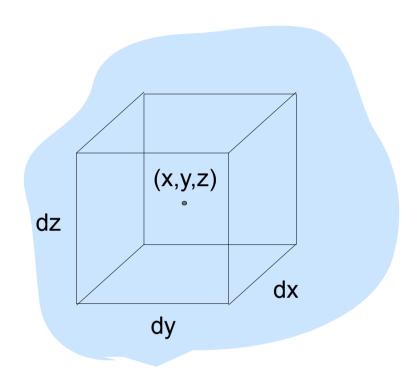
$$\epsilon_o \iint \vec{E} \cdot d\vec{S} = \epsilon_o E_x (x + \frac{dx}{2}, y, z) dy dz$$

combining: electric flux flowing through the volume in the x-direction

BACK -

$$\epsilon_o \iint \vec{E} \cdot d\vec{S} = -\epsilon_o E_x(x - \frac{dx}{2}, y, z) dy dz$$

$$\epsilon_o(E_x(x+\frac{dx}{2},y,z)-E_x(x-\frac{dx}{2},y,z))dydz$$

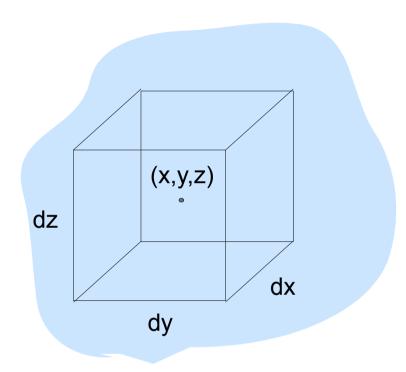


$$\epsilon_o \oint \vec{E} \cdot d\vec{S} = Q$$

Let's compute the electric flux flowing out of each of the 6 faces of this surface

Repeat for the y- and z- directions

$$\begin{split} \epsilon_o \oint \vec{E} \cdot d\,\vec{S} &= & \epsilon_o (E_x(x + \frac{dx}{2}, y, z) - E_x(x - \frac{dx}{2}, y, z)) \, dy \, dz + \\ & \epsilon_o (E_y(x, y + \frac{dy}{2}, z) - E_y(x, y - \frac{dy}{2}, z)) \, dx \, dz + \\ & \epsilon_o (E_z(x, y, z + \frac{dz}{2}) - E_z(x, y, z - \frac{dz}{2})) \, dx \, dy \end{split}$$

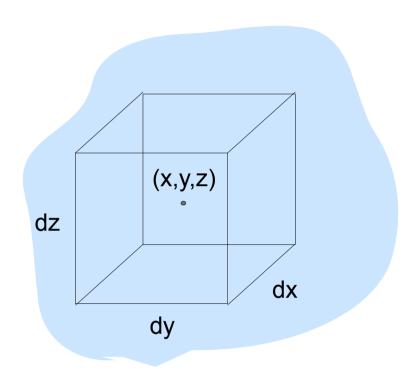


$$\epsilon_o \oint \vec{E} \cdot d\vec{S} = Q$$

Now compute the total charge contained in the volume defined by the small surface

 $Q_{total} = \rho_v \, dx \, dy \, dz$

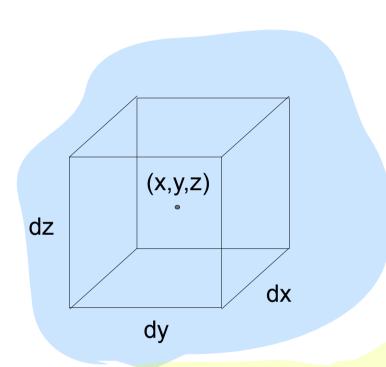
again, what assumption did we make?



$$\epsilon_o \oint \vec{E} \cdot d\vec{S} = Q$$

Repeat for the y- and z- directions

$$\begin{split} \epsilon_o \oint \vec{E} \cdot d\vec{S} &= \quad \epsilon_o(E_x(x + \frac{dx}{2}, y, z) - E_x(x - \frac{dx}{2}, y, z)) \, dy \, dz + \quad = \quad \rho_v \, dx \, dy \, dz \\ \epsilon_o(E_x(x, y + \frac{dy}{2}, z) - E_x(x, y - \frac{dy}{2}, z)) \, dx \, dz + \\ \epsilon_o(E_x(x, y, z + \frac{dz}{2}) - E_x(x, y, z - \frac{dz}{2})) \, dx \, dy \end{split}$$



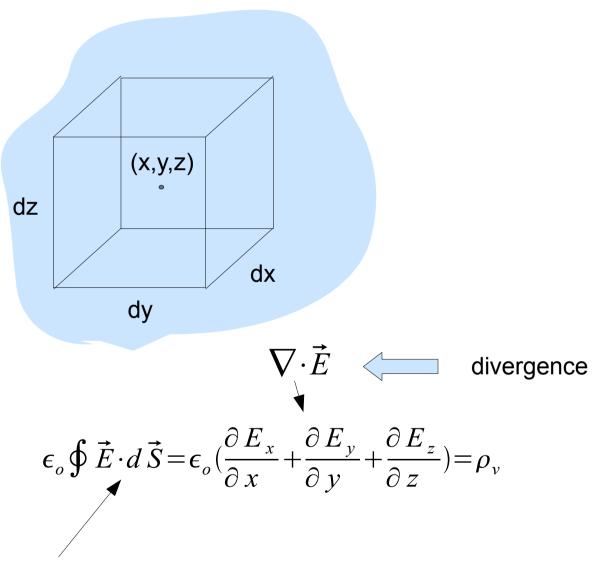
remember - from your early calculus class – the definition of a partial derivative

$$\frac{\partial f(x, y, z)}{\partial x} = \lim \frac{f(x+dx, y, z) - f(x, y, z)}{dx}$$

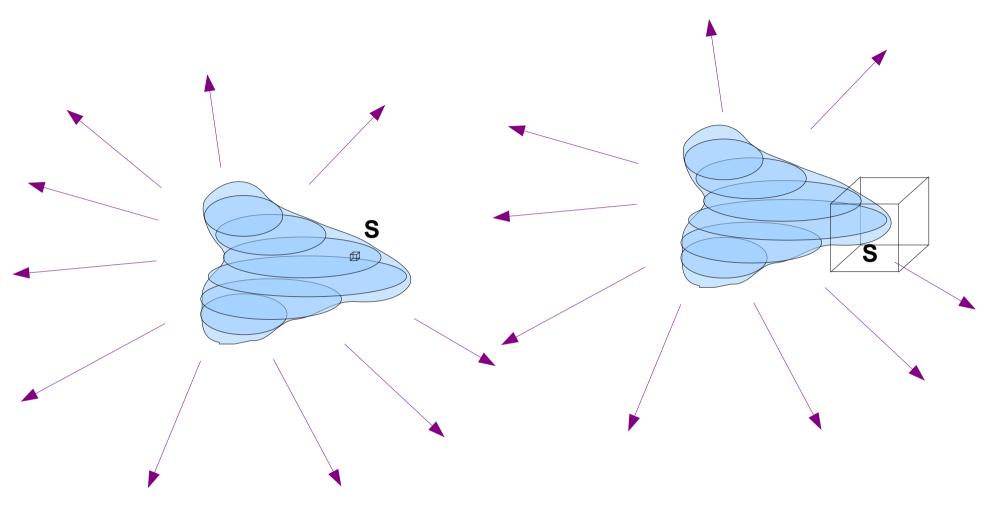
or equivalently,

$$\frac{\partial f(x,y,z)}{\partial x} = \lim \frac{f(x + \frac{dx}{2}, y, z) - f(x - \frac{dx}{2}, y, z)}{dx}$$

$$\epsilon_{o} \oint \vec{E} \cdot d\vec{S} = \underbrace{\frac{(E_{x}(x + \frac{dx}{2}, y, z) - E_{x}(x - \frac{dx}{2}, y, z))}{dx}}_{\epsilon_{o}} + \underbrace{\frac{(E_{y}(x, y + \frac{dy}{2}, z) - E_{y}(x, y - \frac{dy}{2}, z))}{dy}}_{\epsilon_{o}} + \underbrace{\frac{\partial E_{x}}{\partial x}}_{\epsilon_{o}}$$



over an infinitesimally small volume

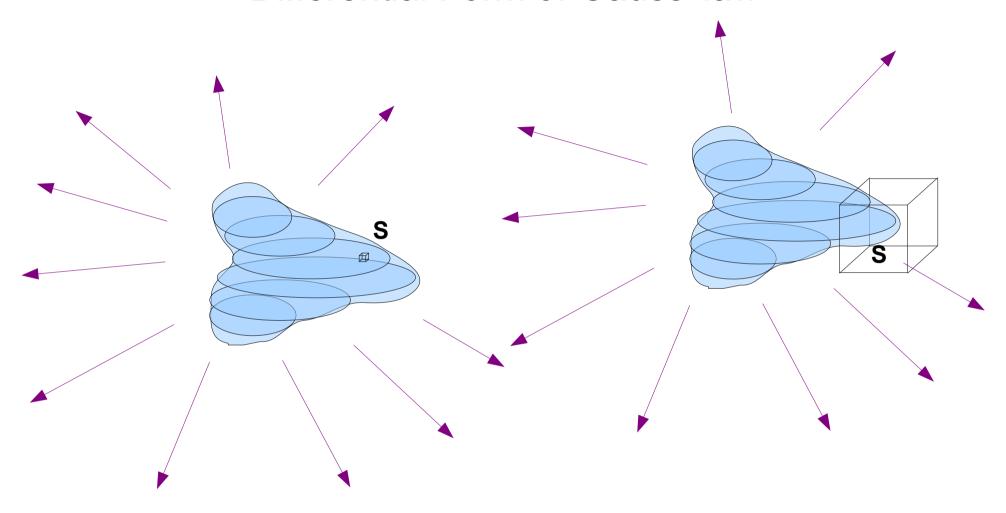


Differential Form of Gauss' Law

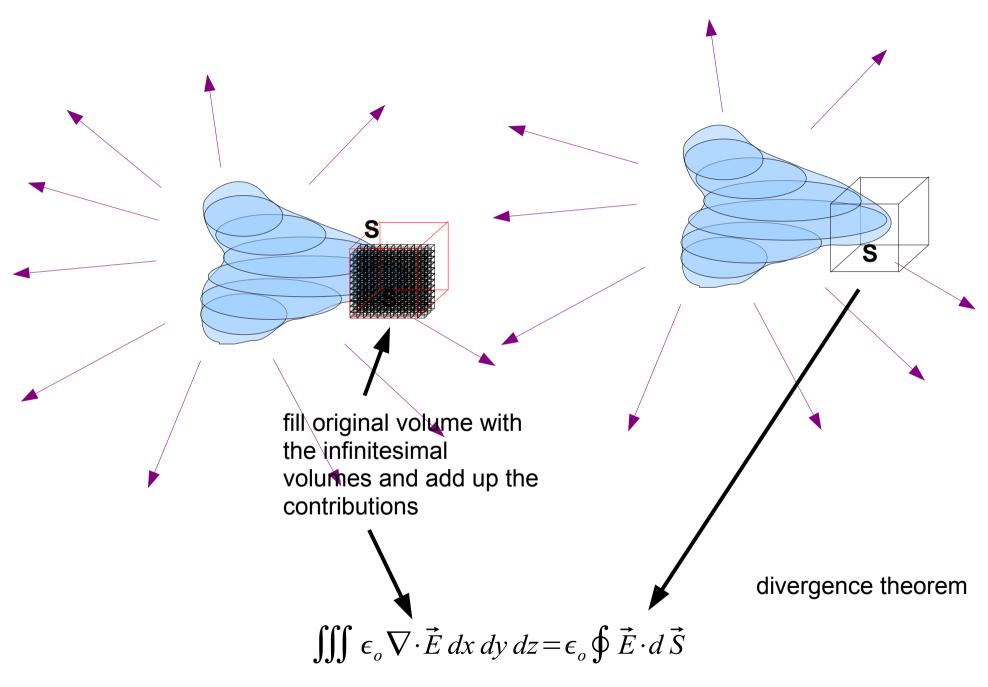
$$\epsilon_o \nabla \cdot \vec{E} = \rho_v$$

Integral Form of Gauss' Law

$$\epsilon_o \oint \vec{E} \cdot d\vec{S} = Q$$



$$\iiint \epsilon_o \nabla \cdot \vec{E} \, dx \, dy \, dz = \epsilon_o \oint \vec{E} \cdot d\vec{S}$$



Maxwell's Equations static fields

$$\nabla \cdot \vec{D} = \rho$$

Gauss' Law for the electric field

$$\oint \vec{D} \cdot d\vec{S} = Q$$

$$\nabla \cdot \vec{B} = 0$$

Gauss' Law for the magnetic field

$$\oint \vec{B} \cdot d\vec{S} = 0$$

$$\nabla \times \vec{E} = \frac{-\partial B}{\partial t}$$

$$\oint \vec{E} \cdot d \vec{l} = -\frac{\partial}{\partial t} \oint \vec{B} \cdot d \vec{S}$$

$$\nabla \times \vec{H} = \frac{\partial D}{\partial t} + \vec{J}$$

$$\oint \vec{H} \cdot d\vec{l} = \frac{\partial}{\partial t} \oint \vec{D} \cdot d\vec{S} + I$$

static fields

late sources to fields	constrains the field

$$\nabla \cdot \vec{D} = \rho$$

Gauss' Law for the electric field

$$\oint \vec{E} \cdot d\vec{S} = Q$$

$$\nabla \cdot \vec{B} = 0$$

Gauss' Law for the magnetic field

$$\oint \vec{B} \cdot d\vec{S} = 0$$

$$\nabla \times \vec{E} = 0$$

$$\oint \vec{E} \cdot d \vec{l} = 0$$

$$\nabla \times \vec{H} = \vec{J}$$

$$\oint \vec{H} \cdot d \vec{l} = I$$

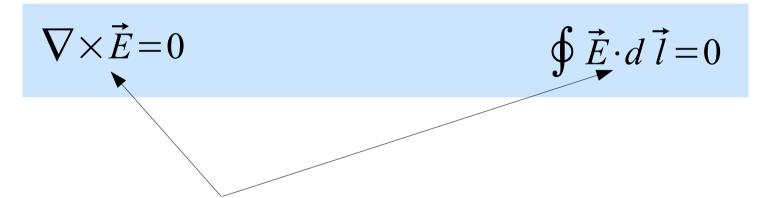
static electric fields

$$\nabla \cdot \vec{D} = \rho$$

Gauss' Law for the electric field

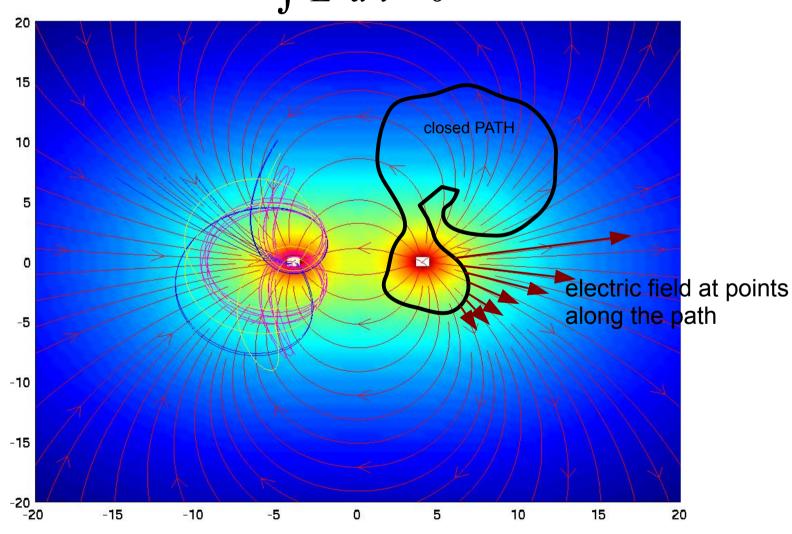
$$\oint \vec{D} \cdot d\vec{S} = Q$$

we know that Gauss' Law tells us that the electric field in any region is related to its source (electrical charges) in a special way. Because all electric fields are generated by charge distributions, if you look at the electric flux through a closed surface it is directly related to the enclosed charge.

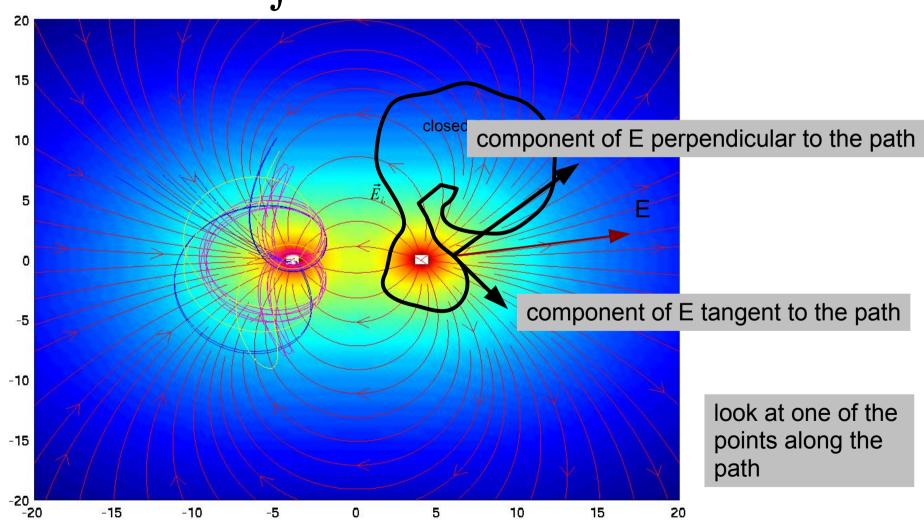


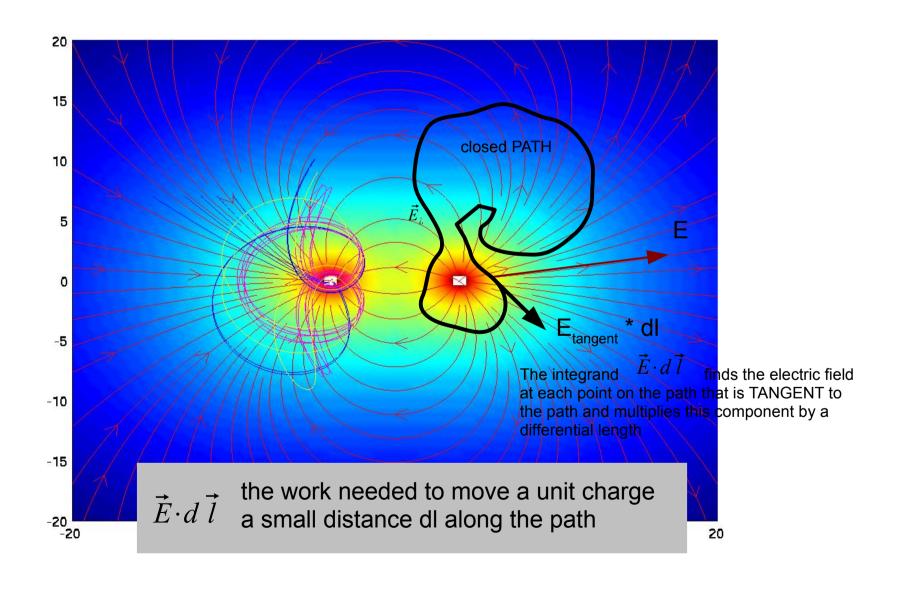
What do these equations tell us?

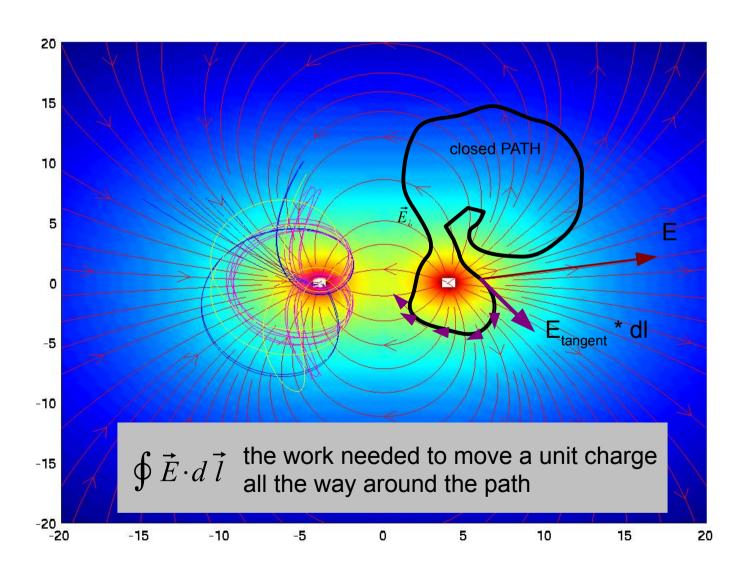
$$\oint \vec{E} \cdot d \vec{l} = 0$$



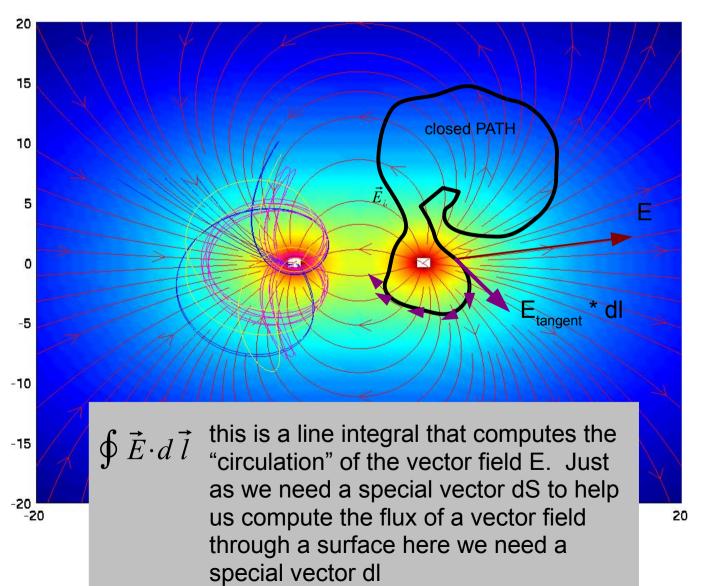
$$\oint \vec{E} \cdot d \vec{l} = 0$$







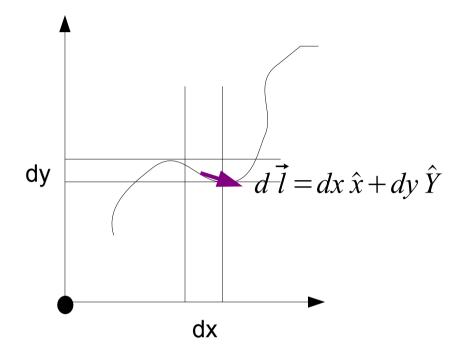
static electric fields



 $d\vec{l}$

magnitude specifies an infinitesimal increment of the path

direction specifies a direction TANGENT to the path



static electric fields

lf

 $\oint \vec{E} \cdot d \, \vec{l}$ the work needed to move a unit charge all the way around the path

is correct then

$$\oint \vec{E} \cdot d \vec{l} = 0$$

states that the amount of work needed to move a

unit charge all the way around the path is 0!?!?!

static electric fields

lf

 $\oint \vec{E} \cdot d \vec{l}$ the work needed to move a unit charge all the way around the path

is correct then

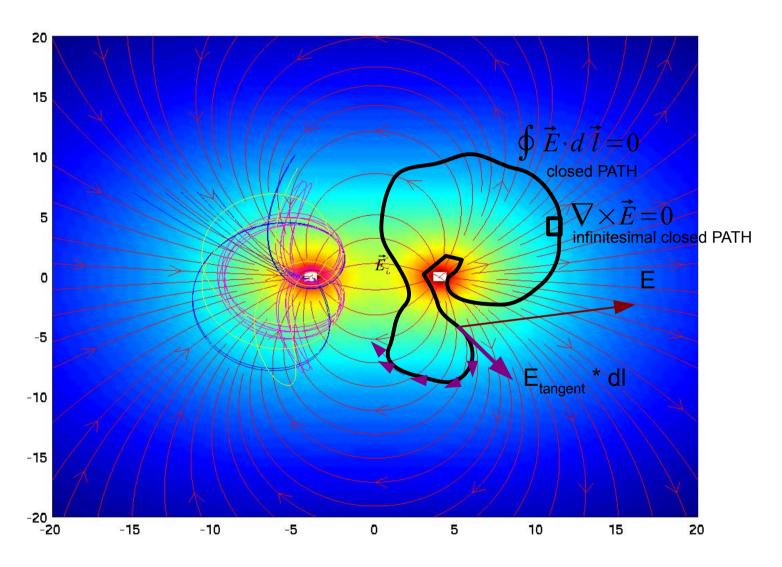
$$\oint \vec{E} \cdot d \vec{l} = 0$$

states that the amount of work needed to move a

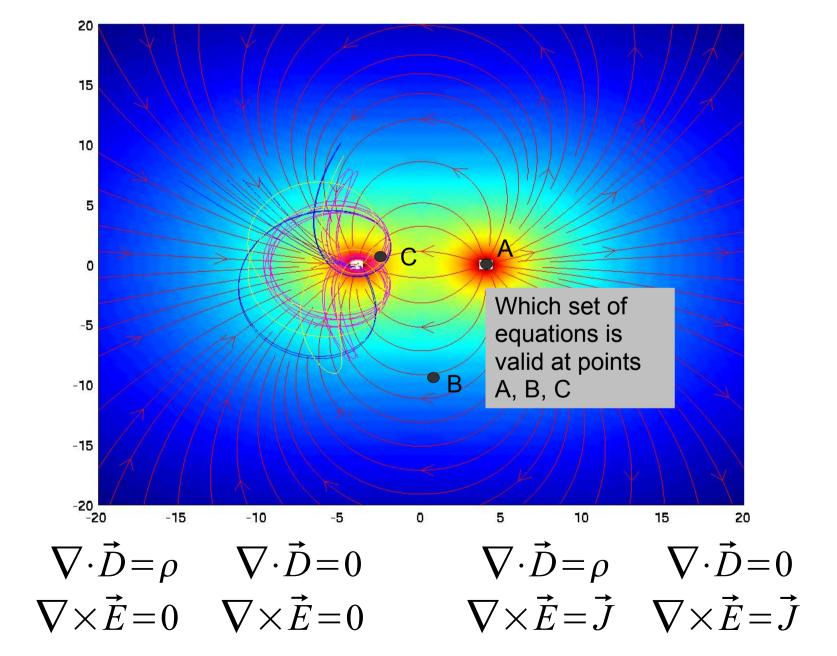
unit charge all the way around the path is 0!?!?!

CONSERVATIVE FIELD

...and just as $\nabla \cdot \vec{D} = \rho$ is equivalent to $\oint \vec{D} \cdot d\vec{S} = Q$ over an infinitely small surface



so $\nabla \times \vec{E} = 0$ is equivalent to $\oint \vec{E} \cdot d \vec{l} = 0$ over an infinitely small path.



Example 1: Find the divergence of $\mathbf{D} = \hat{x}5x + \hat{y}12 \text{ C/m}^2$

Solution: In this case

$$D_x = 5x$$
, $D_y = 12$, and $D_z = 0$.

Therefore, divergence of \mathbf{D} is

$$\nabla \cdot \mathbf{D} = \frac{\partial D_x}{\partial x} + \frac{\partial D_y}{\partial y} + \frac{\partial D_z}{\partial z}$$

$$= \frac{\partial}{\partial x} (5x) + \frac{\partial}{\partial y} (12) + \frac{\partial}{\partial z} (0)$$

$$= 5 + 0 + 0 = 5 \frac{C}{m^3}.$$

Note that the divergence of vector **D** is a scalar quantity which is the volumetric charge density in space as a consequence of Gauss's law (in differential form).

Example 3: Find the curl of the vector field

$$\mathbf{E} = \hat{x}\cos y + \hat{y}\mathbf{1}$$

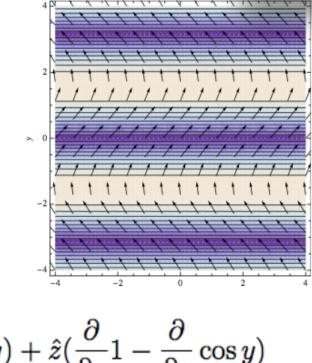
Solution: The curl is

$$abla imes extbf{E} = egin{bmatrix} \hat{x} & \hat{y} & \hat{z} \ rac{\partial}{\partial x} & rac{\partial}{\partial y} & rac{\partial}{\partial z} \ \cos y & 1 & 0 \ \end{pmatrix}$$

$$= \hat{x}(\frac{\partial}{\partial y}0 - \frac{\partial}{\partial z}1) - \hat{y}(\frac{\partial}{\partial x}0 - \frac{\partial}{\partial z}\cos y) + \hat{z}(\frac{\partial}{\partial x}1 - \frac{\partial}{\partial y}\cos y)$$

$$= \hat{x}0 - \hat{y}0 + \hat{z}(0 + \sin y) = \hat{z}\sin y$$

which is another vector field.



CURL-free and DIVERGENCE free