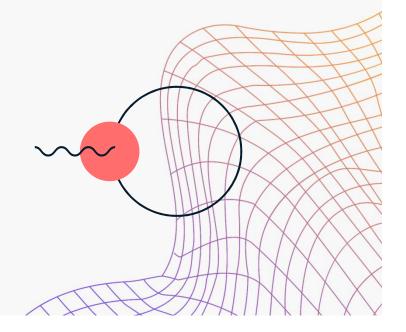
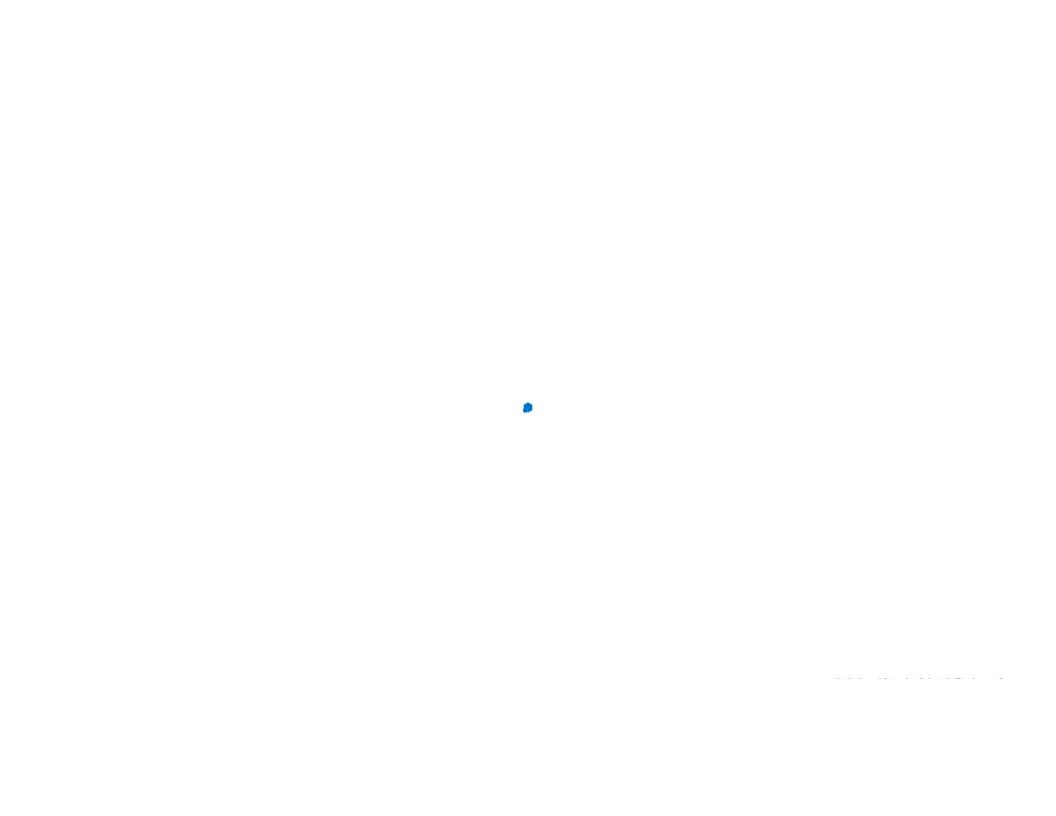


ECE329: Exam 3 Review Session

November 20th, 2025





Exam 3 Content

- Poynting Theorem
- Phasors
- TEM Wave Propagation in Material Media
- Polarization
- Standing Waves
- Bounce Diagrams & TLs

Poynting Vector & Theorem

 $\vec{S} = \vec{E} \times \vec{H}$. Units: W/m². "Instantaneous" power per unit area passing through surface in direction of \vec{S}

Energy unit volume balance equation:

$$\frac{\partial}{\partial t} \left(\frac{1}{2} \epsilon \vec{E} \cdot \vec{E} + \frac{1}{2} \mu \vec{H} \cdot \vec{H} \right) + \nabla \cdot \vec{S} + \vec{J} \cdot \vec{E} = 0$$
Total EM

Source

Fields

Fields

Phasor Notation

$$\vec{E}(x,t) = A\cos(\omega t - \beta x)\hat{z} = \text{Re}\{Ae^{j\omega t}e^{-j\beta x}\hat{z}\} \longleftrightarrow Ae^{-j\beta x}\hat{z} = \tilde{E}(x)$$
Time domain
Phasor

$$\sin(x) = \cos\left(x - \frac{\pi}{2}\right)$$

Time-Averaging

If TEM wave \vec{E} is cosinusoidal,

- Then corresponding \vec{H} is cosinusoidal
- Then phasors \tilde{E} and \tilde{H} exist
- Also, $\vec{S} = \vec{E} \times \vec{H}$ (instantaneous power per unit area) is cosinusoidal squared
- We can write \vec{S} in phasor form too: $\tilde{S} = \tilde{E} \times \tilde{H}^*$
- Time-average of cosinusoidal squared is ½ of the magnitude of the cosinusoidal:

$$\langle \vec{S} \rangle = \frac{1}{2} \operatorname{Re} \{ \tilde{E} \times \tilde{H}^* \}$$

$$\frac{1}{2} \operatorname{Re} \{ V F^* \}$$

Wave Equation in Material Media (Notar)

Assumptions: $\rho = 0$, $\vec{J} = 0$, i.e. region is a source-free. $\sigma \neq 0$ now!

Wave equation: $\nabla^2 \tilde{E} = (j\omega\mu)(\sigma + j\omega\epsilon)\tilde{E}$. Solutions are TEM waves. \vec{E} and \vec{H} point **perpendicular** to the direction of travel.

General form of cosinusoidal solution:
$$\hat{E} = A e^{-\lambda^{2}} e^{-j\beta^{2}} e^{j\phi} \hat{A}$$

$$\hat{E} = A \cos(\omega t - \beta^{2} - \phi) e^{-\lambda^{2}} \hat{A}$$

$$\hat{E} = A \cos(\omega t - \beta^{2} - \phi) e^{-\lambda^{2}} \hat{A}$$

Getting H from E $N = |Ne^{j\pi}|$ $\exists x \vec{R} = -\hat{g}$

$$\vec{E} = Ae^{\alpha y}\cos(\omega t + \beta y + \phi)\,\hat{x}\,[V/m]$$

$$\vec{E} = Ae^{\alpha y}e^{j\beta y}e^{j\phi}\hat{x} \text{ [V/m]}$$

$$\vec{A} e^{\lambda \gamma}e^{j\beta z}e^{j\phi}\hat{x} \text{ [V/m]}$$

Getting E from H

$$\vec{H} = Ae^{\alpha y}\cos(\omega t + \beta y + \phi)\hat{x} [A/m]$$

$$\vec{E} = Ae^{\alpha y} [M] \cos(\omega t + \beta y + \phi + \gamma)\hat{z} \frac{y}{h}$$

$$\vec{H} = Ae^{\alpha y}e^{j\beta y}e^{j\phi}\hat{x} [A/m]$$

$$A|\mathcal{N}|e^{\lambda y}e^{j\beta y}e^{j\phi}\hat{x} [A/m]$$

EXACT Formulae

$$\gamma = \sqrt{(j\omega\mu)(\sigma + j\omega\epsilon)}$$

$$\gamma \eta = j\omega \mu$$

$$\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$$

$$\frac{\gamma}{\eta} = \sigma + j\omega\epsilon$$

APPROXIMATE Formulae

	Condition	β	α	$ \eta $	au	$\lambda = \frac{2\pi}{\beta}$	$\delta = \frac{1}{\alpha}$
Perfect	$\sigma = 0$	$\omega\sqrt{\epsilon\mu}$	0	<u>/µ</u>	0	2π	∞
dielectric	0 - 0	ωγιμ	O	$\sqrt{\epsilon}$	U	$\frac{2\pi}{\omega\sqrt{\epsilon\mu}}$	\sim
Imperfect	<u>σ</u> // 1	21/12/611	$\beta \underline{1} \underline{\sigma} \underline{\sigma} / \underline{\mu}$	$\sim \sqrt{rac{\mu}{\epsilon}}$	σ, σ	2π	$\frac{2}{2}$ $\sqrt{\epsilon}$
dielectric	$\frac{\sigma}{\omega\epsilon} \ll 1$	$\sim \omega \sqrt{\epsilon \mu}$	$\beta \frac{1}{2} \frac{\sigma}{\omega \epsilon} = \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}$	$\sqrt{\frac{\epsilon}{\epsilon}}$	$\sim \frac{\sigma}{2\omega\epsilon}$	$\sim \frac{2\pi}{\omega\sqrt{\epsilon\mu}}$	$\frac{2}{\sigma}\sqrt{\frac{\epsilon}{\mu}}$
Good	$\sigma \sim 1$	$a = \sqrt{\pi} f u \sigma$	$\sim \sqrt{\pi f \mu \sigma}$	$\sqrt{\frac{\omega\mu}{\sigma}}$	45°	2π	1
conductor	$\frac{\sigma}{\omega\epsilon} \gg 1$	$\sim \sqrt{\pi f \mu \sigma}$	$\sim \sqrt{\pi J \mu o}$	$\sqrt{\sigma}$	40	$\sim \frac{2\pi}{\sqrt{\pi f \mu \sigma}}$	$\sim \frac{1}{\sqrt{\pi f \mu \sigma}}$
Perfect	$\sigma - \infty$	~	~	0		0	0
conductor	$\sigma = \infty$	∞	∞	U		U	U

Wave Polarization

Polarization is how the tip of \vec{E} varies over time.

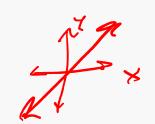
Linear: In phase 0° -- 180° D\$

Acos(wt-132)+Bcos(wt-132) Circular: 90 degrees out-of-phase with equal magnitude

- Right-Handed
- Left-Handed

Elliptical: Anything else

Wave Polarization



Example of linear polarization: $\vec{E} = 3\cos(\omega t - \beta z)\hat{x}$

Example of right-handed circular polarization (RHCP):

$$\vec{E} = 3\cos(\omega t - \beta z)\hat{x} + 3\cos(\omega t - \beta z - \frac{\pi}{2})\hat{y}$$

Aheas Ex Beligs Ez = prop. dir > PHCP

Example of left-handed circular polarization (LHCP):

$$\vec{E} = 3\cos(\omega t - \beta z)\hat{x} - 3\cos(\omega t - \beta z - \frac{\pi}{2})\hat{y}$$

Wave Polarization

Example of elliptical polarization:

$$\vec{E} = 3\cos(\omega t - \beta z)\hat{x} + \cos\left(\omega t - \beta z - \frac{\pi}{2}\right)\hat{y}$$

Example of elliptical polarization:

$$\vec{E} = 3\cos(\omega t - \beta z)\hat{x} + 3\cos(\omega t - \beta z - \frac{\pi}{3})\hat{y}$$

What about this?

$$\vec{E} = 2\cos(\omega t - \beta z)\hat{x} + 4\cos(\omega t - \beta z)\hat{y}$$

Wave Polarization Example

Find the polarization of:

$$\vec{E} = 3\cos(\omega t + \beta x)\hat{z} - 3\cos(\omega t + \beta x - \frac{\pi}{2})\hat{y}$$

$$\vec{w} \times 50 \quad 3\cos(\omega t + \beta x)\hat{z} - 3\cos(\omega t - \frac{\pi}{2})\hat{y}$$

$$\vec{w} \times 50 \quad 3\cos(\omega t + \beta x)\hat{z} - 3\sin(\omega t - \frac{\pi}{2})\hat{y}$$

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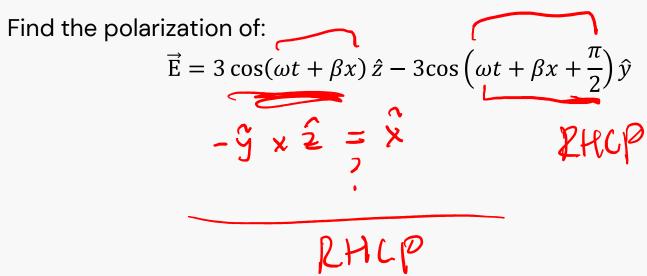
$$\vec{w} \times 50 \quad 3\cos(\omega t + \beta x)\hat{z} - 3\cos(\omega t - \frac{\pi}{2})\hat{y}$$

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$$\vec{w} \times 50 \quad 3\cos(\omega t + \beta x)\hat{z} - 3\cos(\omega t - \frac{\pi}{2})\hat{y}$$

$$\vec{w} \times 50 \quad 3\cos(\omega t - \frac{\pi}{2})\hat{y}$$

Wave Polarization Example



Wave Reflection & Transmission

TEM wave incident normally on a boundary

$$\widetilde{E}_{i}(x) = E_{0}e^{-\alpha_{1}x}e^{-j\beta_{1}x}\widehat{y}$$

$$\widetilde{H}_{i}(x) = \frac{E_{0}}{\eta_{1}}e^{-\alpha_{1}x}e^{-j\beta_{1}x}\widehat{z}$$





$$\sigma_1, \mu_1, \epsilon_1$$
 $x < 0$

$$x = 0$$

$$\sigma_2, \mu_2, \epsilon_2$$

 $x > 0$

Reflection & Transmission Coefficients

$$\widetilde{E}_i(x) = E_0 e^{-\alpha_1 x} e^{-j\beta_1 x} \widehat{y}$$

$$\widetilde{H}_i(x) = \frac{E_0}{\eta_1} e^{-\alpha_1 x} e^{-j\beta_1 x} \widehat{z}$$

$$\widetilde{E}_{r}(x) = E_{\circ} \Gamma e^{+\lambda_{1} \times} e^{+j\beta_{1} \times} \mathring{\gamma}$$

$$\widetilde{H}_{r}(x) = -E_{\circ} \Gamma e^{+\lambda_{1} \times} e^{+j\beta_{1} \times} \mathring{z}$$

$$\sigma_1, \mu_1, \epsilon_1$$
 $x < 0$

$$\tilde{E}_{t}(x) = \mathcal{L} E_{o} e^{-\lambda_{2} x} - \tilde{\beta}_{1} x$$

$$\widetilde{H}_t(x) = \underbrace{\gamma E_o}_{t} e^{-\lambda r^{\chi}} - \widetilde{j} \beta r^{\chi} \widehat{z}$$

$$\sigma_2, \mu_2, \epsilon_2$$

 $x > 0$

Summary

$$\widetilde{E}_i(x) = E_0 e^{-\alpha_1 x} e^{-j\beta_1 x} \widehat{y}$$

$$\widetilde{H}_i(x) = \frac{E_0}{\eta_1} e^{-\alpha_1 x} e^{-j\beta_1 x} \widehat{z}$$

$$\widetilde{E}_r(x) = E_0 \Gamma e^{\alpha_1 x} e^{j\beta_1 x} \widehat{y}$$

$$\widetilde{H}_r(x) = -\frac{E_0}{\eta_1} \Gamma e^{\alpha_1 x} e^{j\beta_1 x} \widehat{z}$$

$$\sigma_1, \mu_1, \epsilon_1 \\ x < 0$$

$$\tilde{E}_t(x) = E_0 \tau e^{-\alpha_2 x} e^{-j\beta_2 x} \hat{y}$$

$$\widetilde{H}_t(x) = \frac{E_0}{\eta_2} \tau e^{-\alpha_2 x} e^{-j\beta_2 x} \hat{z}$$



$$\sigma_2, \mu_2, \epsilon_2$$

 $x > 0$

Coefficients

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$
 $\tau = \frac{2\eta_2}{\eta_2 + \eta_1} = 1 + \Gamma$

Check our work:

1. What if $\eta_1 = \eta_2$?

2. What if $\eta_2 = 0$?

Standing Waves (dielectric to PEC)

$$\widetilde{E}_{i}(y) = -E_{0}e^{-j\beta_{1}y}\hat{x}$$

$$\widetilde{E}_{r}(y) = E_{0}e^{j\beta_{1}y}\hat{x}$$

$$\widetilde{E}_{r}(y) = E_{0}e^{j\beta_{1}y}\hat{x}$$

$$E_{tot} = \widetilde{E}_{i}(y) + \widetilde{E}_{r}(y)$$

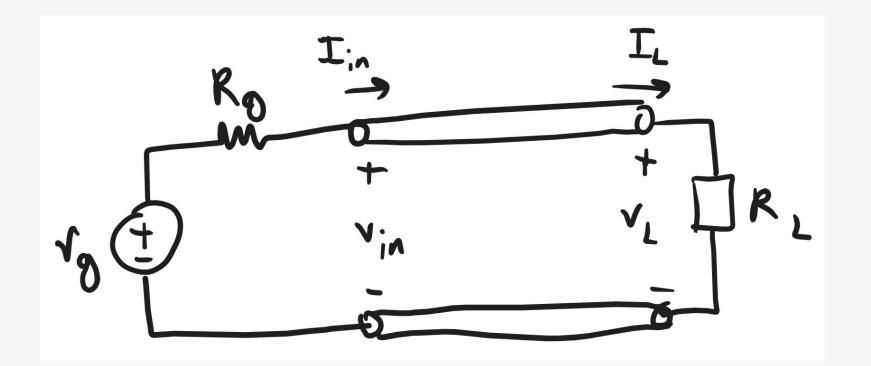
$$E_{tot} = \widetilde{E}_{r}(y) = E_{0}e^{j\beta_{1}y}\hat{x}$$

$$E_{tot} = E_{0}e^{j$$

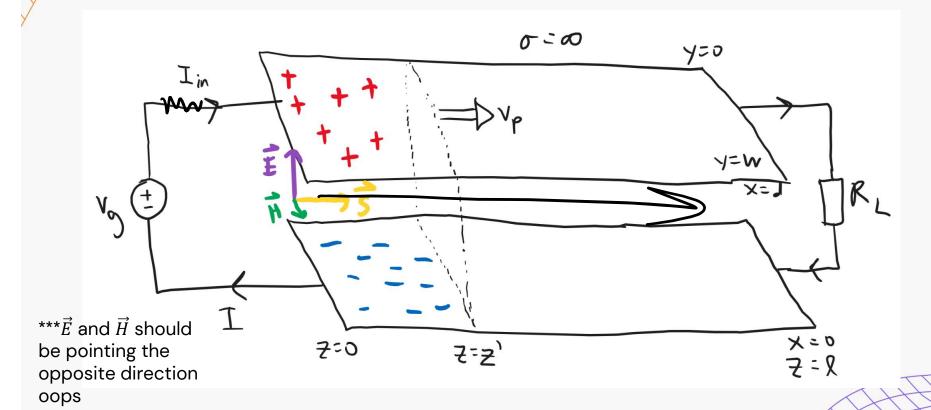
Transmission Lines!

Why do we care?

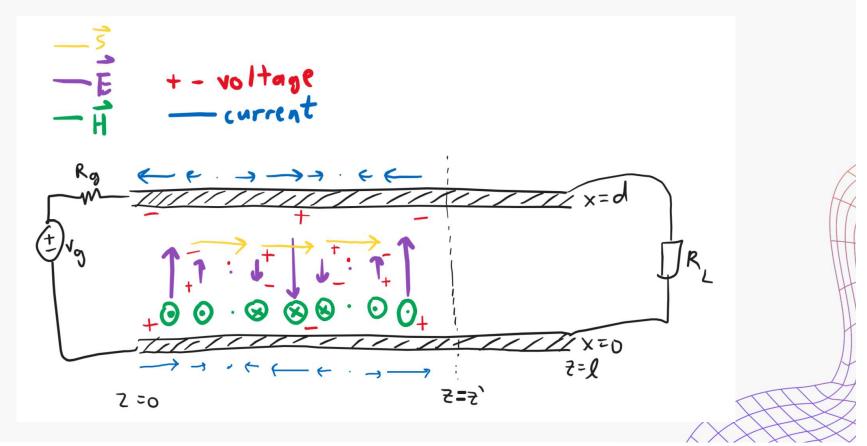
Transmission Line

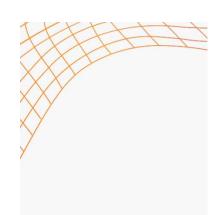


Transmission Line: Parallel Plate Version

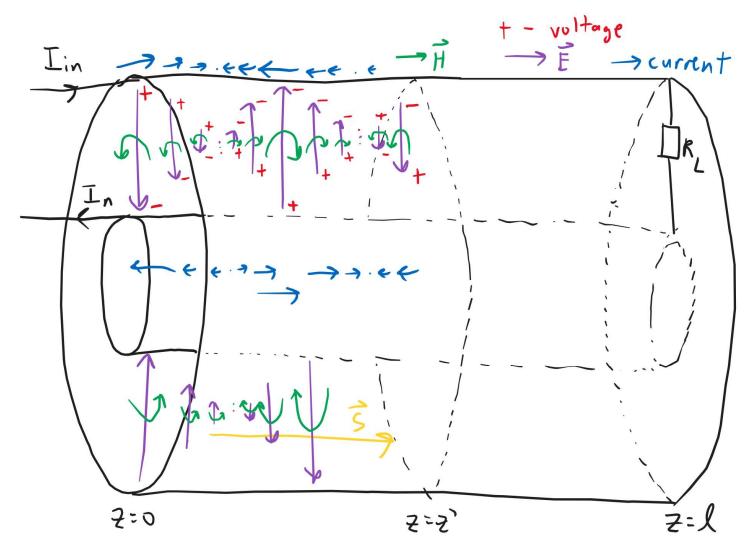


Transmission Line: Parallel Plate Version





Coax Version:



Basic TL: Time Domain, Not Steady State

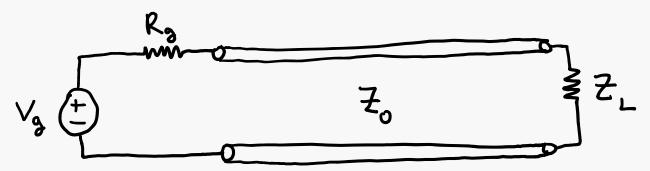


Generator injection coefficient: $\tau_g = \frac{Z_0}{R_g + Z_0} \neq 1 + \Gamma_g$

Load reflection coefficient: $\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0}$

Generator reflection coefficient: $\Gamma_g = \frac{R_g - Z_0}{R_g + Z_0}$

Basic TL: Time Domain, Not Steady State



Special cases:

What if $Z_L = \infty$?

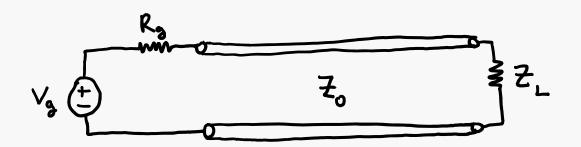
What if $Z_L = Z_0$?



Bounce Diagram Example

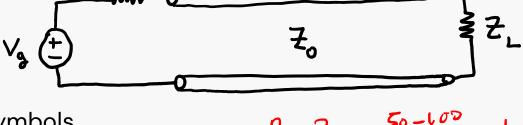
Input: $V_g = 50\delta(t)$ [V] $Z_L = 25\Omega$, $R_g = 50\Omega$, $Z_0 = 100\Omega$ $v = \frac{2}{3}c$, TL length = 4 [m].

Create a voltage bounce diagram for the first 70ns. Create a current bounce diagram for the first 70ns. Plot V(1m, t) for the first 7us.



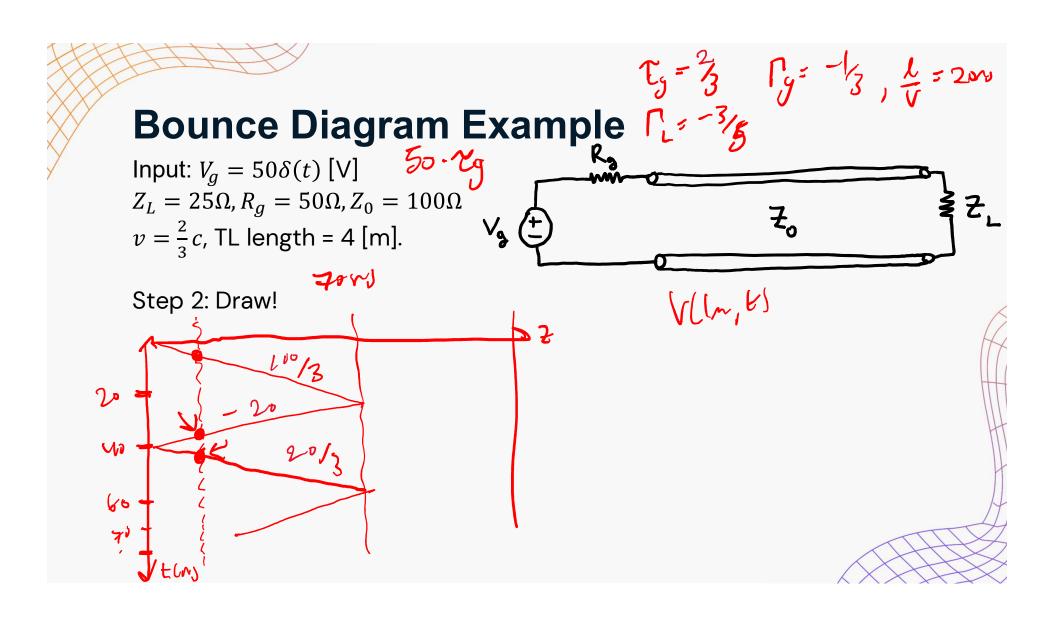
Bounce Diagram Example

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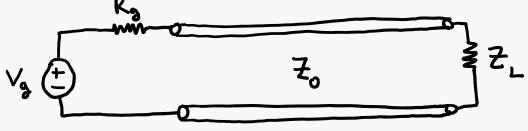
Step 1: Calculate all the funny symbols

$$r_{y} = r_{y} = r_{y$$

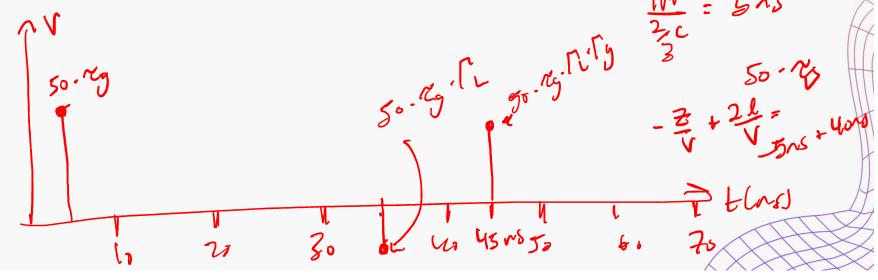




Input: $V_g = 50\delta(t)$ [V] $Z_L = 25\Omega$, $R_g = 50\Omega$, $Z_0 = 100\Omega$ $v = \frac{2}{3}c$, TL length = 4 [m].

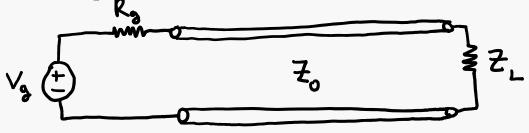


Plot V(1m, t) for the first 70ns.

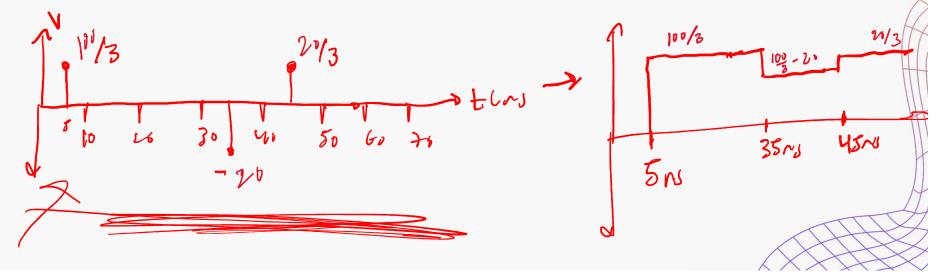


Bounce Diagram Example

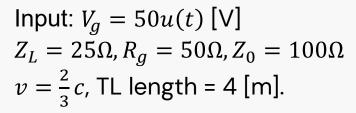
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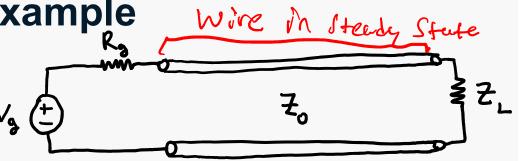


Plot V(1m, t) for the first 70ns.



Bounce Diagram Example





What is the steady-state voltage over the load? What is the steady-state current through the load?

$$V_{SS,L} = \frac{50 \cdot 25}{5.75} = \frac{25}{75} = \frac{50}{3}V$$

$$T_{SS,L} = \frac{V_{SS,L}}{D_L} = \frac{50/3}{25} = \frac{2}{3}A$$

Bounce Diagrams: General Formulation

This is an LTI system!

Input: $\delta(t)$

Output (at position d): V(d, t)

Time to travel down the line: t_0 .

$$V(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) + \tau_g \Gamma_L \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - (n+1)t_0)}_{I(d,t) = \underbrace{\tau_g \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}{v} - nt_0) - \frac{\tau_g \Gamma_L}{Z_0} \sum_{n=0}^{\infty} \left(\Gamma_L \Gamma_g\right)^n \delta(t + \frac{d}$$

For any general input: convolve!

Exam 1 equations, in one place $\nabla \times \vec{E} = 0$

$$\vec{F} = \frac{q_1 q_2}{4\pi\epsilon_0 r^2} \hat{r}$$

$$\vec{F} = q_1 \vec{E} + q_1 (\vec{v}_1 \times \vec{B})$$

$$\vec{E} = \frac{q_2}{4\pi\epsilon_0 r^2} \hat{r}$$

$$\hat{n} \cdot (\vec{D}_1 - \vec{D}_2) = \rho_s$$

$$\hat{n} \times (\vec{E}_1 - \vec{E}_2) = 0$$

$$\hat{n} \cdot (\vec{P}_1 - \vec{P}_2) = -\rho_{b,s}$$

$$Q = CV$$

$$Q = CV \qquad \vec{J} = \sigma \vec{E}$$

$$G = \frac{\sigma}{\epsilon} C \qquad R = \frac{1}{G} \qquad \begin{array}{c} \rho_b = -\nabla \cdot \vec{P} \\ \nabla \cdot \epsilon_0 \vec{E} = \rho_f + \rho_b \end{array}$$

$$\epsilon \oiint \vec{E} \cdot d\vec{S} = Q_{\text{enclosed}}$$

$$\epsilon \oiint \vec{D} \cdot d\vec{S} = Q_{\text{enclosed}}$$

$$\iiint \rho dV = Q_{\text{enclosed}}$$

$$\oint \vec{B} \cdot d\vec{S} = 0$$

$$I = \oiint \vec{J} \cdot d\vec{S} = -\frac{\partial Q_{\text{enclosed}}}{\partial t}$$

$$\epsilon = \epsilon_0 (1 + \chi_e)$$

$$\vec{P} = \epsilon_0 \chi_e \vec{E}$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P} = \epsilon \vec{E}$$

$$\vec{J} = \sigma \vec{E}$$

$$\rho_b = -\nabla \cdot \bar{R}$$

$$\nabla \cdot \epsilon_0 \vec{E} = \rho_f + \rho_b$$

$$\iiint \rho dV = Q_{\text{enclosed}}$$

$$\oiint \vec{J} \cdot d\vec{S} = -\frac{\partial Q_{\text{enclosed}}}{\partial t}$$

$$\nabla \cdot \overrightarrow{D} = \rho$$

$$\nabla \vec{I} - \vec{0}$$

$$\nabla \cdot \vec{J} = -\frac{\partial \rho}{\partial t}$$

$$-\nabla^2 V = \frac{\rho}{\epsilon}$$

$$\nabla \cdot \vec{B} = 0$$

$$\vec{E} = -\nabla V$$

$$\oint \vec{E} \cdot d\vec{l} = 0$$

$$V_{ab} = V(b) - V(a) = -\int_{a}^{b} \vec{E} \cdot d\vec{l}$$

$$\oiint \vec{D} \cdot d\vec{S} = \iiint \nabla \cdot \vec{D} dV$$

$$\oint \vec{E} \cdot d\vec{l} = \iint (\nabla \times \vec{E}) \cdot d\vec{S}$$

$$\int_{a}^{b} \nabla V \cdot d\vec{l} = V(b) - V(a)$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{L}}{\partial t}
-\nabla^2 V = \frac{\rho}{\epsilon}
\nabla \cdot \vec{B} = 0
\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$



Exam 2 equations, in one place

$$\vec{B} = \frac{\mu I}{2\pi r} \hat{\phi}$$

$$d\vec{B} = \frac{\mu I d\vec{\ell} \times \hat{r}}{4\pi r^2}$$

$$\oint_C \vec{H} \cdot d\vec{\ell} = \iint_S \vec{J} \cdot d\vec{S} \qquad \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\oint_{C} \vec{B} \cdot d\vec{\ell} = \mu I_{\text{encl}} \qquad \oint_{C} \vec{E} \cdot d\vec{l} = \varepsilon$$

$$abla imes \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

$$\nabla \cdot \vec{B} = 0$$

$$\Psi = \iint_{S} \vec{B} \cdot d\vec{S}$$

$$-\frac{d}{dt}\iint_{S} \vec{B} \cdot d\vec{S} = \oint_{c} \vec{E} \cdot d\vec{l}$$

$$abla imes ec{E} = -rac{\partial ec{B}}{\partial t}$$

$$\oint_{c} \vec{E} \cdot d\vec{l} = \varepsilon$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$
 $\varepsilon = \frac{W}{q} = \oint_C \frac{\vec{F}}{q} \cdot d\vec{l}$

$$\Psi = LI$$

$$\varepsilon = IR$$

$$\vec{B} = \frac{\mu I}{2\pi r} \hat{\phi} \qquad \qquad \Psi = \iint_{S} \vec{B} \cdot d\vec{S} \qquad \qquad v = \frac{\omega}{\beta} = \lambda f = \frac{1}{\sqrt{\mu \epsilon}} \qquad \vec{J}_{b} = \frac{\partial \vec{P}}{\partial t} + \nabla \times \vec{M}$$

$$\omega = 2\pi f = \frac{2\pi}{T}$$

$$\eta = \frac{\sqrt{\mu}}{\sqrt{\epsilon}}$$

$$\beta = \omega \sqrt{\mu \epsilon}$$

$$\nabla^2 \vec{E} = \mu \epsilon \frac{\partial^2 \vec{E}}{\partial t^2}$$

$$\vec{B} = \frac{\mu I}{2\pi r} \hat{\phi} \qquad \Psi = \iint_{S} \vec{B} \cdot d\vec{S} \qquad v = \frac{\omega}{\beta} = \lambda f = \frac{1}{\sqrt{\mu \epsilon}} \qquad \vec{J}_{b} = \frac{\partial P}{\partial t} + \nabla \times \vec{M}$$

$$d\vec{B} = \frac{\mu I d\vec{\ell} \times \hat{r}}{4\pi r^{2}} \qquad -\frac{d}{dt} \iint_{S} \vec{B} \cdot d\vec{S} = \oint_{C} \vec{E} \cdot d\vec{l} \qquad \omega = 2\pi f = \frac{2\pi}{T} \qquad \vec{H} = \frac{\vec{B}}{\mu_{0}} - \vec{M}$$

$$\oint_{C} \vec{H} \cdot d\vec{\ell} = \iint_{S} \vec{J} \cdot d\vec{S} \qquad \nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \qquad \eta = \frac{\sqrt{\mu}}{\sqrt{\epsilon}} \qquad \vec{B} = \mu_{0} \mu_{r} \vec{H} = \mu \vec{H}$$

$$\hat{n} \cdot (\vec{B}_1 - \vec{B}_2) = 0$$

$$\hat{n} \times (\vec{H}_1 - \vec{H}_2) = \vec{J}_s$$

$$\hat{n} \times (\vec{M}_1 - \vec{M}_2) = \vec{J}_{b,s}$$



Exam 3 equations, in one place

Waves:

	Condition	β	α	$ \eta $	au	$\lambda = \frac{2\pi}{\beta}$	$\delta = \frac{1}{\alpha}$
Perfect		$\omega\sqrt{\epsilon\mu}$	0	. / <u>H</u>	0	9-	∞
dielectric	0	ωνεμ	0	V ε		$\omega\sqrt{\epsilon\mu}$	
Imperfect	$\frac{\sigma}{\omega\epsilon} \ll 1$	$\sim \omega \sqrt{\epsilon \mu}$	$g1 \frac{\sigma}{\sigma} = \frac{\sigma}{2} \sqrt{E}$	$\sim 1/\overline{\mu}$	$\sim \frac{\sigma}{2\omega\epsilon}$	$\sim \frac{2\pi}{\omega\sqrt{\epsilon\mu}}$	$\frac{2}{\epsilon}$
dielectric	$\omega\epsilon$	ωγιμ	$P_2 \sim 2 V \epsilon$	V ε	$2\omega\epsilon$	$\omega\sqrt{\epsilon\mu}$	σ \/ μ
Good	$\frac{\sigma}{}\gg 1$	$\sim \sqrt{\pi f \mu \sigma}$	$\sim \sqrt{\pi f \mu \sigma}$	$\sqrt{\omega\mu}$	45°	$\sim \frac{2\pi}{2\pi}$	$\sim \frac{1}{\sqrt{1-x^2}}$
conductor	WE	VAJAO	γ π η μο	Vσ	13	$\sqrt{\pi f \mu \sigma}$	$\sqrt{\pi f \mu \sigma}$
Perfect	$\sigma = \infty$	∞	∞	0	_	0	0
conductor		00					

$$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$$
 $\tau = \frac{2\eta_2}{\eta_2 + \eta_1} = 1 + \Gamma$

$$v = \frac{\omega}{\beta} = \lambda f$$

$$\nabla^2 \tilde{E} = (j\omega\mu)(\sigma + j\omega\epsilon)\tilde{E}$$

$$A\cos(\omega t - \beta x)\hat{z} \longleftrightarrow Ae^{-j\beta x}\hat{z}$$

$$\Gamma_{L} = \frac{Z_{L} - Z_{0}}{Z_{L} + Z_{0}}$$

$$\tau_{g} = \frac{Z_{0}}{R_{g} + Z_{0}}$$

$$\gamma = \sqrt{(j\omega\mu)(\sigma + j)}$$

$$\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$$

$$\gamma\eta = j\omega\mu$$

$$\gamma = \sigma + j\omega\epsilon$$

$$\gamma = \sqrt{(j\omega\mu)(\sigma + j\omega\epsilon)}$$

$$\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$$

$$\gamma \eta = j\omega \mu$$

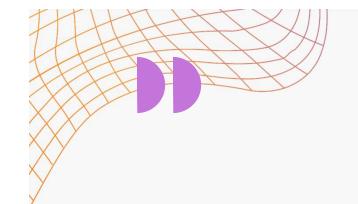
$$\frac{\gamma}{n} = \sigma + j\omega\epsilon$$

$$\vec{S} = \vec{E} \times \vec{H}$$

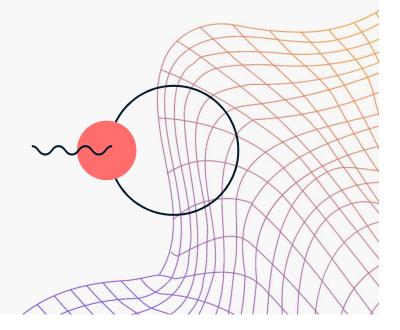
$$\tilde{S} = \tilde{E} \times \tilde{H}^*$$

$$\langle \vec{S} \rangle = \frac{1}{2} \operatorname{Re} \{ \tilde{E} \times \tilde{H}^* \}$$

$$\frac{\partial}{\partial t} \left(\frac{1}{2} \epsilon \vec{E} \cdot \vec{E} + \frac{1}{2} \mu \vec{H} \cdot \vec{H} \right) + \nabla \cdot \vec{S} + \vec{J} \cdot \vec{E} = 0$$



Good luck!



$$\widetilde{T}(0) = Max$$

$$\widetilde{T}(0) = 0$$

V(d) = V+ e+jBd.

$$V(J) = V^{+} e^{+jBJ} + V^{-} e^{-jBJ}$$

$$V(J) = V^{+} e^{+jBJ} + V^{-} e^{-jBJ}$$

$$V(J) = V^{+} e^{+jBJ} - V^{+} e^{-jBJ}$$

$$V(J) = V^{+} e^{-jBJ} - V^{+} e^{-jBJ}$$

$$V(J) = V^{+} (e^{jBJ} - e^{-jBJ})$$

$$T(J) = 2jV^{+} Sin(BJ)$$

$$T(J) = 2V^{+} (o)(BJ)$$

$$Z_{0}$$

$$\frac{\partial}{\partial x} = \frac{\partial}{\partial x} = \frac{\partial$$