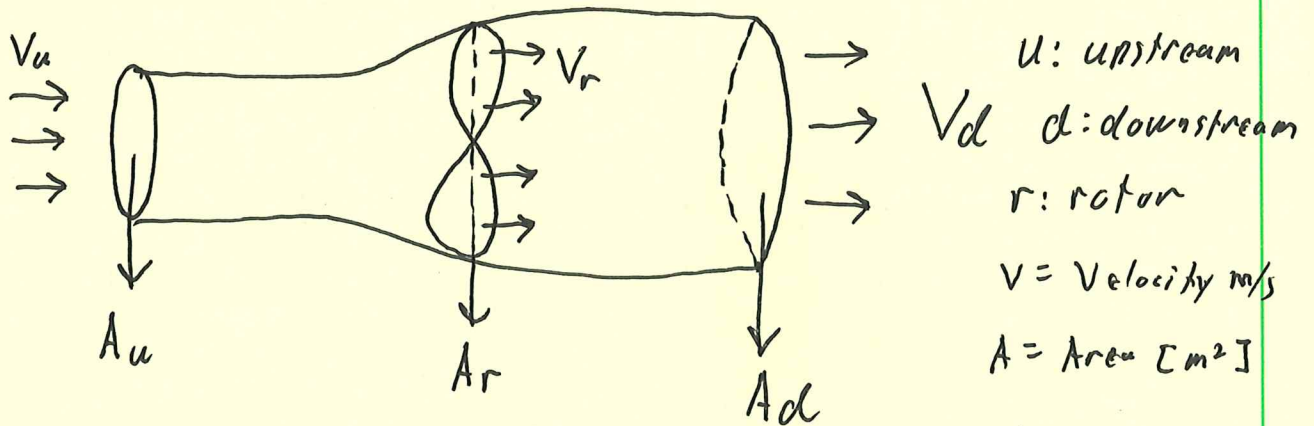


Today

Bernoulli's equation

Betz's Law for maximum Rotor Efficiency

- We went through the derivation of the power present in the wind.
- We saw how this power is associated with the kinetic energy
- Now the question is: How much of this kinetic energy, or how much of this power in the wind stream can be converted to mechanical power?
- It turns out, we cannot extract all the power in the wind stream
- There is a limit, originally derived by a German physicist, Albert Betz (1919)
- We can get a qualitative feeling for what happens as the wind ~~speed~~^{stream} crosses the rotor: the wind speed decreases! → but never drops to zero



- Before the rotor: Kinetic energy = $\frac{1}{2} m V_u^2$
 - ↳ max energy extraction at the rotor would be if wind stops at the rotor $V_d = 0$
 - ↳ Not physically possible → the wind coming behind could not pass
- However, if $V_d = V_u$ (no slowing) then energy extraction would be zero:
 - ⇒ $V_d < V_r < V_u$

Bernoulli's equation

Bernoulli's principle

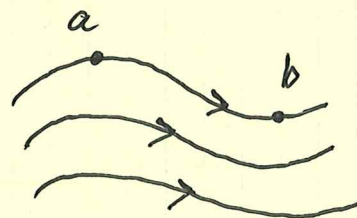
Bernoulli's Principle

The total energy in a fluid is conserved if the flow obeys the following assumptions:

- 1) Points a and b lie on a streamline
- 2) Density, ρ , is constant (incompressible flow)
- 3) steady flow (no turbulence)
- 4) No friction

$$\frac{1}{2} v^2 + gz + \frac{p}{\rho} = \text{const}$$

$$\underbrace{pV}_{\text{pressure Energy}} + \underbrace{\frac{1}{2} mV^2}_{\text{Kinetic Energy}} + \underbrace{mgh}_{\text{potential Energy}} = \text{constant}$$



Streamlines - tangent to velocity vector of flow

In terms of mass that enters & exits the tube:

$$\frac{1}{2} m_a v_a^2 + \rho m_a \frac{h_a}{\rho} + p_a \underbrace{\nabla_a}_{\text{Volume of mass entering}} = \frac{1}{2} m_b v_b^2 + \rho m_b \frac{h_b}{\rho} + p_b \underbrace{\nabla_b}_{\text{Volume of mass exiting}}$$

→ We want to calculate

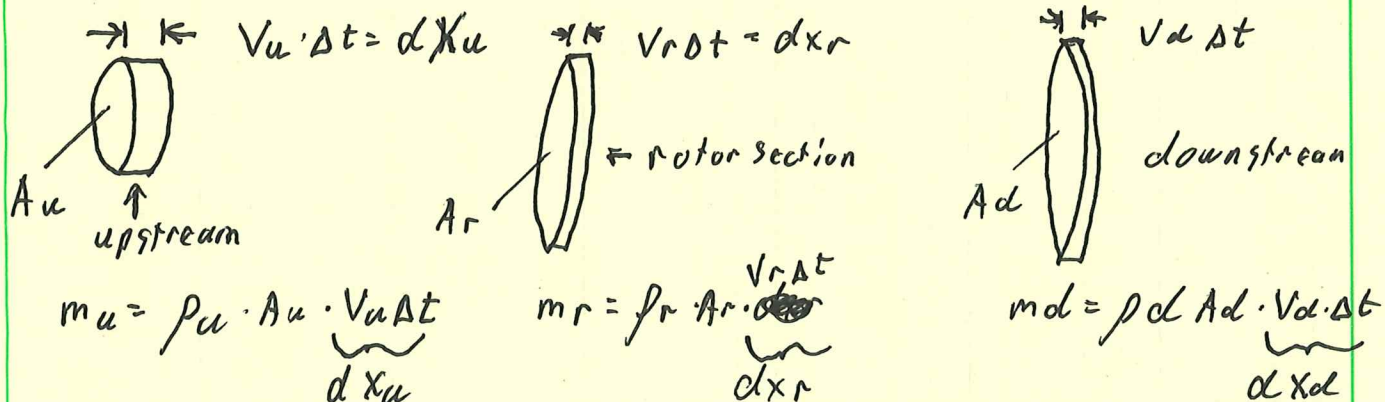
the power (or energy) that can be extracted from the wind as a function of its geometry, and upstream and downstream speeds

We will use three conservation equations:

- Mass
- Energy
- Momentum

~~We will assume: air is incompressible $\Rightarrow \rho$ is constant~~

i) conservation of mass: the mass of an infinitesimal volume remains constant. Δt is a small increment of time

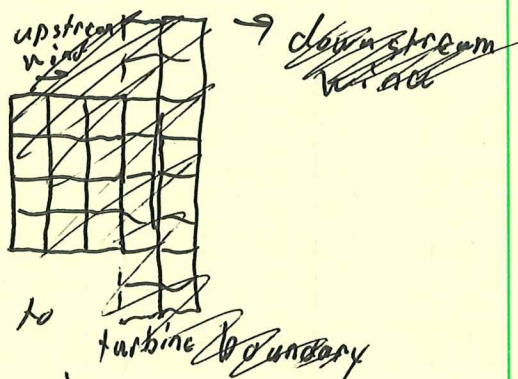


conservation of mass

$$m_u = m_r = m_d \Rightarrow \rho_u \cdot A_u \cdot Vu \cdot \Delta t = \rho_r \cdot A_r \cdot Vr \cdot \Delta t = \rho_d \cdot A_d \cdot Vd \cdot \Delta t$$

$\rho_u = \rho_r = \rho_d = \rho$ (density is constant in tube)

$$\Rightarrow \boxed{A_u Vu = A_r Vr = A_d Vd}$$



ii) Conservation of Energy

Energy upstream is equal to energy downstream plus the energy delivered to the turbine rotor (ΔE_r) ~~as the wind~~.

$$E_u = E_d + \Delta E_r$$

$$E_u = \frac{1}{2} m_u \cdot Vu^2 + m_u \cdot g \cdot h_u + \rho_u \cdot \underbrace{A_u \cdot Vu \cdot \Delta t}_{\text{Volume}}$$

$$E_d = \frac{1}{2} m_d \cdot Vd^2 + m_d \cdot g \cdot h_d + \rho_d \cdot A_d \cdot Vd \cdot \Delta t$$

1. $P_u = P_d$ if we are far enough from turbine
2. By conservation of mass, then

$$\rho u \cdot A_u \cdot V_u \cdot \Delta t = \rho d \cdot A_d \cdot V_d \cdot \Delta t$$

3. $Z_u = Z_d$ (upstream and downstream points are in the same horizontal plane)

$$m_u \cdot g \cdot Z_u = m_d \cdot g \cdot Z_d$$

$$\text{thus: } \frac{1}{2} m_u V_u^2 = \frac{1}{2} m_d V_d^2 + \Delta E_r$$

$$\Delta E_r = \frac{1}{2} m_u V_u^2 - \frac{1}{2} m_d V_d^2$$

$$m_u = \rho V_u \cdot A_u \cdot \Delta t, \quad m_d = \rho V_d \cdot A_d \cdot \Delta t, \quad m_d = m_u$$

$$\Delta E_r = \frac{1}{2} \rho A_r V_r [V_u^2 - V_d^2] \Delta t$$

The power extracted by the turbine is then:

$$P_r = \lim_{\Delta t \rightarrow 0} \frac{\Delta E_r}{\Delta t} = \frac{1}{2} \rho A_r \cdot V_r [V_u^2 - V_d^2]$$

We need to relate V_r with V_u and V_d .

$$\text{It turns out that } V_r = \frac{V_u + V_d}{2}$$

We can derive this through Conservation of momentum. (ii) We won't though.

$$P_r = \frac{1}{2} \rho \cdot A_r \cdot \frac{V_u + V_d}{2} (V_u^2 - V_d^2)$$

Define ratio of downstream to upstream windspeed as:

$$\lambda = \frac{V_d}{V_u} \quad \text{so: (lots of Algebra)}$$

$$P_r = \frac{1}{2} \rho \cdot A_r \cdot V_u^3 \underbrace{\left[\frac{1}{2} (1 + \lambda)(1 - \lambda^2) \right]}_{C_p}$$

$$\frac{dP_r}{d\lambda} = 0 \quad \equiv \quad \frac{dC_p}{d\lambda} = 0 \Rightarrow$$

$$\frac{d}{d\lambda} \left[\frac{1}{2} (1 - \lambda^2 + \lambda - \lambda^3) \right] =$$

$$\frac{1}{2} (1 - 2\lambda - \lambda^2) = 0 \Rightarrow \lambda \begin{matrix} \nearrow 1/3 \\ \searrow 0 \end{matrix}$$

$$\boxed{C_p^{\max} = \frac{1}{2} (1 + 1/3)(1 - (1/3)^2) = 0.593}$$

- does not make sense

The max power that can be extracted is

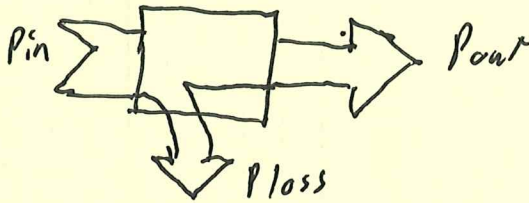
$$P_r = 0.593 \cdot \frac{1}{2} \rho A_r \cdot V_u^3$$

$$C_p^{\max} = 0.593 = \text{Betz Efficiency} = 16/27$$

Most books, including ours, state that the Betz limit is the theoretical efficiency of the rotor. We need to be careful when referring to this efficiency.

Efficiency can be defined as

$$\eta = \frac{P_{out}}{P_{in}}$$



P_{out} in our case is $P_r = 0.593 \cdot \frac{1}{2} A_r \rho V_a^3$

but what is P_{in}

two options:

$$P_{in} = \frac{1}{2} \rho A_u \cdot V_u^3$$

$$\text{or } P_{in} = \frac{1}{2} \rho A_u$$

power available in
wind before being
captured

\Rightarrow not same as power
in Betz expression:

$$\frac{1}{2} \rho A_r V_a^3$$

• If we use this definition of P_{in} , then given $\lambda = 1/3$

$V_d = \frac{1}{3} V_a$ and by conservation of mass

$$A_d \cdot V_d = A_r \cdot V_r = A_u \cdot V_a$$

$$\Rightarrow A_r = A_u \cdot \frac{V_a}{V_r} \quad \text{but } V_r = \frac{V_d + V_d}{2} = \frac{V_a + \frac{1}{3}V_a}{2} = \frac{2}{3} V_a$$

$$\Rightarrow A_r = \frac{3}{2} \cdot A_u$$

$$\Rightarrow P_r = \frac{1}{2} \rho A_r V_a^3$$

$$\Rightarrow P_r = \frac{1}{2} \rho A_r V_a^3 (0.593) = \frac{1}{2} \rho A_u \cdot V_a^3 \cdot \frac{3}{2} (0.593)$$

$$0.889!$$

$$\frac{P_{out}}{P_{in}} = 0.889$$

Another interpretation of P_{in} is the power in the wind stream before the turbine was placed.

In this case $V_r = V_u$
 \uparrow physical location where we place turbine

$$P_{in} = \frac{1}{2} \rho A_u V_u^3 = \frac{1}{2} \rho A_r V_r^3 = \frac{1}{2} \rho A_r V_u^3$$

with this definition, $\eta = 0.593$

\rightarrow ~~both~~ either is valid, as long as you understand

the assumptions that go with each useful relations @ Betz efficiency

$$V_r = \frac{2}{3} V_u \quad V_d = \frac{1}{3} V_u \quad V_d = \frac{V_r}{2}$$

$$A_r = \frac{3}{2} A_u \quad \underline{A_d = 3 A_u} \quad A_d = 2 A_r$$

good HW problem